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MATHEMATICAL CONCEPTS AND HISTORICAL DEVELOPMENT OF THE MASCOT GUIDANCE TECHNIQUE FOR SPACE VEHICLES

By C. D. Baker, W. E. Causey and H. L. Ingram Aero-Astrodynamics Laboratory

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MATHEMATICAL CONCEPTS AND HISTORICAL DEVELOPMENT OF THE MASCOT GUIDANCE TECHNIQUE FOR SPACE VEHICLES

SUMMARY

The recent development of improved integration routines, improved trajectory computation algorithms, and faster, lighter, more flexible flight-worthy digital computers has opened up new possibilities for improved guidance concepts and effective application of optimal guidance schemes to meet the challenges of the post-Apollo space vehicles.

This report documents one such guidance concept which permits practical realization of many heretofore unrealizable optimal guidance tasks, namely, on-board optimization of ascent trajectories through the atmosphere, self-targeting, optimal rendezvous, optimal coast-burn-coast-burn orbital transfer, and reentry for high lift-to-drag-ratio type of vehicles.

This collection of techniques combined into one guidance program has been called MASCOT (Manned Shuttle Comprehensive Optimization and Targeting).

I. INTRODUCTION

The advent of a new generation of space vehicles (specifically NASA's post-Apollo space shuttle) with advanced features such as completely reusable stages, sophisticated on-board digital computers, and airplane-type landing characteristics for both booster and orbiter has required a re-evaluation of the space vehicle guidance concepts used in the past. When re-examined, these traditional guidance concepts have been found to be inadequate for the new generation of space vehicles. In response to this need, new concepts, procedures, and techniques have recently been developed which provide a significant improvement in optimal guidance applications. In particular, this new approach yields a physically realizable optimal guidance scheme which results in nearly optimal performance for the boost phase, the rendezvous phase, and the reentry phase of the post-Apollo shuttle vehicle flight path. This new system and concept has been given the name MASCOT.

The MASCOT concept is made possible by the development of new mathematical techniques and the significant improvement of others. It also takes advantage of the improved speed, memory capacity, and reliability of the new flight-worthy digital computers.

In this report, the evolution and mathematical theory of the MASCOT guidance technique are explained. In addition, some computer-simulated trajectories obtained by means of the MASCOT program are presented to demonstrate the accuracy, flexibility, and optimality of the MASCOT system. Some comparisons will be made, whenever practical, with results obtained from the present Saturn Iterative Guidance Mode (IGM).

II. SOME BACKGROUND ON GUIDANCE, NAVIGATION, AND CONTROL

The operation of a guidance system involves three interrelated divisions of effort, navigation, guidance signal generation, and control. Navigation is concerned with the determination of the current position and velocity of the vehicle. Navigation is normally an openloop process for short flights but must be made closed-loop by navigation update in some instances, i.e., long flight times.

With an accurate knowledge of all physical parameters of vehicle and environment, current position and velocity, and an accurate knowledge of the desired terminal conditions, it is possible to determine the proper directions of the engines thrust to obtain the desired end conditions. This closed-loop process of thrust-direction determination is referred to as guidance signal generation.

The control system implements the guidance signals in addition to employing such maneuvers that may be required to preserve the structural integrity of the vehicle. Thus, the control system may temporarily ignore or minimize the influence of the guidance signal in order to protect the vehicle from winds, wind gusts, wind shears, vibrational disturbances, or fuel sloshing problems. Control, too, is a closed-loop process.

III. THE GENERAL CONCEPT OF GUIDANCE

Implementation of the guidance signal will determine the vehicle flight path to reach a desired destination or set of terminal conditions. Perfect operation of the navigation system, exact generation of the guidance signal, and exact implementation of the control system, together with an exact knowledge of the vehicle physical parameters and

an exact knowledge of the physical environment during the entire flight to the desired end conditions, would make it possible to solve for the guidance signal only once. This signal would, of course, be a function of time or some other convenient variable so that the guidance signal would change continuously during the flight.

In practice, perfect operation of the three systems cannot be achieved. Thus, a practical guidance system may make the computations at the initiation of guidance, and predict the required guidance signal or function to guide to the required end conditions. Since the initial information will have some inaccuracies, the process must be repeated periodically during the flight, treating each instant at which the new computations occur as a new set of initial conditions.

IV. OPTIMAL GUIDANCE

Optimal guidance, a subclass of the broad class of guidance concepts, is characterized usually by the deliberate maximization or minimization of some aspect of vehicle performance, for example, maximum payload to a given orbit or equivalently minimum fuel required for a given payload.

To accomplish optimal guidance of a vehicle, a mathematical model of the vehicle motions must first be chosen. Appearing in these equations of motion are the so-called control variables. These variables are the equation parameters which can be given an arbitrary (within prescribed limits that depend on the problem) value at any instant along the vehicle's flight path. This large amount of freedom of selection for the control variables allows a time history for the control variables to be chosen which achieves a desired destination and also optimizes some specified aspect of the vehicle performance. For a typical rocket-powered vehicle, the control variable is usually the thrust direction, and a time history of this thrust direction is determined (as described previously) to maximize the payload delivered to a particular destination.

A. Mathematical Techniques of Optimal Guidance

The different mathematical techniques used to select the optimum control variable are usually grouped into a body of knowledge known as optimization theory or calculus-of-variations theory.

When some type of optimization theory is applied to the differential equations simulating the motion of a rocket-powered vehicle, a two-point boundary value problem is produced. This means that not all of the initial conditions for the differential equations involved are known

at the initial time. The unknown initial conditions must be determined so that they cause the results of the integration of the differential equations to satisfy some pre-specified conditions at the final time or destination. To accomplish this, in practice, one usually attempts to discover, numerically, some mathematical relations which connect the initial conditions with the final conditions. Then, the desired conditions at the destination are placed in these relations, and the resulting equations are solved, hopefully, to yield values for the missing initial conditions. These initial conditions and the relations connecting the initial conditions with the final conditions yield the time history of the control variables that optimize the chosen criterion of the vehicle's performance. In practice, there may be additional relations or constraints to be satisfied by a particular vehicle's trajectory which produce a multi-point boundary value problem instead of the simple two-point boundary value problem described above. These aspects of optimization theory are examined in more detail in the section on mathematical development.

B. The Philosophy of Optimal Guidance: Old and New

In the past, computer technology and mathematical techniques were inadequate to allow the consideration of a realistic computational algorithm for trajectory optimization as a practical on-board guidance signal generator. Thus, older techniques for on-board guidance signal generation relaxed the reality of the mathematical simulation of the vehicle's motion or degraded the optimality of the solution path in order to solve the resultant boundary value problem rapidly enough to control a particular vehicle's flight. The new MASCOT concept (which is a realistic computational algorithm for trajectory optimization) can be considered as a guidance signal generator for all phases of a vehicle's flight (boost phase, rendezvous phase, and reentry phase). This advance is possible at the present time because of improvements in computer technology and mathematical techniques for the solution of optimal trajectory problems.

Before going directly into the explanation and results associated with MASCOT, we briefly outline the historical developments which led to the present form of the MASCOT guidance technique. For readers not familiar with some of the ideas and terminology contained in this historical development, an extensive list of references and a bibliography are included at the end of the report.

V. HISTORICAL BACKGROUND

A. Delta Minimum Guidance

Beginning with the V-2 rockets in the mid-1940's and continuing through the Redstone, Jupiter, and Pershing missiles, the "delta-minimum" guidance concept was used successfully to guide rocket flights. The delta-minimum concept required that both nominal and perturbed trajectories follow essentially the same geometrical trajectory regardless of other considerations. On-board flight computations were simple, and analog computation was used for the execution of the delta-minimum concept.

B. Iterative Guidance Mode

In 1960, research work was begun to develop new guidance concepts for the Saturn space vehicles [1,2,3]. This work was motivated by the development of new mathematical techniques for maximization of payload through optimization methods and by the development of digital computers to replace analog computers as on-board hardware. It was also obvious that space trajectories would require greater flexibility to cope with sudden changes, such as engine out, and that more options must be permitted in the selection of flight profiles. The guidance law which resulted from the research work begun in 1960 and which has been flown on Saturn vehicles was given the name IGM, Iterative Guidance Mode.

IGM is essentially an approximate formulation of the calculus-of-variations problem that allows analytic construction of major parts of the solution, so that only a simple iterative numerical process is required for solution. This approach avoids the time-consuming numerical integration procedures that have been required to compute a general solution to the fundamental calculus-of-variations problems. The speed needed for real-time application has been the primary motivation for the derivation of semi-explicit methods of this type.

However, as a result of the approximations, the optimality and flexibility of such flight schemes are limited, primarily in that they are nearly optimal only for short arcs of powered flights and for specialized mission (boundary value) conditions in a restricted coordinate system. This limitation can be relaxed somewhat in practice by use of special purpose adjustments, but only at the expense of additional preflight analysis and simulation.

The basic simplifications made in the Iterative Guidance Mode to obtain analytic construction of major parts of the solution were (1) to

assume a uniform gravitational field rather than an inverse square law and (2) to apply the same transversality condition at engine cutoff regardless of the mission flown. There were, incidentally, some small-angle approximations and ingenious special purpose adjustments made to improve the optimality of the scheme and to reduce the computational effort required for on-board mechanization. However, the basic concept of the simplifications is best seen in view of the assumption concerning the gravitational field and the assumption of the adequacy of a single transversality condition.

C. QUOTA

Next came the QUasi Optimal Trajectory Analysis, QUOTA [4], which belongs in the same category with IGM since it too is an approximation to the calculus-of-variations (COV) solution.

The fundamental approximation in QUOTA may be viewed in at least two different ways. The first way may be said to be an approximation to the COV in the sense that the Euler-Lagrange equations are replaced by a slightly different set of equations, the purpose of which is to allow analytic integration of both the "state" and "co-state" equations. Of course, the "co-state" variables must be interpreted in a generalized sense because they are not obtained from the Euler-Lagrange equations.

A second manner of viewing the approximations to achieve the solutions will be mentioned. From many observations of the behavior of the Lagrange multipliers (λ 's) in the calculus of variations, it has been noted that for rocket flights in a wide variety of missions, these λ 's are very nearly linear functions of time. The QUOTA equations may be derived by assuming linear λ 's and by expanding the gravity term in series.

The advantage of this approach is a very rapid computational scheme which is much more flexible than IGM and also leads to a smaller loss of optimality. Even this small loss of optimality may be regained by making the assumption that the $\lambda's$ are linear only for a portion of the flight; thus, the λ versus time curve is represented by a series of connecting straight lines where the slopes of the linear λ segments are determined from the Euler-Lagrange equations. For an Apollo-type mission, the $\lambda's$ may be assumed to be linear for the entire flight with only a negligible loss in payload.

With either of the viewpoints mentioned above, the true gravitational field may be accurately represented and transversality conditions may be fitted to the particular end conditions. Needless to say, the optimality of the solution must be checked because of the substitution of approximate equations for the Euler-Lagrange equations.

Computationally, QUOTA offered much more flexibility than IGM, required less preflight analysis and only slightly increased the amount of on-board computation required. Because IGM was entirely adequate for all Saturn flights, there has been no need to change from IGM to QUOTA and, therefore, QUOTA has never been tested on any actual flights. It is still available for any mission which requires flexibility beyond IGM capability and for which the same computational equipment must be used.

D. OPGUID AND SWITCH

Before 1965, general (flexible) numerical procedures for computing precise optimal trajectories were too unreliable in convergence and costly in computational requirements to be considered for real-time guidance. However, an indirect method for computing optimal trajectories [5,6] was developed in 1965 incorporating improved techniques to obtain a substantial gain in speed, convergence, and flexibility. A simple scaling rule for the amount of the Newton correction that was permitted per iteration resulted in an extremely large region of convergence that was surprisingly insensitive to accurate initialization of the boundary value problem.

The indirect approach is particularly well suited for real-time use, where the continual adjustment of the guidance scheme to accommodate perturbations in initial conditions is readily accomplished by a single Newton iteration on the boundary value problem. In 1966, the feasibility of this approach as a real-time guidance scheme for optimizing single-burn-arc orbital injection missions was demonstrated [7] and named OPGUID (OPtimal GUIDance).

However, many orbit transfer problems require the use of several burn arcs separated by relatively long optimal coast arcs. A multiburn-arc version of OPGUID, developed in 1967 [8], demonstrated that the attractive fundamental approach of OPGUID could successfully converge a general formulation of this problem, with variable boundary conditions. A sophisticated version of the multi-burn program (SWITCH) has been developed [9] that has successfully converged a variety of orbital transfer problems with an efficiency and reliability comparable to that of the original OPGUID.

As a result, the indirect method of SWITCH is not only feasible but considerably superior to existing implementations of quasilinearization in convergence as well as efficiency. A principal feature of SWITCH is the use of classical two-body theory to render the computations for coast arcs explicit. Since high-thrust multi-burn orbit transfers usually involve coast arcs many times longer in duration than burn arcs,

the explicit method results in a substantial savings in computation per iteration. A universal variable formulation of the two-body problem with closed-form expressions for the state transition matrix is used. This formulation was adapted from the work in references 8, 10, 11 and 12 in a novel way to avoid the cumbersome computation of the three-dimensional tensor of second partial derivatives of final state with respect to initial state that is required when computing the partial derivative of final co-state with respect to initial state.

Since all the partial derivatives are available at each iteration, as was the case for the original OPGUID, the SWITCH algorithm is appropriate for computing real-time corrections to in-flight perturbations.

Unlike the OPGUID algorithm, the SWITCH algorithm does require reasonable initialization. That is, it is not possible with SWITCH as it was with OPGUID to misalign the thrust direction by 90 or 180 degrees and retain convergence. However, rough estimates of impulsive solutions have proved more than adequate as initialization in every trial case.

E. MASCOT

With the advent of the space shuttle with its high aerodynamic lifting characteristics both on ascent and descent, it has become imperative that optimal guidance laws be devised to optimally steer the vehicle through the atmospheric portions of flight.

This has been accomplished essentially by introducing into the SWITCH program the aerodynamic effects of both lift and drag [13]. Additionally, the effect on thrust of pressure variation with altitude has been included in the propulsion computations.

These changes have recently been carried out, and some of the observed results may be summarized as follows:

- 1. Maximum payload and maximum sensitivity to convergence occur when atmospheric effects are introduced into both the state and co-state equations.
- 2. Approximately two-thirds of the payload increases obtained under (1) may be kept by introducing the atmospheric effects into the state equations only. In this case, convergence is far easier.
- 3. Extremely difficult convergence cases may be approached gradually by multiplying the atmospheric model by $0 \le K \le 1$ where K starts at zero and gradually increases to 1. For each value of K, the case is converged before increasing the value of K.

When the atmospheric effects, together with changes to be described later, were added to the SWITCH concept, the name MASCOT was chosen for the overall scheme to handle multiple burn-coast-burn optimal trajectories both in and out of the atmosphere.

VI. MATHEMATICAL DEVELOPMENT FOR MASCOT

A. The Choice of a Physical Model Common to All Flight Phases

The first step in the development of an optimal guidance technique for a rocket-powered vehicle is the mathematical modeling of the vehicle's trajectory. To do this, a second order three-dimensional vector of ordinary differential equations is usually used which consists of the sums of the vector accelerations produced by all the forces to be considered acting on the vehicle. For the MASCOT scheme, this sum of vector accelerations must consist of terms produced by forces acting during the boost phase, the rendezvous phase, and the reentry phase. During the computation of a trajectory for a particular phase, all of the terms in the sum for all of the phases do not have to be considered and the unneeded terms can be easily ignored with the logic of the computer program. The next section develops in detail the general mathematical model, and then the terms to be ignored in particular phases are pointed out specifically.

B. Mathematical Modeling of Vehicle's Motion

1. Comments on Coordinate Transformation

A three-dimensional Cartesian coordinate system with an origin at the earth's center will be used. The orientation of this coordinate system will be assumed to remain fixed with respect to time and the initial orientation is completely arbitrary. To compare trajectories in this arbitrarily oriented coordinate system with any other coordinate system, their relative orientations at comparison times must be known so that a coordinate transformation can be performed on one of the coordinate systems. Some coordinate systems of interest do not always have their origin at the earth's center, but this is a simple translation if relative orientations are the same. For example, in booster work, an inertial coordinate system with origin at the earth's center could be defined to have the z-axis perpendicular to the earth's equatorial plane and pointing northward, the x-axis in the equatorial plane and pointing toward the Greenwich Meridian at some reference time (usually launch time), and the y-axis placed in the equatorial plane to form a right-hand system. Then, any other coordinate system can be oriented with respect to this coordinate system with the aid of the standard Euler angle rotation

matrices. That is, for a given angle α , the Euler angle rotation matrices for rotations about the x, y, and z axis are written as follows:

$$(\alpha)_{1} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \alpha & \sin \alpha \\ 0 & -\sin \alpha & \cos \alpha \end{bmatrix}$$

$$(\alpha)_{2} = \begin{bmatrix} \cos \alpha & 0 & -\sin \alpha \\ 0 & 1 & 0 \\ \sin \alpha & 0 & \cos \alpha \end{bmatrix}$$

$$(\alpha)_3 = \begin{bmatrix} \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

Then coordinates in the equatorial coordinate system just defined (denoted by \bar{x}_e) can be transformed to coordinates in the standard Apollo coordinate system (denoted by \bar{x}_p) in the following manner:

$$\bar{x}_{p} = (-A_{Z_{0}})_{1}(-\phi_{d})_{2}(-\lambda_{o})_{3}\bar{x}_{e},$$

where

 λ_{o} is the longitude of the launch site measured positive west

 ϕ_{d} is the geodetic latitude of the launch site

 ${\rm A_{Z}}_{\rm O}$ is the launch azimuth of firing direction and is measured clockwise from a line perpendicular to the plumbline at the launch site and pointing northward parallel to the launch site meridian around to the firing direction.

Note that the inverse transformation to obtain equatorial coordinates from plumbline coordinates is easily remembered due to its mnemonic form. That is,

$$\bar{x}_{e} = (\lambda_{o})_{3}(\phi_{d})_{2}(A_{Z_{o}})_{1}\bar{x}_{p}.$$

Also, the transformation matrix, [A] = $(\lambda_0)_3(\phi_d)_2(A_{Z_0})_1$, remains constant with time.

For reentry work, a more interesting coordinate system might be a coordinate system with the origin at the reentry point with its x-axis pointed radially away from the earth's apparent gravitational center, its z-axis parallel to a projection of the instantaneous velocity vector in the local horizontal plane, and the y-axis finishing a right-handed coordinate system. A transformation from this coordinate system (denoted by x_r, y_r, z_r) to the equatorial coordinate system can be written as

$$\bar{\mathbf{x}}_{e} = (\lambda_{r})_{3}(\varphi_{d_{r}})_{2}(\mathbf{A}_{\mathbf{Z}_{r}})_{1} \left\{ \bar{\mathbf{x}}_{r} + \mathbf{R}_{r} \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \right\},$$

where

 $\lambda_{r}^{}$ is the longitude of the reentry point measured positive west,

 $\phi_{\mbox{\scriptsize d}_{\mbox{\tiny L}}}$ is the geodetic latitude at the reentry point,

 ${\rm A_{Z}_{r}}$ is the instantaneous reentry flight direction measured as is ${\rm A_{Z_{o}}}$,

 R_r is the reentry point altitude.

Thus, the equations of motion for a point mass in a three-dimensional inertial Cartesian coordinate system whose orientation to the standard equatorial coordinate system is known can be written as will be shown in the following paragraphs.

 Acceleration of a Point Mass in an Earth-Centered Arbitrarily Oriented Inertial Coordinate System

In an arbitrarily oriented earth-centered Cartesian coordinate system, the differential equations to be used for simulating the motion of a point mass subject to gravitational, aerodynamic, and thrusting forces can be written as follows:

$$\ddot{\bar{x}} = (F/m)\bar{u} + \frac{\bar{L} + \bar{D}}{m} - \frac{(GM)\bar{x}}{R^3} + \bar{g}(\bar{x}). \tag{1}$$

In the above vector differential equation, the first term on the right is the thrusting term, where F is the instantaneous magnitude of the thrust, m is the instantaneous mass, and $\bar{\mathbf{u}}$ is a unit vector which is considered to be a control variable for the direction of the thrust. In the second term, L is a vector of aerodynamic forces due to lift and \bar{D} is a vector of aerodynamic forces due to drag. The determination and control of the thrusting force and the aerodynamic forces will be explained in the paragraphs to follow. The third term in equation (1) is the gravitational force term for a spherical central body, where GM is the gravitational constant and R is the magnitude of the position vector of the point mass under consideration. The fourth term which is considered to be a function of the position vector is a symbolic representation of corrections to the gravitational force expression which are needed when a nonspherical shape for the central body is considered. For simplicity in the rest of this development, the fourth term on the right-hand side of equation (1) will be ignored, and no further explanation of the derivation of the third term will be attempted since this expression is a very standard representation of the gravitational force due to a spherical central body.

To begin an explanation of the first term (the term due to thrust) in equation (1), the thrust force F will be assumed to be constant for vacuum flight and to have the following form for atmospheric flight:

$$F = F_{S} + A_{e}(P_{O} - P),$$
 (2)

where

 F_s is the vehicle's thrust measured at sea level (P = P_o)

A is the exit area of the engine

 P_{o} , P are the atmospheric pressure at sea level and at any altitude, respectively.

For atmospheric flight, the mass flow rate m is given by the relation

$$\dot{m} = \frac{-F_s}{g_o I_{sp_s}}, \qquad (3)$$

where $I_{\text{SP}_{S}}$ is a constant (measured to correspond with F_{S}) indicating the efficiency of a particular set of engines and $g_{\text{O}} = GM/R_{\text{O}}^{2}$ is a constant giving the acceleration due to gravity at the assumed R_{O} (radius of the spherical central body). For vacuum flight the mass flow rate is assumed to be the same as for atmospheric flight and the force F_{V} and

efficiency I_{Sp_V} for vacuum flight are related to F_S and I_{Sp_S} as follows:

$$F_v = F_s + A_e P_o$$

$$I_{sp_v} = (F_v/F_s) I_{sp_s}$$

In either case, the mass at any time t referenced to an initial time $t_{\rm O}$ is given by

$$m(t) = m(t_0) + \dot{m}(t - t_0).$$
 (4)

To explain how the unit vector $\bar{\mathbf{u}}$ and the aerodynamic force vectors $\bar{\mathbf{L}}$ and $\bar{\mathbf{D}}$ are to be determined, a missile-fixed or vehicle-fixed coordinate system (denoted by $\mathbf{x}_m, \mathbf{y}_m, \mathbf{z}_m$) must be introduced. In this coordinate system, $\bar{\mathbf{u}}$ will be denoted by $\bar{\mathbf{u}}_m$ and another unit vector $\bar{\mathbf{a}}_m$ ($\bar{\mathbf{a}}_m$ is the vehicle axis which when aligned with the air stream allows no aerodynamic lifting force to be produced) will be introduced. Figure 1 illustrates the angles to be used to locate $\bar{\mathbf{u}}_m$ and $\bar{\mathbf{a}}_m$ in the missile-fixed coordinate system.

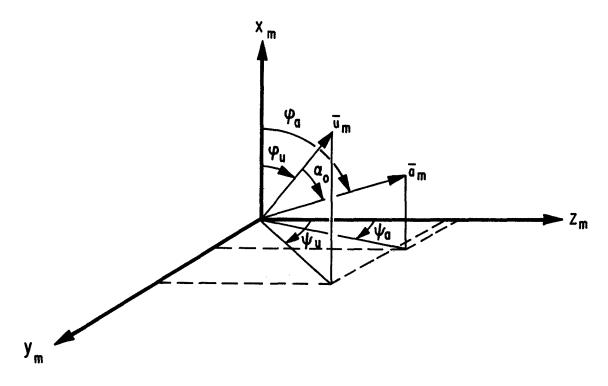


Figure 1. Angles used to Locate $\bar{\mathbf{u}}_m$ and $\bar{\mathbf{a}}_m$ in the Missile-Fixed Coordinate System

In the missile-fixed coordinate system, the angles ϕ_u and ψ_u are measured on the ground as a function of trajectory time or burning time to locate \bar{u}_m , which is the thrust direction produced by the unswiveled engines. Similarly, the angles ϕ_a and ψ_a are measured on the ground as a function of trajectory time to locate \bar{a}_m . These angles locating \bar{u}_m and \bar{a}_m in a missile-fixed coordinate system need to be determined only once before the initial flight of each vehicle. Then the angle α_0 shown in figure 1 can also be computed as a function of trajectory time. The angle α_0 and the unit vector \bar{a} or \bar{a}_m will be used later in the determination of \bar{L} and \bar{D} , but for now only the unit vector \bar{u} or \bar{u}_m is of interest.

As shown in figure 2, the angles χ_p and χ_y will be used to locate \bar{u} or \bar{u}_m in the original inertial Cartesian coordinate system (x,y,z). The prime coordinate system (x',y',z') with the x' coordinate aligned with \bar{u} will be shown again in figure 5 and used to help define the aerodynamic forces. It will be assumed that the vehicle's control system acts instantaneously so that the angles χ_p and χ_y , and thus the direction of \bar{u} in the inertial coordinate system, can be changed instantaneously. As the angle χ_p and χ_y or the direction of \bar{u} change with respect to the inertial coordinate system shown in figure 2, the orientation of the

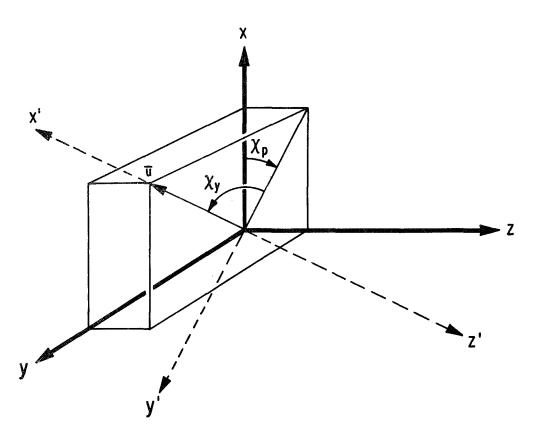


Figure 2. Angles Used to Locate $\bar{\mathbf{u}}$ in the Inertial Coordinate System 14

missile-fixed coordinate system will also be changed with respect to the inertial coordinate system, since the angles ϕ_u and ψ_u cannot be changed by the vehicle's control system.

Often the vehicle's control system may be given a time history of the angles X_p and X_y to follow. In this case, \bar{u} must be computed in terms of X_p and X_y so that it can be used in equation (1) for simulation purposes. As shown in figure 2,

$$\bar{\mathbf{u}} = \begin{bmatrix} \mathbf{u}_1 \\ \mathbf{u}_2 \\ \mathbf{u}_3 \end{bmatrix} = \begin{bmatrix} \cos \mathbf{x}_{\mathbf{y}} & \cos \mathbf{x}_{\mathbf{p}} \\ \sin \mathbf{x}_{\mathbf{y}} \\ \cos \mathbf{x}_{\mathbf{y}} & \sin \mathbf{x}_{\mathbf{p}} \end{bmatrix}. \tag{6}$$

If optimization theory is used to obtain $\bar{\mathbf{u}}$, then the components of $\bar{\mathbf{u}}$ in the inertial coordinate system may be determined directly by the optimization theory. In this case, for the information of the vehicle's control system, the angles \mathbf{X}_p and \mathbf{X}_y can be computed in terms of the components of $\bar{\mathbf{u}}$ as follows:

$$\chi_{y} = \arctan\left(\frac{u_{2}}{\sqrt{u_{1}^{2} + u_{2}^{2}}}\right) \qquad (-\frac{\pi}{2} < \chi_{y} < \frac{\pi}{2})$$
 (7)

$$X_p = \arctan (u_1/u_3)$$
 $(0 \le X_p \le 2\pi).$ (8)

This completes the present discussion of \bar{u} which appears in the first term of equation (1). In section IV-C, how \bar{u} is determined by optimization theory is discussed.

Now to explain how the expressions for \bar{L} and \bar{D} are obtained in the second term of equation (1), the unit vector \bar{a} or \bar{a}_m introduced in figure 1 will be used. First, it will be assumed that $\bar{a} \neq \bar{u}$ so that the unit vectors \bar{a} and \bar{u} define a plane in the reference coordinate system (see figure 3).

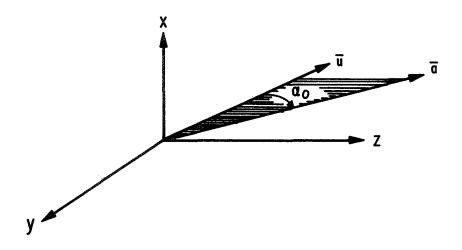


Figure 3. The Plane Formed by \bar{u} and \bar{a} in the Inertial Coordinate System

In a later section, the simplifying assumption $\bar{a}=\bar{u}$ is made and the results of this assumption are treated. As mentioned previously, the unit vector \bar{a} is defined to lie along the instantaneous zero lift axis of the vehicle. Thus, if \bar{a} and the relative velocity vector \bar{V}_r of the point mass are aligned, \bar{L} will be zero. The relative velocity vector in the reference coordinate system is given by

$$\bar{\nabla}_{r} = \dot{\bar{x}} - \bar{\omega} \times \bar{x} - \bar{W}, \tag{9}$$

where $\bar{\omega}$ is the rotational velocity vector of the central body in the reference coordinate system and \bar{W} is an arbitrary vector function describing winds in the reference coordinate system. Since \bar{a} is a unit vector in the zero lift direction, a lift force (denoted by \bar{L}) will be produced when there is an angle α between \bar{a} and \bar{V}_r as shown in figure 4. Figure 4 shows that the lifting force \bar{L} which occurs when there is an angle α between \bar{a} and \bar{V}_r lies in the plane formed by the vectors \bar{a} and \bar{V}_r . Naturally, the vector \bar{D} is in a direction opposite to \bar{V}_r .

To explain further how the unit vector $\tilde{\mathbf{a}}$ is to be defined, it will be assumed that the directions of $\tilde{\mathbf{u}}$ and $\tilde{\mathbf{a}}$ in the missile-fixed coordinate system are determined as shown in figure 1. It will also be assumed that these directions in the missile-fixed coordinate system depend only on the vehicle characteristics such as the position of the center of gravity and the center of pressure as functions of trajectory time. Thus, the angle α_0 between $\tilde{\mathbf{u}}$ and $\tilde{\mathbf{a}}$ (as shown in figures 1 and 3) can be determined

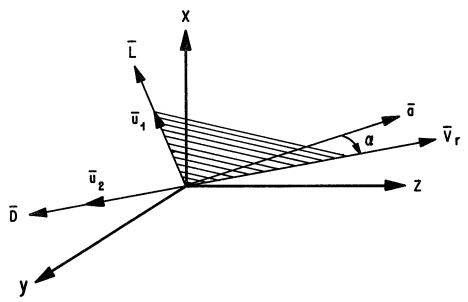


Figure 4. The Lift and Drag Force in the Inertial Coordinate System

as a function of trajectory time. Since α_0 depends on the vehicle characteristics, it cannot be used as a control variable and varied by the vehicle's control system. Although the angle α_0 is not considered to be a control variable, it will be assumed that the vehicle's engines can roll the vehicle about $\bar{\mathbf{u}}$ (as shown in figure 3) so that the orientation of the plane formed by the vectors $\bar{\mathbf{a}}$ and $\bar{\mathbf{u}}$ is a control variable. Also, as the direction of $\bar{\mathbf{u}}$ is changed (with the control variables $\mathbf{x}_{\mathbf{p}}$ and $\mathbf{x}_{\mathbf{y}}$), the direction of $\bar{\mathbf{a}}$ will change because the angle between $\bar{\mathbf{a}}$ and $\bar{\mathbf{u}}$ (denoted by α_0) is predetermined and cannot be varied.

To write expressions for the components of \bar{a} in the reference coordinate system, a new coordinate system whose orientation changes with trajectory time (denoted by x',y',z') will be introduced. This new coordinate system is obtained by performing in succession the Euler angle rotations $(X_p)_2$ and $(X_y)_3$ so that the x' axis lies along \bar{u} as shown in figure 2. In the prime coordinate system, the angles α_0 and x_R (which orient the plane formed by \bar{u} and \bar{a}) can be depicted as in figure 5. The symbol \bar{a} ' will be used to denote the unit vector \bar{a} with its components in the prime coordinate system. These components (see figure 5) are given by the following equation:

$$\bar{\mathbf{a}}' = \begin{bmatrix} \cos \alpha_0 \\ \sin \alpha_0 & \cos X_R \\ \sin \alpha_0 & \sin X_R \end{bmatrix}. \tag{10}$$

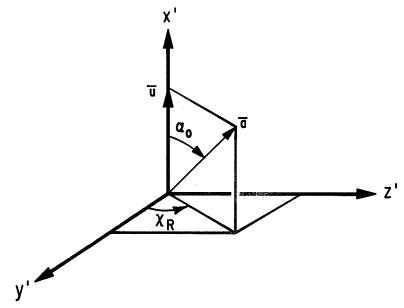


Figure 5. The Orientation of the Plane Formed by $\bar{\mathbf{u}}$ and $\bar{\mathbf{a}}$

Then, \bar{a} with components in the reference coordinate system is obtained as follows:

$$\bar{a} = (X_p)_2(-X_y)_3\bar{a}'.$$
 (11)

Notice that the successive Euler angle rotations $(-\chi_y)_3$ and $(\chi_p)_2$ are the inverse of the Euler angle rotations used to obtain the prime coordinate system. With a determined by equation (11) in terms of χ_p , χ_y , χ_R , and α_o , unit vectors in the direction of \bar{L} and \bar{D} can be written as:

$$\bar{\mathbf{u}}_{1} = \frac{(\bar{\mathbf{v}}_{r} \times \bar{\mathbf{a}}) \times \bar{\mathbf{v}}_{r}}{|(\bar{\mathbf{v}}_{r} \times \bar{\mathbf{a}}) \times \bar{\mathbf{v}}_{r}|}$$
(12)

$$\bar{\mathbf{u}}_2 = -\frac{\bar{\mathbf{v}}_r}{|\bar{\mathbf{v}}_r|} . \tag{13}$$

Figure 4 will aid the reader in visualization of the construction of the vectors $\bar{\bf u}_1$ and $\bar{\bf u}_2$ which are written in the reference coordinate

system (since \bar{a} and \bar{V}_r are in the reference coordinate system). Now the following expressions for \bar{L} and \bar{D} can be written:

$$\bar{L} = \frac{1}{2} \rho A_r (\bar{V}_r \cdot \bar{V}_r) C_L \bar{u}_1$$
 (14)

$$\bar{\mathbf{D}} = \frac{1}{2} \rho \mathbf{A}_{\mathbf{r}} (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}}) \mathbf{C}_{\mathbf{D}} \bar{\mathbf{u}}_{\mathbf{z}}, \tag{15}$$

where

ρ is the atmospheric density

 $\mathtt{A}_{\mathtt{r}}$ is the reference area of the vehicle

 C_{τ} is the lift coefficient of the vehicle

 $\mathbf{C}_{\mathbf{D}}$ is the drag coefficient of the vehicle.

The atmospheric density ρ is usually considered to be a function of instantaneous altitude and the quantities A_r , C_L , and C_D must be measured on the ground. In the measurement of A_r , C_L , and C_D , a vehicle-fixed coordinate system is used (denoted by x_V, y_V, z_V). For simplicity, it will be assumed that the instantaneous orientation of this vehicle-fixed coordinate system is defined so that the x_V -axis lies along \bar{a} , the z_V -axis defines the plane of the vehicle where the relative velocity vector \bar{v}_r would produce the maximum values for C_L and C_D for a given angle α between \bar{v}_r and \bar{a} , and the y_V -axis completes a right-handed coordinate system. This coordinate system, with \bar{u} and two possible locations for \bar{v}_r , is depicted in figure 6.

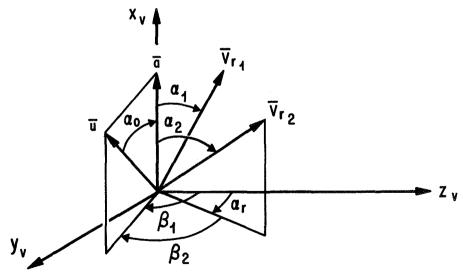


Figure 6. Coordinate System Used to Measure the Lift and Drag Coefficients

The reference area A_R will be taken to be the area of the (y_v, z_v) plane obscured by the vehicle if a sighting along the $x_{\mathbf{v}}$ axis is made at an infinite distance from the origin. If \bar{V}_r lies in the (x_V,z_V) -plane as depicted by \bar{V}_{r_1} in figure 6, then the lift coefficient \mathtt{C}_{L} and the drag coefficient \mathtt{C}_{D} can be measured to depend only on the instantaneous value of the angle α between \bar{a} and \bar{v}_r and the Mach number M of the vehicle. If \bar{V}_r is not in the (x_V, z_V) -plane as depicted by $ar{\mathtt{V}}_{\mathtt{r}_{2}}$, then $\mathtt{C}_{\mathtt{L}}$ and $\mathtt{C}_{\mathtt{D}}$ must also depend on the angle $lpha_{\mathtt{r}}$ as shown in figure 6. As mentioned previously, the orientation of u with respect to a vehicle-fixed coordinate system can be determined or measured before the vehicle is flown. Thus, the angles α_0 and β_1 can be determined using the angles measured in figure 1. The angles α_0 and β_1 are needed in relating the vehicle-fixed coordinate system to the original reference coordinate system so that the angles α and α_R can be computed and used to obtain corresponding values for C_{T_i} and C_{D_i} . Figure 6 shows that the following equation will determine α for either position of $\bar{\mathbf{v}}_{\mathbf{r}}$ (i.e., \bar{V}_{r_1} or \bar{V}_{r_2}).

$$\alpha = \arctan \left\{ \frac{\left[\frac{(\bar{a} \times \bar{v}_r) \times \bar{a}}{|(\bar{a} \times \bar{v}_r) \times \bar{a}|}\right] \cdot \bar{v}_r}{(\bar{v}_r \cdot \bar{a})} \right\} \quad (-\pi \le \alpha \le \pi). \quad (16)$$

To determine α_R , the angle β_2 shown in figure 6 must be determined. The following equation can be used to obtain β_2 :

$$\beta_2 = \arctan \left\{ \frac{\left[\bar{\mathbf{a}} \times (\bar{\mathbf{u}} \times \bar{\mathbf{a}})\right] \cdot (\bar{\mathbf{v}}_r \times \bar{\mathbf{a}})}{(\bar{\mathbf{u}} \times \bar{\mathbf{a}}) \cdot (\bar{\mathbf{v}}_r \times \bar{\mathbf{a}})} \right\} \quad (0 \le \beta_2 \le 2\pi). \tag{17}$$

Then $\alpha_{\mathbf{R}}$ is given by

$$\alpha_{R} = \beta_1 - \beta_2. \tag{18}$$

With α and α_R computed as shown in equations (16) and (18), values for C_L and C_D can be obtained. Thus, enough information is available to compute \bar{L} and \bar{D} as given in equations (14) and (15). This completes a general explanation of the equations of motion given by equation (1).

To re-emphasize the concepts discussed previously, an outline will now be given of the order of the computations to be performed to obtain a value for \ddot{x} (as given by equation (1)) at a particular instant of trajectory time. At a particular instant of trajectory time (t), the position vector (\ddot{x}) of the point mass (m) is known along with the velocity vector $\dot{\ddot{x}}$. Thus, the altitude (h) of the point mass can be computed as follows:

$$h = R - R_{o},$$
 (19)

where R = $\sqrt{\bar{x} \cdot \bar{x}}$ and R_o is the radius of the spherical central body. With a value of h as obtained from equation (19), atmospheric tables can be used to obtain corresponding values of pressure (P), density (ρ), and velocity of sound (V_S) . Since the gravitational constant of the central body (GM) is assumed known, the third term in equation (1) due to gravity can be computed immediately. To compute values for the first term in equation (1), equation (2) is used to obtain a value for F, since A_e , F_s , and P_o are known constants and P has been obtained as described. Also, m and $\bar{\mathbf{u}}$ are assumed to be known at each instant of trajectory time. The unit vector u may be known directly in terms of its three components, or it may be known in terms of the angles X_D and X_V , in which case equation (6) is used to compute u. Then, the first term in equation (1) can be computed. To compute values for the second term in equation (1), $\bar{\textbf{V}}_r$ must be computed by equation (9). The vector constant $\bar{\omega}$ needed in equation (9) and the wind function \overline{W} are assumed known. With a value for the vector V_r available, the following equation can be used to compute Mach number M:

$$M = \frac{\sqrt{\bar{V}_r \cdot \bar{V}_r}}{V_s} . \tag{20}$$

Also, equations (16) and (18) can be used to compute α and α_R if values of \bar{a} are available. The unit vector \bar{a} may be assumed to be known directly in terms of its components, or it can be specified in terms of x_p , x_y , α_o , and x_R as shown in equations (10) and (11). With values for α , α_R , and M obtained, a curve fit or table look-up can be used to

obtain values of C_L and C_D , which depend on α , $\alpha_{R,2}$ and M. Then equations (14) and (15) can be used to compute \bar{L} and \bar{D} since the quantities needed are now all available. Thus, the third term in equation (1) can be computed to complete the computation of equation (1).

The previous discussion shows how values of \bar{x} can be obtained at each instant of trajectory time when the control variables X_p , X_y , and X_R are known. Thus, numerical integration of equation (1) could be used to obtain a trajectory for prespecified control functions X_p , X_y , and X_R .

Also, optimization theory could be applied directly to the equations of motion (equation (1)) in its present form to determine the correct time histories for \bar{u} and \bar{a} , but the resulting computer program would be much too complicated to consider for guidance purposes.

For this reason, some simplifying assumptions and approximations to these differential equations will now be made that will result in a much more compact and efficient computer program for the application of optimization theory.

 Simplifications to General Three-Dimensional Equations of Motion with Atmospheric Effects

The original equations of motion (equation (1)) are completely accurate representations of the ascent phase of the shuttle vehicle's flight. For the vacuum phase of a shuttle vehicle's flight, an accurate representation is obtained by leaving out the term

$$\frac{\bar{L} + \bar{D}}{m}$$
,

and for the reentry phase, an accurate representation is obtained by leaving out the term

$$(F/m)$$
 \bar{u} .

The only simplifications to be made to equation (1) before optimization theory is applied are simplifications of the expressions for \bar{L} and \bar{D} which will be used in both the ascent and the reentry phases. Also, the expression $\bar{g}(\bar{x})$ accounting for oblateness effects will be neglected in all three phases, at least in illustrating the application of optimization theory to the equations of motion (equation (1)).

The first simplification to be made in the development of new expressions for \bar{L} and \bar{D} is to assume that $\bar{a}=\bar{u}$. For most vehicles, α_0 (the angle between \bar{u} and \bar{a} as shown in figure 2) is not very large because of the usual aerodynamic symmetry about the thrust vector direction. Thus, the assumption $\bar{a}=\bar{u}$ is not very restrictive as will be seen. With the assumption that $\bar{a}=\bar{u}$, the vehicle-fixed coordinate system shown in figure 6 does not have to be introduced. Instead \bar{V}_r can be pictured immediately in the prime coordinate system of figure 8.

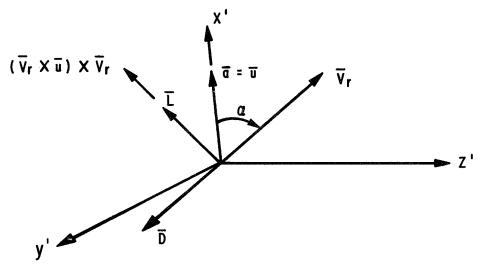


Figure 7. The Lift and Drag Forces with $\bar{a} = \bar{u}$

Then, the new expressions for \bar{L} and \bar{D} become

$$\bar{L} = \frac{1}{2} \rho A_{r} (\bar{v}_{r} \cdot \bar{v}_{r}) \left\{ C_{L} \left[\frac{(\bar{v}_{r} \times \bar{u}) \times \bar{v}_{r}}{|(\bar{v}_{r} \times \bar{u}) \times \bar{v}_{r}|} \right] \right\}$$
(21)

$$\bar{\mathbf{D}} = \frac{1}{2} \rho \ \mathbf{A}_{\mathbf{r}} (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}}) \left\{ \mathbf{C}_{\mathbf{D}} \left[-\frac{\bar{\mathbf{v}}_{\mathbf{r}}}{|\bar{\mathbf{v}}_{\mathbf{r}}|} \right] \right\}. \tag{22}$$

Now the coefficients \textbf{C}_L and \textbf{C}_D will depend only on Mach number and the angle α defined by the equation

$$\alpha = \arctan \left\{ \frac{\left[\frac{(\bar{\mathbf{v}}_{r} \times \bar{\mathbf{u}}) \times \bar{\mathbf{v}}_{r}}{|(\bar{\mathbf{v}}_{r} \times \bar{\mathbf{u}}) \times \bar{\mathbf{v}}_{r}|}\right] \cdot \bar{\mathbf{u}}}{\left[\frac{\bar{\mathbf{v}}_{r}}{|\bar{\mathbf{v}}_{r}|}\right] \cdot \bar{\mathbf{u}}} \right\}$$
 (defined for $-\pi < \alpha < \pi$). (23)

Also, the following additional approximating equations for \textbf{C}_{L} and \textbf{C}_{D} will be used.

$$C_{L} \approx C_{L_{\alpha}} \sin \alpha$$
 (24)

$$C_{D} \approx C_{A} + 2\eta C_{L\alpha}^{2} (1-\cos \alpha)$$
 (25)

where $C_{L_{Cl}}$, C_A , and η are all now considered to depend only on Mach number. These approximations have been found to closely represent most C_L and C_D tables in the range of Mach and alpha of interest and are used mainly because of their simplification of the optimization equations.

Substituting the above approximations into the expressions for \bar{L} and \bar{D} gives

$$\bar{\mathbf{L}} = \frac{1}{2} \rho \mathbf{A}_{\mathbf{r}} (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}}) \left\{ (\mathbf{C}_{\mathbf{L}\alpha} \sin \alpha) \left[\frac{(\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{u}}) \times \bar{\mathbf{v}}_{\mathbf{r}}}{|(\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{u}}) \times \bar{\mathbf{v}}_{\mathbf{r}}|} \right] \right\}$$
(26)

$$\bar{\mathbf{D}} = \frac{1}{2} \rho \mathbf{A}_{\mathbf{r}} (\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}}) \left\{ [\mathbf{C}_{\mathbf{A}} + 2\eta \ \mathbf{C}_{\mathbf{L}_{\mathbf{Q}}}^{2} (1 - \cos \alpha)] \left[\frac{-\bar{\mathbf{V}}_{\mathbf{r}}}{|\bar{\mathbf{V}}_{\mathbf{r}}|} \right] \right\}. \tag{27}$$

Notice that

$$|(\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{u}}) \times \bar{\mathbf{v}}_{\mathbf{r}}| = |\bar{\mathbf{v}}_{\mathbf{r}}|^2 \sin \alpha = (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}}) \sin \alpha$$

because α is the angle between $\overline{\mathtt{V}}_{\mathtt{r}}$ and $\overline{\mathtt{u}}$. Also,

$$\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{u}} = |\bar{\mathbf{v}}_{\mathbf{r}}| \cos \alpha$$
.

Thus,

$$\tilde{\mathbf{L}} = \frac{1}{2} \rho \, \mathbf{A}_{\mathbf{r}} \, \mathbf{C}_{\mathbf{L}_{\mathbf{C}}} \, [(\tilde{\mathbf{V}}_{\mathbf{r}} \times \tilde{\mathbf{u}}) \times \tilde{\mathbf{V}}_{\mathbf{r}}]$$
 (28)

$$\bar{\mathbf{D}} = -\frac{1}{2} \rho \mathbf{A}_{\mathbf{r}} [|\bar{\mathbf{v}}_{\mathbf{r}}| (\mathbf{C}_{\mathbf{A}} + 2\eta \mathbf{C}_{\mathbf{L}_{\alpha}}^{2}) - 2\eta \mathbf{C}_{\mathbf{L}_{\alpha}}^{2} (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{u}})] \bar{\mathbf{v}}_{\mathbf{r}}. \tag{29}$$

Now the following identity will be used:

$$(\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{u}}) \times \bar{\mathbf{v}}_{\mathbf{r}} = |\bar{\mathbf{v}}_{\mathbf{r}}|^2 \bar{\mathbf{u}} - (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{u}}) \bar{\mathbf{v}}_{\mathbf{r}}.$$

Then the final form of the lift and drag equations to be used is

$$\tilde{\mathbf{L}} = \frac{1}{2} \rho \mathbf{A}_{\mathbf{r}} \mathbf{C}_{\mathbf{L}_{\mathcal{O}}} [|\bar{\mathbf{v}}_{\mathbf{r}}|^{2} \bar{\mathbf{u}} - (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{u}}) \bar{\mathbf{v}}_{\mathbf{r}}]$$
(30)

$$\bar{\mathbf{D}} = -\frac{1}{2} \rho \mathbf{A}_{\mathbf{r}} [|\bar{\mathbf{v}}_{\mathbf{r}}| (\mathbf{C}_{\mathbf{A}} + 2\eta \ \mathbf{C}_{\mathbf{L}_{\mathbf{C}'}}^2) - 2\eta \ \mathbf{C}_{\mathbf{L}_{\mathbf{C}'}}^2 (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{u}})] \bar{\mathbf{v}}_{\mathbf{r}}.$$
(31)

These are the expressions for \bar{L} and \bar{D} that will be used in equation (1) for the application of optimization theory. At this point, it will be mentioned again that equation (1) can be integrated numerically to yield a trajectory (without any optimization considerations) if $\bar{a}=\bar{u}$ is known directly in terms of its components or if X_p and X_y are known and equation (6) is used to obtain \bar{u} . Appendix I is a computer program

listing and a sample printout which uses the above equations for \bar{L} and \bar{D} and assumes the following time history for $\bar{a}=\bar{u}$:

$$\bar{u} = \frac{\bar{u}_0 + \dot{\bar{u}}_0(t - t_0)}{|\bar{u}_0 + \dot{\bar{u}}_0(t - t_0)|}.$$
 (32)

The values, \bar{u}_0 , $\dot{\bar{u}}_0$, and the flight time, t_f , are parameters in this program which can be varied to satisfy specified end conditions and minimize desired quantities. In determining how to vary the parameters \bar{u}_0 and $\dot{\bar{u}}_0$ to satisfy the end conditions, variational differential equations for the matrices

$$\frac{\partial \bar{x}(t)}{\partial \bar{u}_{o}}$$
, $\frac{\partial \dot{\bar{x}}(t)}{\partial \bar{u}_{o}}$, $\frac{\partial \bar{x}(t)}{\partial \dot{\bar{u}}_{o}}$, and $\frac{\partial \dot{\bar{x}}(t)}{\partial \dot{\bar{u}}_{o}}$

were developed, as explained in reference 14, and an iterative algorithm constructed. The program is mentioned at this time so that the interested reader can examine the listing to see a sample set of data and how the atmospheric and aerodynamic quantities are determined for the numerical integration. Other references to this listing and further explanations of the technique will also be given in some of the following sections.

4. Alternate Determination of a and u

Often it is more desirable to determine \bar{a} and \bar{u} in terms of angle of attack α , bank angle β , β_r (to be defined), and α_o , mentioned previously, instead of using the inertial angles x_p , x_y , x_R , and α_o . How this can be done will be explained at this point before discussing the application of optimization theory to equation (1). To begin, a new coordinate system denoted by x", y", z" will be defined as shown in figure 8. Note that, in this coordinate system, the origin is at the point mass (m) and \bar{r} is the position vector of the point mass (i.e., $\bar{r} = \bar{x}$ in the reference coordinate system). As can be seen from figure 8, the \bar{V}_r vector is defined to lie along the z" axis, the \bar{V}_r x vector lies along the y" axis, and the $(\bar{V}_r \times \bar{r}) \times \bar{V}_r$ vector lies along the x" axis. Thus, the \bar{x} " coordinate system is transformed to the original x,y,z coordinate system as follows:

$$\bar{\mathbf{x}} = \left[\frac{(\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{r}}) \times \bar{\mathbf{v}}_{\mathbf{r}}}{|(\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{r}}) \times \bar{\mathbf{v}}_{\mathbf{r}}|}, \frac{\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{r}}}{|\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{r}}|}, \frac{\bar{\mathbf{v}}_{\mathbf{r}}}{|\bar{\mathbf{v}}_{\mathbf{r}}|} \right] \bar{\mathbf{x}}^{"} = [\mathbf{B}]\bar{\mathbf{x}}^{"}. (33)$$

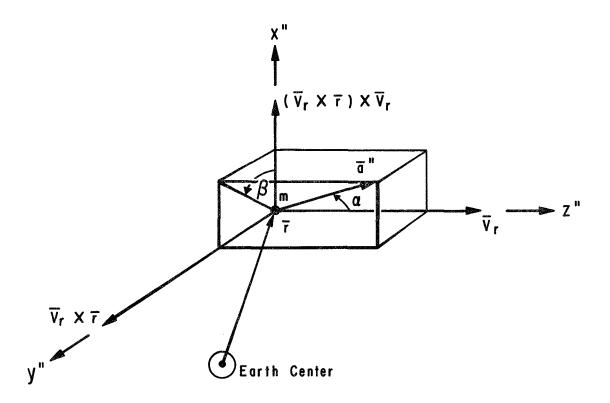


Figure 8. The Location of the Zero Lift Vector with an Angle of Attack and a Bank Angle

Then, as seen in figure 8,

$$\bar{a}'' = \begin{bmatrix} \sin \alpha & \cos \beta \\ \sin \alpha & \sin \beta \\ \cos \alpha \end{bmatrix}$$

and

$$\bar{\mathbf{a}} = \left[\frac{(\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{r}}) \times \bar{\mathbf{v}}_{\mathbf{r}}}{|(\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{r}}) \times \bar{\mathbf{v}}_{\mathbf{r}}|}, \frac{\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{r}}}{|\bar{\mathbf{v}}_{\mathbf{r}} \times \bar{\mathbf{r}}|}, \frac{\bar{\mathbf{v}}_{\mathbf{r}}}{|\bar{\mathbf{v}}_{\mathbf{r}}|} \right] \bar{\mathbf{a}}^{"} = [\mathbf{B}]\mathbf{a}^{"}.$$

The inverse transformation is given by

$$\tilde{\mathbf{a}}^{"} = [\mathbf{B}]^{\mathrm{T}} \tilde{\mathbf{a}}$$

and then

$$\alpha = \arctan \left[\frac{\sqrt{(a_1'')^2 + (a_2'')^2}}{a_3''} \right] \quad \text{(defined for } 0 < \alpha < \pi \text{)}$$
 (34)

$$\beta = \arctan \left[(a_2''/a_1'') \right] \quad (defined for $0 \le \beta \le 2\pi).$ (35)$$

When \bar{u} is not the same as \bar{a} and is allowed to be oriented with respect to \bar{a} and V_r , then another coordinate system must be defined (denoted by x''', y''', z'''). To visualize this orientation see figure 9.

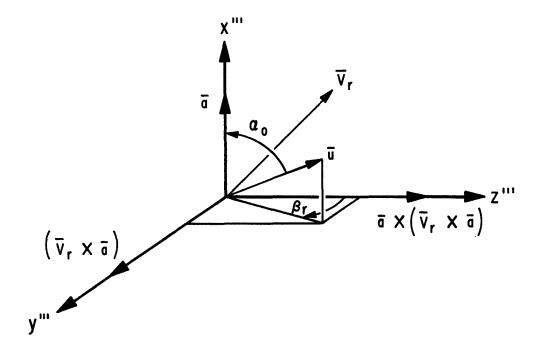


Figure 9. The Location of u with Respect to a

The transformation from a vector \vec{x}^{iii} in this coordinate system to the original \vec{x} coordinate system is obtained as follows:

$$\bar{x} = \left[\bar{a}, \frac{\bar{v}_r \times \bar{a}}{|\bar{v}_r \times \bar{a}|}, \frac{\bar{a} \times (\bar{v}_r \times \bar{a})}{|\bar{a} \times (\bar{v}_r \times \bar{a})|}\right] \bar{x}''' = [C]\bar{x}'''.$$
(36)

Thus,

$$\bar{\mathbf{u}} = [\mathbf{C}]\bar{\mathbf{u}}^{"}.$$

Therefore,

$$\bar{\mathbf{u}} = [C] \begin{bmatrix} \cos \alpha_{\mathbf{o}} \\ -\sin \alpha_{\mathbf{o}} & \sin \beta_{\mathbf{r}} \\ -\sin \alpha_{\mathbf{o}} & \cos \beta_{\mathbf{r}} \end{bmatrix}.$$

Then the inverse transformation is given by

$$\bar{\mathbf{u}}^{"} = [\mathbf{C}]^{\mathrm{T}} \bar{\mathbf{u}}$$

and thus

$$\alpha_{o} = \arctan \frac{\sqrt{(u_{2}^{"'})^{2} + (u_{3}^{"'})^{2}}}{u_{1}^{"'}} \quad (defined for 0 < \alpha_{o} < \pi)$$
 (37)

$$\beta_{r} = \arctan \left[u_{2}^{"'} / u_{3}^{"'} \right] \quad \text{(defined for } 0 \le \beta_{r} \le 2\pi \text{).}$$
 (38)

The preceding equations show how to compute \bar{a} and \bar{u} with the angles α , β , α_0 , and β_r or conversely how to compute α , β , α_0 , and β_r when the unit vectors \bar{a} and \bar{u} are given. If it is assumed that $\bar{a}=\bar{u}$, then the triple prime coordinate system does not have to be introduced, and only the angles α and β are needed to compute \bar{a} and thus \bar{u} . Conversely, α and β can be computed when $\bar{u}=\bar{a}$ is known or given.

In the next section, optimization theory will be applied to the equations of motion (equation (1)) with \bar{L} and \bar{D} given by the simplified expressions which resulted from assuming $\bar{a}=\bar{u}$. One of the results of the application of optimization theory will be a time history for \bar{u} , and thus \bar{a} that will produce an optimum trajectory to the desired destination. This time history ($\bar{u}=\bar{a}$ as a function of time) can be used to compute X_p and X_y or α and β as functions of time for guidance purposes.

C. Application of Optimization Theory to Equations of Motion

1. Equations of Motion

The simplified equations of motion discussed in the previous section will be used here to illustrate the application of optimization theory. These equations with the simplified \bar{L} and \bar{D} should adequately represent the motion of most space shuttle type of vehicles during atmospheric flight. If it is found that they are not adequate, the reader should remember that they are used here only to illustrate the approach, and whatever corrections are needed can be added to the equations without changing the philosophy of the approach.

The simplified equations for \bar{L} and \bar{D} can be substituted into equation (1) of the previous section to give the following form for the equations of motion:

$$\ddot{\bar{x}} = (F/m)\bar{u} - \frac{GM\bar{x}}{R^3} + g(\bar{x}) + (\rho A_r/2m) \left\{ C_{L_{\alpha}} [\bar{v}_r \cdot \bar{v}_r)\bar{u} - (\bar{v}_r \cdot \bar{u})\bar{v}_r \right\} - [(\bar{v}_r \cdot \bar{v}_r)^{1/2}(C_A + 2\eta C_{L_{\alpha}}^2) - 2\eta C_{L_{\alpha}}^2 (\bar{v}_r \cdot \bar{u})] \bar{v}_r \right\}.$$
(39)

In equation (39), F is given by equation (2) and m by equations (3) and (4). Typical values of the constants needed to use equations (2), (3), and (4) can be found in the computer program listing and sample

case printout of Appendix I. The constant GM needed to compute the second term of equation (39) and the form of the equations for g(\bar{x}) can also be found in Appendix I. The atmospheric subroutine shown in Appendix I shows how the atmospheric density ρ , the atmospheric pressure P, and the velocity of sound V_s are obtained as functions of altitude for use in equation (39). With a value for V_s , equation (20) can be used to compute the Mach number. Then the aerodynamic subroutine of Appendix I shows how values of $C_{L_{\alpha}}$, $C_{\underline{A}}$, and η are obtained as functions of Mach number. If it is noted that \bar{V}_r is given by equation (9) and that the instantaneous radius of the oblate earth's surface is determined in the differential equation subroutine of Appendix I, then the computation of all the terms in equation (39) has been explained.

A transition to state vector notation will be made to facilitate the explanation of the application of optimization theory to equation (39). To do this, let

$$X = \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \\ x_5 \\ x_6 \\ x_7 \end{bmatrix} = \begin{bmatrix} x \\ y \\ z \\ \dot{x} \\ \dot{y} \\ \dot{z} \\ m \end{bmatrix}. \tag{40}$$

Then

$$\dot{X} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \\ \dot{x}_5 \\ \dot{x}_6 \\ \dot{x}_7 \end{bmatrix} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{y} \\ \dot{z} \\ \dot{x}_6 \\ \dot{x}_7 \end{bmatrix} = \begin{bmatrix} f_1(x_1, x_2, \dots, x_7) \\ f_2(x_1, x_2, \dots, x_7) \\ \vdots \\ \vdots \\ f_7(x_1, x_2, \dots, x_7) \end{bmatrix}$$
(41)

where

$$f_{1} = x_{4}$$

$$f_{2} = x_{5}$$

$$f_{3} = x_{6}$$

$$\begin{bmatrix} f_{4} \\ f_{5} \\ f_{6} \end{bmatrix} = (F/x_{7})\bar{u} - \frac{GM \begin{bmatrix} x_{1} \\ x_{2} \\ x_{3} \end{bmatrix}}{(x_{1}^{2} + x_{2}^{2} + x_{3}^{2})^{3/2}} + \bar{g}(x_{1}, x_{2}, x_{3})$$

$$+ \frac{\rho A_{r}}{2x_{7}} \left\{ c_{L_{\alpha}} \left[(\bar{v}_{r} \cdot \bar{v}_{r})\bar{u} - (\bar{v}_{r} \cdot \bar{u})\bar{v}_{r} \right] - \left[(\bar{v}_{r} \cdot \bar{v}_{r})^{1/2} (c_{A} + 2\eta \ c_{L_{\alpha}}^{2}) - 2\eta \ c_{L_{\alpha}}^{2} (\bar{v}_{r} \cdot \bar{u}) \right] \bar{v}_{r} \right\}$$

$$(42)$$

 $f_7 = \dot{m}$ (a constant developed in equation (3)).

Note that, in the previous expressions for f_4 , f_5 , and f_6 ; F depends on x_1, x_2, x_3 ; ρ depends on x_1, x_2, x_3 ; \bar{V}_r depends on x_1, x_2, x_3, x_4 , x_5, x_6 ; and the aerodynamic coefficients C_{LQ} , C_A , and η all depend on $x_1, x_2, x_3, x_4, x_5, x_6$. This dependence can also be seen by referring to the differential equation subroutine of Appendix I. The preceding transition to state vector notation now allows the equations of motion to be written in standard first order form which is usually seen when optimization theory is developed. That is,

$$\dot{X} = f(X, \bar{u}), \tag{43}$$

where \dot{X} , f, and X are all vectors of dimension 7, and \bar{u} is a vector of dimension 3.

Before applying optimization theory to this system of equations, the optimization criteria and the boundary conditions must be discussed. Such a discussion appears in the next two sections.

2. Definition of Optimization Criteria

The optimization criteria selected for discussion in this section were chosen mainly for illustration, and some approximations were made to keep the equations as simple as possible while maintaining as much physical realism as possible. Again it must be emphasized that, if this particular selection of an optimization criteria is found to be unsatisfactory, then whatever criteria that can be selected which are satisfactory can be used without changing the basic philosophy of the MASCOT technique.

The selected criteria are given as:

$$x_8(t_f) = k_1 x_7(t_f) + k_2 \left[\int_{t_0}^{t_f} \dot{Q} dt \right] + k_3 \left[\int_{t_0}^{t_f} D^2 dt \right].$$
 (44)

That is, $x_8(t_f)$ is to be minimized where the constants or weighting factors k_1 , k_2 , and k_3 can be selected to achieve different ratios of values among the three terms in the expression for $x_8(t_f)$. For example, in reentry, k_1 could be zero with k_2 and k_3 equal to .5, or in ascent, k_1 could be minus one and k_2 and k_3 zero. In equation (44) \dot{Q} , the convective heating rate per unit area of the vehicle, is given by

$$\dot{Q} = \frac{e}{\sqrt{\sigma}} \rho^{1/2} \left| \bar{V}_{\mathbf{r}} \right|^3 \tag{45}$$

where e is a constant and σ is the radius of curvature of the vehicle's nose. Values for these constants are given in Appendix I. Also, in equation (44)

$$D^2 \approx \frac{\left|\overline{L}\right|^2 + \left|\overline{D}\right|^2}{m^2}.$$

The following steps are needed to derive the exact expression for D^2 . From the simplified equation for \bar{L} and \bar{D} (equations (30) and (31)), it can be seen that

$$\left|\bar{\mathbf{L}}\right|^{2} = \bar{\mathbf{L}} \cdot \bar{\mathbf{L}} = \left(\frac{1}{2} \rho \, \mathbf{A_{r}} \, \mathbf{C_{L_{r}}}\right)^{2} \left[\left(\bar{\mathbf{V}_{r}} \cdot \bar{\mathbf{V}_{r}}\right)^{2} - \left(\bar{\mathbf{V}_{r}} \cdot \bar{\mathbf{V}_{r}}\right) \left(\bar{\mathbf{V}_{r}} \cdot \bar{\mathbf{u}}\right)^{2}\right] \tag{46}$$

$$\begin{split} |\bar{\mathbf{D}}|^{2} &= \bar{\mathbf{D}} \cdot \bar{\mathbf{D}} = (\frac{1}{2} \rho \mathbf{A}_{\mathbf{r}})^{2} [(\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}})^{1/2} (\mathbf{C}_{\mathbf{A}} + 2 \eta \ \mathbf{C}_{\mathbf{L}_{\alpha}}^{2}) \\ &- 2 \eta \ \mathbf{C}_{\mathbf{L}_{\alpha}}^{2} (\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{u}})]^{2} (\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}}) \\ &= (\frac{1}{2} \rho \ \mathbf{A}_{\mathbf{r}})^{2} [(\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}}) (\mathbf{C}_{\mathbf{A}} + 2 \eta \ \mathbf{C}_{\mathbf{L}_{\alpha}}^{2})^{2} \\ &- 4 \eta \ \mathbf{C}_{\mathbf{L}_{\alpha}}^{2} (\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}})^{1/2} (\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{u}}) (\mathbf{C}_{\mathbf{A}} + 2 \eta \ \mathbf{C}_{\mathbf{L}_{\alpha}}^{2}) \\ &+ 4 (\eta \ \mathbf{C}_{\mathbf{L}_{\alpha}}^{2})^{2} (\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{u}})^{2} [(\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}})^{2}] (\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}}). \end{split}$$

Now note that $(\overline{\mathbf{V}}_{\mathbf{r}} \cdot \overline{\mathbf{u}}) = |\overline{\mathbf{V}}_{\mathbf{r}}|\cos \alpha$ so that

$$(\vec{v}_r \cdot \vec{u})^2 = (\vec{v}_r \cdot \vec{v}_r) \cos^2 \alpha = (\vec{v}_r \cdot \vec{v}_r) (1 - \sin^2 \alpha). \tag{48}$$

In equation (48), $\sin^2\alpha$ will be approximated by 2(1 - $\cos \alpha$) to give

$$(\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{u}})^{2} = (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}})[1 - 2(1 - \cos \alpha)]$$

$$= (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}})[2 \cos \alpha - 1]$$

$$= 2(\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}})^{1/2}(\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{u}}) - (\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}}).$$
(49)

The substitution of the final form of equation (49) into equations (46) and (47) gives

$$\left|\bar{\mathbf{L}}\right|^{2} \approx \left(\frac{1}{2} \rho \, \mathbf{A}_{\mathbf{r}}\right)^{2} \left(2C_{\mathbf{L}_{\alpha}}^{2}\right) \left[\left(\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}}\right)^{2} - \left(\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{V}}_{\mathbf{r}}\right)^{3/2} \left(\bar{\mathbf{V}}_{\mathbf{r}} \cdot \bar{\mathbf{u}}\right)\right] \tag{50}$$

$$\begin{split} \left|\bar{\mathbf{D}}\right|^{2} \approx \left(\frac{1}{2} \rho \mathbf{A}_{r}\right)^{2} \left[\left(\bar{\mathbf{V}}_{r} \cdot \bar{\mathbf{V}}_{r}\right) \left(\mathbf{C}_{A}^{2} + 4\eta \mathbf{C}_{A} \mathbf{C}_{L_{\alpha}}^{2}\right) \right. \\ \left. - 4\eta \mathbf{C}_{A} \mathbf{C}_{L_{\alpha}}^{2} \left(\bar{\mathbf{V}}_{r} \cdot \bar{\mathbf{u}}\right) \left(\bar{\mathbf{V}}_{r} \cdot \bar{\mathbf{V}}_{r}\right)^{1/2} \right] \left(\bar{\mathbf{V}}_{r} \cdot \bar{\mathbf{V}}_{r}\right). \end{split} \tag{51}$$

Adding equations (50) and (51) and dividing by m^2 gives the final form to be used for D^2 . That is,

$$D^{2} = (\rho A_{r}/2m)^{2} [(\bar{V}_{r} \cdot \bar{V}_{r})^{2} (C_{A}^{2} + 4\eta C_{A} C_{L_{\alpha}}^{2} + 2C_{L_{\alpha}}^{2})$$

$$- 2(\bar{V}_{r} \cdot \bar{u})(\bar{V}_{r} \cdot \bar{V}_{r})^{3/2} (C_{L_{\alpha}}^{2} + 2\eta C_{A} C_{L_{\alpha}}^{2})].$$
(52)

With the preceding explanation of \dot{Q} and D^2 and using equation (44), it can be seen that

$$\dot{x}_8 = k_1 \dot{x}_7 + k_2 \dot{Q} + k_3 D^2 = f_8(x_1, x_2, \dots, x_7). \tag{53}$$

Thus, $x_8(t)$ as defined by equation (53) is a new variable which is added to the seven variables of the preceding section so that $x_8(t_f)$ is the quantity selected to be minimized at the final time with $x_8(t_0) = k_1 m_0$.

 Definition and Explanation of Some Example Boundary or Mission Conditions

The previous two sections have put the illustrative problem being solved in this report in the form:

(a) $X(t_0)$ and t_0 are given

(b)
$$X(t)$$
 is defined by $\dot{X}(t) = f[X(t), \bar{u}(t)]$ where $t_0 \le t \le t_f$ (54)

(c) $x_8(t_{\mbox{\scriptsize f}})$ is to be minimized by the choice of $\bar{u}(t).$

In equation (54), X is now an eight-dimensional vector and $\bar{\bf u}$ is a three-dimensional vector. The only thing missing from equation (54) is some additional constraints which are usually placed on some of the values of $x_1(t_f)$, $x_2(t_f)$, ..., $x_7(t_f)$. These functional constraints are called the boundary (or end or mission) conditions.

The first set of boundary conditions to be discussed is an example set of reentry boundary conditions. For example, on a reentry trajectory a desired value for the magnitude of the radius vector, Mach number, the path angle, down range, and cross range could be specified for the end of the trajectory. In functional form the preceding specifications result in five equations as follows:

$$G_1 = \frac{x_1^2 + x_2^2 + x_3^2}{R_c^2} - 1 = 0$$
 (54)

$$G_2 = \frac{\overline{V}_r \cdot \overline{V}_r}{V_s^2 M_c^2} - 1 = 0 \tag{55}$$

$$G_3 = \frac{x_1 x_4 + x_2 x_5 + x_3 x_6}{R_c \sqrt{x_4^2 + x_5^2 + x_6^2}} - \cos \vartheta_c = 0$$
 (56)

$$G_{4} = \left\{ \begin{bmatrix} x_{1} \\ x_{2} \\ x_{3} \end{bmatrix} \cdot \begin{bmatrix} \frac{\bar{x}_{0}}{|\bar{x}_{0}|} \tan \varphi_{DR} - \frac{\bar{x}_{0} \times (\dot{\bar{x}}_{0} \times \bar{x}_{0})}{|\bar{x}_{0} \times (\dot{\bar{x}}_{0} \times \bar{x}_{0})|} \end{bmatrix} \right\} / R_{c} = 0$$
(57)

$$G_{5} = \left\{ \begin{bmatrix} x_{1} \\ x_{2} \\ x_{3} \end{bmatrix} \cdot \begin{bmatrix} \frac{\dot{x}_{0} \times \bar{x}_{0}}{|\dot{x}_{0} \times \bar{x}_{0}|} \end{bmatrix} \right\} / R_{c} - \sin \varphi_{CR} = 0.$$
 (58)

In all of these equations, the values of x_1 , x_2 , x_3 , x_4 , x_5 , and x_6 are used at the final time. In equation (54), R_c is the desired value of the magnitude of the radius vector at the final time, and when $G_1 = 0$, it can be seen that $x_1^2 + x_2^2 + x_3^2$ will be equal to R_c^2 . Similarly, in equation (55), M_c is the desired value of Mach number at the final time; in equation (56), ϑ_c is the desired value of the angle between the inertial position vector and the inertial velocity vector (path angle); in equation (57), ϕ_{DR} is the desired value of the down range angle; and in equation (58), ϕ_{CR} is the desired value of the cross range angle. In order to better understand equations (57) and (58), figure 10 is used.

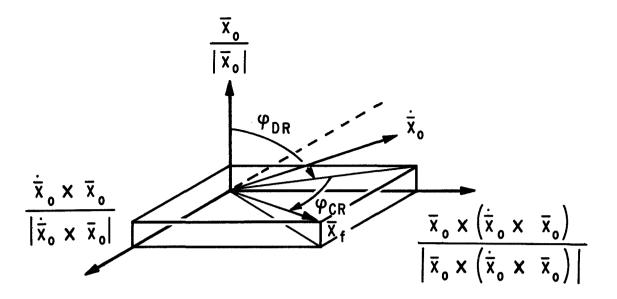


Figure 10. A Definition of the Down Range and Cross Range Angles

In this figure a coordinate system is defined using the position and velocity vector at the initial time $(\bar{\mathbf{x}}_{o} \text{ and } \dot{\bar{\mathbf{x}}}_{o}),$ and then the angles ϕ_{DR} and ϕ_{CR} are used to locate the final position vector $\bar{\mathbf{x}}_{f}$ with respect to the coordinate system defined by $\bar{\mathbf{x}}_{o}$ and $\dot{\bar{\mathbf{x}}}_{o}.$ The figure shows that

$$\tan \varphi_{DR} = \frac{\bar{x}_{f} \cdot \left[\frac{\bar{x}_{o} \times (\dot{\bar{x}}_{o} \times \bar{x}_{o})}{|\bar{x}_{o} \times (\dot{\bar{x}}_{o} \times \bar{x}_{o})|} \right]}{\bar{x}_{f} \cdot \left[\frac{\bar{x}_{o}}{|\bar{x}_{o}|} \right]}$$
(59)

$$\sin \varphi_{CR} = \frac{\vec{x}_{f} \cdot \left[\frac{\dot{\vec{x}}_{o} \times \vec{x}_{o}}{|\dot{\vec{x}}_{o} \times \vec{x}_{o}|} \right]}{|\vec{x}_{f}|}.$$
 (60)

Since $|\bar{x}_f|$ is to be equal to R_c , it can be seen that equations (57) and (58) follow from equations (59) and (60).

The computer program for computing equations (54), (55), (56), (57), and (58) is called subroutine BOUND in Appendix I. Notice that all of the equations are normalized so that $G_1^2 + G_2^2 + G_3^2 + G_4^2 + G_5^2$ will have a magnitude near the value of one. The preceding sum of squares is usually used as an error check to determine when the boundary conditions are satisfied. That is, it must be less than some tolerance (for example, .5 x 10^{-10}).

With the preceding definition of an example set of boundary conditions, the complete trajectory optimization problem being solved in this paper can now be stated in functional notation. That is,

(a) $X(t_0)$ and t_0 are given

(b)
$$X(t)$$
 is defined by $\dot{X}(t) = f[X(t), \bar{u}(t)]$ where $t_0 \le t \le t_f$ (61)

(c) $x_8(t_f)$ is to be minimized and $G[X_f(t_f), t_f]$ is to be made equal to zero by the choice of $\bar{u}(t)$.

Appendix I is a computer program listing which solves the problem stated in equation (61) with the assumption that

$$\bar{u}(t) = \frac{\bar{u}_{o} + \dot{\bar{u}}_{o}(t - t_{o})}{|\bar{u}_{o} + \dot{\bar{u}}_{o}(t - t_{o})|}$$

where the vector constants $\bar{\mathbf{u}}_0$ and $\dot{\bar{\mathbf{u}}}_0$ are assumed to be unknown parameters which the program must select along with \mathbf{t}_f to satisfy condition (c) of equation (61). This approach to trajectory optimization is called parameter optimization particularly when the time interval \mathbf{t}_0 to \mathbf{t}_f is broken into n segments (at the times $\mathbf{t}_1,\mathbf{t}_2,\ldots,\mathbf{t}_n$) and $\mathbf{u}(\mathbf{t})$ is defined by

$$u(t) = \frac{\bar{u}_{0} + \dot{\bar{u}}_{0}(t - t_{0})}{|\bar{u}_{0} + \dot{\bar{u}}_{0}(t - t_{0})|} \qquad \text{for } t_{0} \leq t \leq t_{1}$$

$$u(t) = \frac{\bar{u}(t_{1}) + \dot{\bar{u}}_{1}(t - t_{1})}{|\bar{u}(t_{1}) + \dot{\bar{u}}_{1}(t - t_{1})|} \qquad \text{for } t_{1} \leq t \leq t_{2}$$

$$\vdots$$

$$u(t) = \frac{\bar{u}(t_{n}) + \dot{\bar{u}}_{n}(t - t_{n})}{|\bar{u}(t_{n}) + \dot{\bar{u}}_{n}(t - t_{n})|} \qquad \text{for } t_{n} \leq t \leq t_{f}.$$

$$(62)$$

Then the parameters the program must select to satisfy condition (c) of equation (61) are $\bar{\mathbf{u}}_0$, $\dot{\mathbf{u}}_0$, $\dot{\mathbf{u}}_1$, $\dot{\mathbf{u}}_2$, ..., $\dot{\mathbf{u}}_n$, and \mathbf{t}_f . As stated previously, the computer program listed in Appendix I and the sample case are a solution of the problem stated by equation (61) using only the parameters $\bar{\mathbf{u}}_0$, $\dot{\mathbf{u}}_0$, and \mathbf{t}_f with the boundary conditions given by equations (54), (55), (56), (57), and (58). Before explaining in more detail how this computer program works, a set of example boundary conditions for a rendezvous mission and an ascent mission will be given, and it will be noted here that the computer program of Appendix I has been used to solve these problems when the subroutines BOUND and PBOUND are replaced with the appropriate new subroutines for ascent and rendezvous.

For an ascent mission, the magnitude of the radius vector, the magnitude of the velocity vector, the angle between the radius vector and the velocity vector, and the angle between the plane containing the position and velocity vector and the equatorial plane could be specified. This yields the following set of boundary conditions (note that all values of x_1 , x_2 , x_3 , x_4 , x_5 , and x_6 are used at t_f):

$$G_1 = \frac{x_1^2 + x_2^2 + x_3^2}{R_c^2} - 1 = 0$$
 (63)

$$G_2 = \frac{x_4^2 + x_5^2 + x_6^2}{V_c^2} - 1 = 0$$
 (64)

$$G_3 = \frac{x_1 x_4 + x_2 x_5 + x_3 x_6}{R_c V_c} - \cos \vartheta_c = 0$$
 (65)

$$G_{4} = \frac{\left\{ \begin{bmatrix} x_{1} \\ x_{2} \\ x_{3} \end{bmatrix} \times \begin{bmatrix} x_{4} \\ x_{5} \\ x_{6} \end{bmatrix} \right\} \cdot \bar{A}}{R_{c} V_{c}} - \sin \varphi_{c} \cos i_{c} = 0.$$
 (66)

In equation (63), R_c is the specified radius vector magnitude; in equation (64), V_c is the specified velocity vector magnitude; in equation (65), ϑ_c is the specified angle between the radius vector and the velocity vector; and in equation (66), i_c is the specified inclination of the

flight plane to the equatorial plane. Also, in equation (66), \bar{A} is a unit vector perpendicular to the equatorial plane. Figure 11 shows \bar{A} and a plumbline coordinate system oriented, with respect to the equatorial coordinate system, by the azimuth Az and the geodetic latitude ϕ_d of some point such as the launch site.

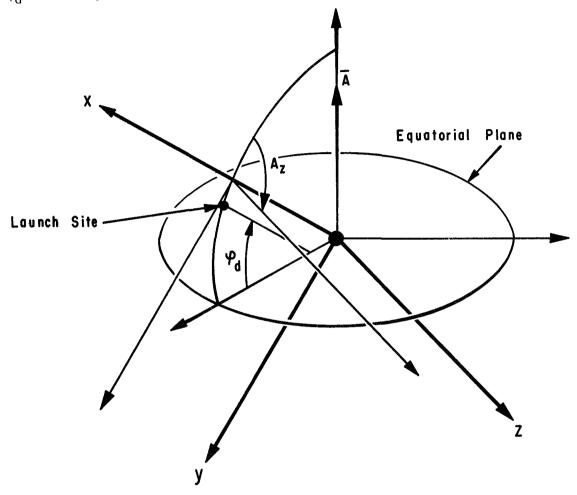


Figure 11. The Orientation of the Plumbline Coordinate System and the Unit North Vector \tilde{A}

Figure 11 shows that

$$\bar{\mathbf{A}} = \begin{bmatrix} \sin \phi_{d} \\ \cos \phi_{d} & \sin A_{z} \\ \cos \phi_{d} & \cos A_{z} \end{bmatrix}. \tag{67}$$

This completes the explanation of an example set of ascent boundary conditions.

For a rendezvous mission, let the coordinates of the target vehicle (in the same coordinate system as the pursuit vehicle) be given by the six-dimensional vector Y, where

$$Y = \begin{bmatrix} x \\ y \\ y \\ z \\ \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \begin{bmatrix} y_1 \\ y_2 \\ y_3 \\ y_4 \\ y_5 \\ y_6 \end{bmatrix}. \tag{68}$$

Then the boundary conditions can be written in the form:

$$G_1 = \frac{x_1}{y_1} - 1 = 0 \tag{69}$$

$$G_2 = \frac{x_2}{y_2} - 1 = 0 \tag{70}$$

$$G_3 = \frac{x_3}{y_3} - 1 = 0 \tag{71}$$

$$G_4 = \frac{x_4}{y_4} - 1 = 0 \tag{72}$$

$$G_5 = \frac{x_5}{y_5} - 1 = 0 \tag{73}$$

$$G_6 = \frac{x_6}{y_6} - 1 = 0. (74)$$

Note that in the above equations the values of x_1 , x_2 , x_3 , x_4 , x_5 , and x_6 are all taken at the final time and the values of y_1, y_2, \ldots, y_6 depend only on the final time so that equations (69), (70), ..., (74) form a set of boundary conditions in the form $G[X(t_f), t_f] = 0$ where G is a six-dimensional vector.

The preceding discussion completes the explanation of all three sets of boundary conditions. Now the operation of the computer program in Appendix I will be explained in more detail. The starting point will be the problem statement of equation (61) with the five-dimensional

 $G[X(t_f), t_f]$ vector given by equations (54), (55), (56), (57), and (58). As stated before, $\bar{\mathbf{u}}(t)$ is assumed to have the form

$$\bar{u}(t) = \frac{\bar{u}_{o} + \dot{\bar{u}}_{o}(t - t_{o})}{|\bar{u}_{o} + \dot{\bar{u}}_{o}(t - t_{o})|}$$

and the parameters \bar{u}_0 and $\dot{\bar{u}}_0$ (appearing in the $\bar{u}(t)$ expression) and t_f are used to satisfy condition (c) of equation (61). With the preceding form for $\bar{u}(t)$ and the fixed initial conditions of condition (a) in equation (61), it can be stated that $X(t_f)$ depends only on α , β , \bar{u}_0 , and t_f , where α and β are shown in figure 8, and define a unit vector for \bar{u}_0 as shown in the explanation following equation (33). That is.

$$\bar{\mathbf{u}}_{o} = (\sin \alpha \cos \beta) \left[\frac{(\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}) \times \bar{\mathbf{v}}_{r_{o}}}{\left| (\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}) \times \bar{\mathbf{v}}_{r_{o}} \right|} \right] + \sin \alpha \sin \beta \left[\frac{\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}}{\left| \bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o} \right|} \right]$$

$$+\cos\alpha\left[\frac{\bar{\mathbf{v}}_{\mathbf{r_0}}}{|\bar{\mathbf{v}}_{\mathbf{r_0}}|}\right]. \tag{75}$$

It might also seem that $X(t_f)$ should depend on the magnitude of \bar{u}_0 , but the definition of $\bar{u}(t)$ as a unit vector tends to eliminate this possibility because the magnitude of \bar{u}_0 must also be considered. That is, any arbitrary initial magnitude of \bar{u}_0 will produce the same $X(t_f)$ that an initial magnitude of \bar{u}_0 equal to one would produce, when α and β are kept the same and the magnitude of \bar{u}_0 is adjusted with the ratio of the two different \bar{u}_0 magnitudes.

. Now it can be stated that $G[X(t_f), t_f]$ and $x_8(t_f)$ depend on α , β , \bar{u}_0 , and t_f . Thus, two new vectors (F and z) can now be defined. That is,

$$F(z) = F(\alpha, \beta, \dot{\bar{u}}_0, t_f) = \begin{bmatrix} G[X(t_f), t_f] \\ W_1 x_8(t_f) \end{bmatrix}$$
(76)

where

$$Z = \begin{bmatrix} \alpha \\ \beta \\ \dot{u}_{o} \\ t_{f} \end{bmatrix}.$$

In equation (76), notice that F is a six-dimensional vector and z is a six-dimensional vector. The fact that F and z are of the same dimension is somewhat coincidental, since, for the following development, it is required only that the dimension of z be greater than or equal to the dimension of F. Note also the arbitrary weighting factor W_1 whose use will be explained later.

The preceding discussion allows condition (c) of equation (61) to be stated in the following form: Determine the parameters α , β , $\bar{\mathbf{u}}$, and \mathbf{t}_f to minimize \mathbf{F}^T F with a choice of the weighting factor \mathbf{W}_1 which allows \mathbf{G}^T G to be zero. Note that \mathbf{F}^T means F transpose so that \mathbf{F}^T F is a scalar, and similarly for \mathbf{G}^T G. To determine the vector of unknown parameters z, which minimizes \mathbf{F}^T F, a Taylor series expansion of F about an arbitrarily guessed vector \mathbf{z}^* is made. That is,

$$F(z) = F(z^*) + (\partial F/\partial z)_{\dot{x}}(z - z^*) + \dots$$
 (77)

The notation $(\partial F/\partial z)_*$ means the matrix of partial derivatives of the vector F with respect to the vector z evaluated at the star point. Its determination will be explained later. If $(\partial F/\partial z)_*$ in equation (77) is not zero, then a vector z can be determined such that $F(z) = KF(z^*)$ where K is a scalar such that $0 \le K \le 1$. Also, if all the terms of order greater than one are neglected in equation (77), then the difference in this linear approximation to F(z) and $KF(z^*)$ will depend on z. That is,

$$\epsilon(z) = F(z) - KF(z^*)$$

$$= (1 - K)F(z^*) + (\partial F/\partial z)_*(z - z^*).$$
(78)

Equation (77) shows that $\epsilon^T(z)\epsilon(z)$ is a minimum when the vector z satisfies the following equation:

$$(\partial F/\partial z)_{+}^{T} (\partial F/\partial z)_{+} (z - z^{*}) = -(1 - K)^{2} (\partial F/\partial z)_{+}^{T} F(z^{*}).$$
 (79)

Notice that, if the function F(z) satisfies appropriate continuity conditions, then a value of K close enough to one can be chosen so that the value of z obtained from equation (79) will produce a value of F(z), using equation (77), that will be equal to $KF(z^*)$ within any desired degree of accuracy. The computer program of Appendix I uses equation (79) and some logic for choosing a sequence of W_1 's and a sequence of K's to determine a vector z which minimizes F(z). Since the program listing is self-explanatory, an explanation of the logic is not included here. The only other aspect of the listing in Appendix I to be explained is the determination of $(\partial F/\partial z_*)$ which appears in equations (77), (78), and (79).

Since the vector F depends on $X(t_f)$ and t_f in its original form, $(\partial F/\partial z)_*$ is obtained using the chain rule. That is,

$$(\partial F/\partial z) = \frac{F[X(t_f), t_f]}{\partial \alpha, \beta, \dot{\bar{u}}_o, t_f} = \frac{F[X(t_f), t_f]}{X(t_f)} \left(\frac{\partial X(t_f)}{\partial z}\right) + \frac{\partial F[X(t_f), t_f]}{\partial t_f} \left(\frac{\partial t_f}{\partial z}\right).$$
(80)

On the right-hand side of equation (80), it can be seen that

$$\frac{\partial F[X(t_f), t_f]}{\partial X(t_f)} \quad \text{and} \quad \frac{\partial F[X(t_f), t_f]}{\partial t_f}$$

are obtained by explicit partial differentiation of the expression for $F[X(t_f),t_f]$ with respect to the variables $X(t_f)$ and t_f . Also, to further explain the other two terms on the far right-hand side of equation (80), the following definitions are repeated:

$$\frac{\partial t_{\mathbf{f}}}{\partial \mathbf{z}} = \begin{bmatrix} \frac{\partial t_{\mathbf{f}}}{\partial \alpha} \\ \frac{\partial t_{\mathbf{f}}}{\partial \beta} \\ \frac{\partial t_{\mathbf{f}}}{\partial \dot{\mathbf{z}}} \\ \frac{\partial t$$

and

$$\frac{\partial X(t_f)}{\partial z} = \left[\frac{\partial X(t_f)}{\partial \alpha}, \frac{\partial X(t_f)}{\partial \beta}, \frac{\partial X(t_f)}{\partial \dot{\bar{u}}_0}, \dot{X}(t_f) \right]. \tag{82}$$

In equation (82), the chain rule is again applied to the first two columns of the matrix for $\partial X(t_f)/\partial z$ to give

$$\frac{\partial X(t_f)}{\partial \alpha} = \frac{\partial X(t_f)}{\partial \bar{u}_o} \left(\partial \bar{u}_o / \partial \alpha\right) + \frac{\partial X(t_f)}{\partial \dot{u}_o} \left(\partial \dot{\bar{u}}_o / \partial \alpha\right) \tag{83}$$

and

$$\frac{\partial X(t_{f})}{\partial \beta} = \frac{\partial X(t_{f})}{\partial \bar{u}_{o}} (\partial \bar{u}_{o}/\partial \beta) + \frac{\partial X(t_{f})}{\partial \dot{\bar{u}}_{o}} (\partial \dot{\bar{u}}_{o}/\partial \beta). \tag{84}$$

Since $\dot{\bar{u}}_0$, α , and β are assumed to be independent parameters, $\partial \dot{\bar{u}}_0/\partial \alpha$ and $\partial \dot{\bar{u}}_0/\partial \beta$ are zero. Equation (75) gives the relation between α , β , and \bar{u}_0 so that

$$\frac{\partial \bar{\mathbf{u}}_{o}}{\partial \alpha} = \cos \alpha \left\{ \cos \beta \left[\frac{(\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}) \times \bar{\mathbf{v}}_{r_{o}}}{|(\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}) \times \bar{\mathbf{v}}_{r_{o}}|} \right] + \sin \beta \left[\frac{\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}}{|\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}|} \right] \right\}$$

$$- \sin \alpha \left[\frac{\bar{\mathbf{v}}_{r_{o}}}{|\bar{\mathbf{v}}_{r_{o}}|} \right]$$
(85)

and

$$\frac{\partial \bar{\mathbf{u}}_{o}}{\partial \beta} = \sin \alpha \left\{ \cos \beta \left[\frac{\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}}{|\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o}|} \right] - \sin \beta \left[\frac{\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o} \times \bar{\mathbf{v}}_{r_{o}}}{|\bar{\mathbf{v}}_{r_{o}} \times \bar{\mathbf{x}}_{o} \times \bar{\mathbf{v}}_{r_{o}}|} \right] \right\}. \quad (86)$$

Now the only undetermined matrices needed for $\partial F/\partial z$, as given by equation (80), are the matrices $\partial X(t_f)/\partial \bar{u}_0$ and $\partial X(t_f)/\partial \bar{u}_0$ which appear in equations (82), (83), and (84). These matrices must be determined by numerical integration of the variational equations. Equation (61) shows that $X(t_0)$ and t_0 are fixed and $\dot{X} = f(X,u)$. Thus,

$$\frac{\partial X(t_0)}{\partial \bar{u}_0} = 0 \tag{87}$$

$$\frac{\partial X(t_0)}{\partial \dot{t}_0(t_0)} = 0 \tag{88}$$

and

$$\frac{\mathrm{d}}{\mathrm{d}t} \left[\frac{\partial \mathbf{X}(t)}{\partial \bar{\mathbf{u}}_{0}, \dot{\bar{\mathbf{u}}}_{0}} \right] = \left[\frac{\partial \mathbf{f}(\mathbf{X}, \bar{\mathbf{u}})}{\partial \bar{\mathbf{u}}_{0}, \dot{\bar{\mathbf{u}}}_{0}} \right] = \left[\frac{\partial \mathbf{f}(\mathbf{X}, \bar{\mathbf{u}})}{\partial \mathbf{X}} \right] \left[\frac{\partial \mathbf{X}(t)}{\partial \bar{\mathbf{u}}_{0}, \dot{\bar{\mathbf{u}}}_{0}} \right] + \left[\frac{\partial \mathbf{f}(\mathbf{X}, \bar{\mathbf{u}})}{\partial \bar{\mathbf{u}}} \right] \left[\frac{\partial \bar{\mathbf{u}}(t)}{\partial \bar{\mathbf{u}}_{0}, \dot{\bar{\mathbf{u}}}_{0}} \right]. \tag{89}$$

The initial condition matrices given by equations (87) and (88) allow equation (89) to be integrated numerically from t_0 to t_f to determine the matrices $\partial X(t_f)/\partial \bar{u}_0$ and $\partial X(t_f)/\partial \bar{u}_0$. Notice that the matrices

$$\begin{bmatrix} \frac{\partial f(X,\bar{u})}{\partial X} \end{bmatrix}, \quad \begin{bmatrix} \frac{\partial f(X,\bar{u})}{\partial \bar{u}} \end{bmatrix}, \quad \text{and} \quad \begin{bmatrix} \frac{\partial \bar{u}}{\partial \bar{u}_0}, \dot{\bar{u}}_0 \end{bmatrix}$$

are obtained by explicit partial differentiation of the expressions for $f(X, \bar{u})$ and $\bar{u}(t)$.

The preceding discussion completes an explanation and brief derivation of the basic ideas included in the computer program of Appendix I. For the actual expressions of all the partial derivatives and any other equations of interest, the reader is referred to Appendix I.

4. Derivation of Optimization Conditions

In the previous section of this report, the optimization problem described by equation (61) was solved using the parameter t_f and the parameters \bar{u}_0 and \bar{u}_0 appearing in a particular form of $\bar{u}(t)$. In this section, the optimization conditions needed to determine $\bar{u}(t)$ satisfying equation (61) will be derived without assuming a specified form for $\bar{u}(t)$ (i.e., the optimization conditions will determine the form for $\bar{u}(t)$). The derivation used here is rather informal, and is included mainly to give the reader an idea about the basis for optimization conditions and their form. A more precise derivation for similar problems can be found in references 15 and 16.

The first step in this derivation is the definition of an optimization criteria (J) with the constraints adjoined to J with vectors of "Lagrangian" multipliers (p and λ). That is,

$$J = x_{8}(t_{f}) + p^{T} G[X(t_{f}), t_{f}] + \int_{t_{o}}^{t_{f}} \left\{ \lambda(t)^{T} \left[\dot{X}(t) - f[X(t), \bar{u}(t)] \right] \right\} dt.$$

$$(90)$$

In equation (90) p is the vector of multipliers associated with the constraints of condition (c) in equation (61), and \wedge (t) is the vector of multipliers associated with the constraints of condition (b) in equation (61). Since p is defined to have the same dimension as G and \wedge the same dimension as X, it can be seen that J is a scalar. For a given set of $X(t_0)$ and t_0 , a minimization of J, a satisfaction of conditions (b) of equation (61), and a satisfaction of the condition $g[X(t_f),t_f]=0$ by the selection of u(t) will produce a minimum of $x_8(t_f)$ and thus solve the problem stated in equation (61).

To minimize J as given in equation (90), with the proper selection of a $\bar{\mathbf{u}}(t)$, consider the class C of all $\mathbf{u}(t)$ (where $\mathbf{t}_0 \leq \mathbf{t} \leq \mathbf{t}_f$) which satisfy the differential equations $\dot{\mathbf{X}} = \mathbf{f}(\mathbf{X}, \bar{\mathbf{u}})$ and the boundary conditions $\mathbf{G}[\mathbf{X}(\mathbf{t}_f), \mathbf{t}_f] = \mathbf{0}$. Let $\bar{\mathbf{u}}^*(t)$ denote a particular control function in this class and $\delta \mathbf{u}(t)$ a small variation in $\bar{\mathbf{u}}^*(t)$ such that $\bar{\mathbf{u}}(t)$ equal to $\bar{\mathbf{u}}^*(t) + \delta \bar{\mathbf{u}}(t)$ is in C. Then $\bar{\mathbf{u}}^*(t)$ will be at least a local minimum of J if $\delta \mathbf{J} = \mathbf{0}$ and $\delta^2 \mathbf{J} > \mathbf{0}$. The computer program in Appendix I can be

used to show that the class C is not empty and that variations in $\bar{u}^*(t)$ (produced by a $\delta \bar{u}(t)$) are also in C at least for some of the $\bar{u}^*(t)$ in C. Thus, the computer programed Appendix I can be used to show the existing ence of a nonempty subclass C contained in C such that every element u(t) in C^* is continuous with respect to t and has variations $\delta \bar{u}(t)$ which produce continuous variations in the trajectory given by X(t). This is the class of control functions to be considered here in the examination of δJ and $\delta^2 J$. Thus, for a particular $\bar{u}^*(t)$ in C^* , a small variation $\delta \bar{u}(t)$ will give $\bar{u}^*(t)$ and $\bar{u}^*(t)$ in $\bar{u}^*(t)$

 $\begin{array}{c} \text{The read points of the sequence of its equation between the sequence of the sequence$

In equation (91) the term

$$\frac{1}{\int \frac{d^{T}}{dt} \delta \dot{x}} dt = \frac{1}{2} \left(\frac{1}{2} + \frac{1}{2} \right) \left(\frac{1}{2} + \frac{1}{2} + \frac{1}{2} \right) \left(\frac{1}{2} + \frac{1}{2$$

can be integrated by parts to give the squelion (c1), and (c1) as the constitution of constitution (c1), and (c1), and (c1) are the constitution (c2) as equalion (c3), and (c4) parts to give the squestion of constitution (c3) and constitution of the same of the squestion of the squestion (c3). The squestion (c4) and constitution (c4), and c4, and c5, and c5

$$\delta J = \left\{ \begin{bmatrix} 0,0,0,0,0,0,0,0,1 \end{bmatrix} + p^{T} \begin{bmatrix} \frac{\partial G[X(\mathbf{t}_{f}),\mathbf{t}_{f}]}{\partial X(\mathbf{t}_{f})} \end{bmatrix}_{*}^{*} + \lambda^{T}(\mathbf{t}_{f}) \right\} \delta X(\mathbf{t}_{f})$$

int ∂^2) constituted by diveloped and examine to this in the second very very level state that the first $\int_{\mathbb{R}^2} \mathbf{f} \cdot \mathbf$

$$-\int_{0}^{t} \left[\left\{ \dot{\lambda}^{T}(t) + \lambda^{T}(t) \left[\frac{\partial f[X(t), \bar{u}(t)]}{\partial X(t)} \right] \right\} \frac{\delta X(t)}{\delta X(t)} \right] dt dt$$

$$(3) Log (3) B$$

$$+ \lambda^{\mathbf{T}}(\mathbf{t}) \begin{bmatrix} \frac{\partial \mathbf{f}[\mathbf{X}(\mathbf{t}), \bar{\mathbf{u}}(\mathbf{t})]}{\partial \bar{\mathbf{u}}(\mathbf{t}), \text{ wod}} & \delta \bar{\mathbf{u}}(\bar{\mathbf{t}}) \end{bmatrix} \delta \mathbf{d} \mathbf{f}^{\lambda} = \delta \mathbf{u}^{\lambda} + \delta \mathbf{u}^{\lambda}$$

objecte points occur on a majectory which sarismus

From equation (93), the list of necessary conditions are obtained by requiring that $\delta J = 0$. This gives

is (b) modificate data bearess and new the condition of

(a)
$$\lambda^{T}(t_{f}) = -[0,0,0,0,0,0,0,1] - p^{T} \left[\frac{\partial G[X(t_{f}),t_{f}]}{\partial X(t_{f})} \right]_{*}$$

(b)
$$p^{T} \dot{G}^{*}[X(t_{f}), t_{f}] = 0$$

(94) "
(94) "
(95) A temperation of (1.6) for (2.6) At emptions of the emption of (2.6) and (3.6) and (4.6) and (4.

(d)
$$\lambda^{T}(t) \left[\frac{\partial f[X(t), \bar{u}(t)]}{\partial \bar{u}(t)} \right]_{\text{exections}} = 0.$$

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Thus, any candidate trajectory for the minimization of J must satisfy conditions (a), (b), (c), and (d) of equation (94). Conditions (a) and (b) are called transversality conditions, condition (c) is the defining differential equation for $\lambda(t)$, and condition (d) is used to define $\bar{u}(t)$. The next section of this report will explain more about how

equation (94) is used to obtain candidate trajectories for the minimization of J.

At this point $\delta^2 J$ could be developed and examined to obtain the conditions which assure that $\delta^2 J>0$, but this has already been done and explained very well in chapter 6 of reference 16. Thus, it will not be done again here, but the reader is urged to examine this material to understand the following sufficiency conditions which will be given. That is, $\delta^2 J>0$, if

(a)
$$\frac{\partial^2 \{\lambda^T f[X(t), \bar{u}(t)]\}}{\partial \bar{u}(t) \partial \bar{u}(t)}$$
 is negative definite, (95)

- (b) the normality condition is satisfied on a trajectory which satisfies equations (94) and (a) above,
- (c) no conjugate points occur on a trajectory which satisfies equations (94) and (a) above.

In equation (95), condition (a) is usually called the strengthened Legendre-Clebsch condition and can be combined with condition (d) of equation (94) to say that

$$H(t) = \lambda^{T} f[X(t), \bar{u}(t)]$$
 (96)

must be a local maximum with respect to $\bar{\mathbf{u}}(t)$ for $\mathbf{t}_0 \leqq \mathbf{t} \leqq \mathbf{t}_f$. An explanation of the meaning of conditions (b) and (c) of equation (95) will be deferred until section 6 on the solution of the boundary value problem resulting from an application of the other optimization conditions just developed. This completes the derivation and explanation of the optimization conditions which will be used in the next section.

5. Application of Optimization Equations

The complete set of differential equations in first order form to be used for this illustration is given by

$$\dot{x}_{1} = x_{4}
\dot{x}_{2} = x_{5}
\dot{x}_{3} = x_{6}$$

$$\begin{bmatrix}
\dot{x}_{4} \\
\dot{x}_{5} \\
\dot{x}_{6}
\end{bmatrix} = (F/x_{7})\bar{u} - \frac{GM \begin{bmatrix} x_{1} \\ x_{2} \\ x_{3} \end{bmatrix}}{(x_{1}^{2} + x_{2}^{2} + x_{3}^{2})^{3/2}} + \bar{g}(x_{1}, x_{2}, x_{3})
+ (\rho A_{r}/2x_{7}) \left\{ C_{L_{\alpha}} [(\bar{V}_{r} \cdot \bar{V}_{r})\bar{u} - (\bar{V}_{r} \cdot \bar{u}) \bar{V}_{r}] \right\}$$

$$- [(\bar{V}_{r} \cdot \bar{V}_{r})^{1/2}(C_{A} + 2\eta C_{L_{\alpha}}^{2}) - 2\eta C_{L_{\alpha}}^{2}(\bar{V}_{r} \cdot \bar{u})] \bar{V}_{r}$$

$$\dot{x}_{7} = \dot{m}$$
(97)

$$\begin{split} \dot{\mathbf{x}}_{8} &= \mathbf{k}_{1}\dot{\mathbf{m}} + \mathbf{k}_{2}(\mathbf{e}\sqrt{\sigma})\rho^{1/2}|\bar{\mathbf{v}}_{\mathbf{r}}|^{3} \\ &+ \mathbf{k}_{3}(\rho\mathbf{A}_{\mathbf{r}}/2\mathbf{x}_{7})^{2}[(\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}})^{2}(\mathbf{C}_{\mathbf{A}}^{2} + 4\eta \ \mathbf{C}_{\mathbf{A}} \ \mathbf{C}_{\mathbf{L}_{\mathcal{Q}}}^{2} + 2\mathbf{C}_{\mathbf{L}_{\mathcal{Q}}}^{2}) \\ &- 2(\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{u}})(\bar{\mathbf{v}}_{\mathbf{r}} \cdot \bar{\mathbf{v}}_{\mathbf{r}})^{3/2}(\mathbf{C}_{\mathbf{L}_{\mathcal{Q}}}^{2} + 2\eta \ \mathbf{C}_{\mathbf{A}} \ \mathbf{C}_{\mathbf{L}_{\mathcal{Q}}}^{2})]. \end{split}$$

With these differential equations the Hamiltonian H(t) defined by equation (96) can be written as

$$H(t) = \lambda_{1}x_{4} + \lambda_{2}x_{5} + \lambda_{3}x_{6} + [\lambda_{4}, \lambda_{5}, \lambda_{6}] \left[(F/x_{7})\bar{u} - \frac{GM \left[\begin{array}{c} x_{1} \\ x_{2} \\ x_{3} \end{array} \right]}{(x_{1}^{2} + x_{2}^{2} + x_{3}^{2})^{3/2}} \right]$$

$$+ \bar{g}(x_{1}, x_{2}, x_{3}) + (\rho A_{r}/2x_{7}) \left\{ C_{L_{\alpha}} [(\bar{v}_{r} \cdot \bar{v}_{r})\bar{u} - (\bar{v}_{r} \cdot \bar{u})\bar{v}_{r}] \right\}$$

$$- [(\bar{v}_{r} \cdot \bar{v}_{r})^{1/2} (C_{A} + 2\eta C_{L_{\alpha}}^{2}) - 2\eta C_{L_{\alpha}}^{2} (\bar{v}_{r} \cdot \bar{u})] \bar{v}_{r} \right\}$$
(98)

(equation (98) continued on next page)

$$+ \lambda_{8} \left\{ k_{1}\dot{m} + k_{2}(e \sqrt{\sigma}) \rho^{1/2} | \bar{v}_{r}|^{3} + k_{3}(\rho A_{r}/2x_{7})^{2} [(\bar{v}_{r} \cdot \bar{v}_{r})^{2}(C_{A}^{2} + 4\eta C_{A} C_{L\alpha}^{2} + 2C_{L\alpha}^{2}) \right.$$

$$-2(\bar{v}_{r} \cdot \bar{u})(\bar{v}_{r} \cdot \bar{v}_{r})^{3/2}(C_{L\alpha}^{2} + 2\eta C_{A} C_{L\alpha}^{2})] \right\} .$$

To maximize H(t) with respect to u(t), only the terms involving u(t) need to be considered. That is,

$$\begin{split} \mathbf{H'}(\mathbf{t}) &= \left[\lambda_4, \lambda_5, \lambda_6\right] \left[(\mathbf{F/x_7}) \mathbf{\bar{u}} + (\rho \mathbf{A_r/2x_7}) \left\{ \mathbf{C_{L_{\alpha}}} [(\mathbf{\bar{v}_r} \cdot \mathbf{\bar{v}_r}) \mathbf{\bar{u}} - (\mathbf{\bar{v}_r} \cdot \mathbf{\bar{u}}) \mathbf{\bar{v}_r}] \right. \\ &+ 2\eta \ \mathbf{C_{L_{\alpha}}^2} \left(\mathbf{\bar{v}_r} \cdot \mathbf{\bar{u}} \right) \mathbf{\bar{v}_r} \right\} \right] \\ &- \lambda_8 \mathbf{k_3} (\rho \mathbf{A_r/2x_7})^2 \left[2 \left(\mathbf{\bar{v}_r} \cdot \mathbf{\bar{u}} \right) (\mathbf{\bar{v}_r} \cdot \mathbf{\bar{v}_r})^{3/2} (\mathbf{C_{L_{\alpha}}^2} + 2\eta \ \mathbf{C_A} \ \mathbf{C_{L_{\alpha}}^2}) \right]. \end{split}$$

Then H(t) can be written as

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$$H(t) = \bar{z}(t) + H'(t) = \bar{z}(t) + \bar{h}^{T}(t) \bar{u}(t),$$
 (100)

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where 4: 3

$$\bar{z}(t) = \lambda_1 x_4 + \lambda_2 x_5 + \lambda_3 x_6 + [\lambda_4, \lambda_5, \lambda_6] \left[-\frac{\left[\frac{x_1}{x_2} \right]}{(x_1^2 + x_2^2 + x_3^2)^{3/2}} + \bar{g}(x_1, x_2, x_3) \right]$$

$$-(\rho A_{r}/2x_{7})(C_{A} + 2\eta C_{L_{Q}}^{2})(\bar{v}_{r} \cdot \bar{v}_{r})^{1/2}$$

$$+\lambda_{7}\dot{m} + \lambda_{8}[k_{1}\dot{m} + k_{2}(eN\sigma)\rho^{1/2}|\bar{v}_{r}|^{3}]$$
(101)

$$+ \ k_3 (\rho A_r/2x_7)^2 (\bar{v}_r \cdot \bar{v}_r)^2 (c_A^2 + 4\eta \ c_A \ c_{L_C}^2 + 2c_{L_C}^2]$$

and

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$$\bar{h}^{T} = [\lambda_{4}, \lambda_{5}, \lambda_{6}] \left\{ [(F/x_{7}) + (\rho A_{r}/2x_{7}) C_{L\alpha}(\bar{v}_{r} \cdot \bar{v}_{r})] \middle| \begin{array}{c} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{array} \right\}$$

 $-\lambda_8 k_3 \left(\rho A_r/2x_7\right)^2 2 \left(\overline{v}_r \cdot \overline{v}_r\right)^{3/2} \left(c_{L\alpha}^2 + 2\eta c_A c_{L\alpha}^2\right) \overline{v}_r^T.$ Since u(t) has been assumed to be a unit vector throughout this report, it can be written as main and all appreciations of man market, a

$$\bar{\mathbf{u}}(\mathbf{t}) = \frac{\bar{\mathbf{p}}(\mathbf{t})}{|\bar{\mathbf{p}}(\mathbf{t})|}, \qquad \qquad \bar{\mathbf{h}}_{\bar{\mathbf{h}}}$$

so that p(t) becomes the actual control variable which is used to maximize H(t). Applying condition (d) of equation (94) to equation (100) with

$$\bar{u} = \frac{\bar{p}(t)}{|\bar{p}(t)|}$$

gives

$$\frac{\partial H(t)}{\partial \bar{p}(t)} = \bar{h}^{T} \left\{ \frac{\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}}{|\bar{p}|} - \frac{\bar{p} \, \bar{p}^{T}}{|\bar{p}|^{3}} \right\}. \tag{104}$$

As can be seen in equation (104),

$$\frac{\partial H(t)}{\partial \bar{p}(t)} = 0,$$

when $\tilde{p}(t) = \pm \tilde{h}(t)$. Also, condition (a) of equation (95) applied to equation (100) will show that

$$\frac{\partial^2 H(t)}{\partial \bar{p}(t) \partial \bar{p}(t)}$$

will be a negative definite matrix only if $\bar{p}(t) = \bar{h}(t)$. Thus, the optimal control $\bar{u}(t)$ for $t_0 \le t \le t_f$ is determined by

$$\bar{\mathbf{u}}(t) = \frac{\bar{\mathbf{h}}(t)}{|\bar{\mathbf{h}}(t)|}, \qquad (105)$$

where $\bar{h}(t)$ is given by equation (102). As can be seen in equation (102), the values of some of the multipliers $\lambda_1,\lambda_2,\ldots,\lambda_8$ are needed at each t to determine $\bar{u}(t)$. Thus, the differential equations for these multipliers given by condition (c) of equation (94) must be used. This equation can be written in the form

$$\dot{\lambda} = -\frac{\partial X}{\partial H} \tag{106}$$

where H is given in equation (98). To take the partial derivatives indicated in equation (106) and write explicit equations for the $\dot{\lambda}$'s

is a rather lengthy task and thus will not be included here. The Fortran expressions for these differential equations can be found in the differential equation subroutine (DEQ) of the computer program listing in Appendix II. For a given set of initial conditions $(X(t_0),$ $\lambda(t_0)$, and t_0), this computer program integrates numerically the differential equations given by equations (97) and (106) and uses equation (105) to yield at each t (where $t_0 \le t \le t_f$) a value for X(t), $\lambda(t)$, and $\bar{u}(t)$. The numerical integration of the differential equations stops at a given time (t_f) . At this time t_f conditions (a) and (b) of equation (94) can be applied to any of the three sets of boundary conditions (G's) described in section (3) to give the transversality conditions which complete the boundary value problem. As an example, equations (54), (55), (56), (57), and (58) are used, and the result is the equations listed in subroutine BOUND of Appendix II. As can be seen in this subroutine, or in conditions (a) and (b) of equation (94), values for the end condition multipliers (p's) must be given to evaluate the transversality conditions.

This completes the discussion of the application of the optimization conditions developed in the previous section. To reiterate the steps in the calculation of a candidate optimal trajectory, the following steps are listed and called equation (107):

- (a) Values of $X(t_0)$ and t_0 are given as fixed values.
- (b) Values of $\lambda(t_0)$, p, and t_f must be known or determined.
- (c) The differential equations

$$\dot{X}(t) f[X(t), \ddot{u}(t)]$$
(107)

$$\dot{\lambda}(t) = \left[\frac{\partial f[X(t), \bar{u}(t)]}{\partial X(t)}\right]^{T} \lambda(t)$$

with

$$\bar{u}(t) = \frac{\bar{h}(t)}{|\bar{h}(t)|}$$

(where $\bar{h}(t)$ is defined by equation (102)) must be integrated numerically to t_f with the initial conditions given in conditions (a) and (b).

(equation (107) continued on next page)

(d). The known or determined values of $\lambda(t_0)$, p, and t_f asympton of the sin (b) must cause the following boundary condition to be active as asymptonic of the single condition to be active as asymptonic of the single condition to be active as asymptonic of the single condition of the sin

The determination of $\lambda(t_0)$, p, and t_f to satisfy the boundary conditions of condition (d) subject to the initial conditions (condition (a)) and the differential equation constraints of condition (c) is the boundary value problem to be solved. Methods for its solution are discussed below.

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As can be seen in equation (107), the values of $\lambda(t_0)$ are the only variables that can be used to change the values of X(t) and $\lambda(t)$, because, by condition (a), $X(t_0)$ and t_0 are fixed, and, by condition (c), the differential equations and optimal u(t) relation must hold. Thus, the boundary conditions given in (d) of equation (107) can be written as

$$F[\lambda(t_0), p, t_f] = 0, \qquad (108)$$

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where the dimension of F is equal to the dimension of G, plus the dimension of λ , plus one. Actually F has the form

112.7

but $X(t_f)$ and $\lambda(t_f)$ appearing in the right-hand side of the above equation depend implicitly on $\lambda(t_0)$ which leads to the functional form given in equation (108). Now for a guessed set of $\lambda(t_0)$, p, and t_f (denoted by λ_0^* , p*, t*f), a Taylor series expansion can be written:

$$F[\lambda(t_{o}),p,t_{f}] = F[\lambda_{o}^{*},p^{*},t_{f}^{*}] + \left[\frac{\partial F[\lambda(t_{o}),p,t_{f}]}{\partial \lambda(t_{o}),p,t_{f}}\right]_{\lambda_{o}^{*},p^{*},t_{f}^{*}} \begin{bmatrix} \triangle \lambda(t_{o}) \\ \triangle p \\ \triangle t_{f} \end{bmatrix}_{*} \dots$$

$$(110)$$

The higher order terms in the above expression can be neglected, a fudge factor K (where $0 < K \le 1$) can be chosen, and the above equation solved to yield the corrections $(\triangle \lambda(t_0), p, \text{ and } \triangle t_f)$ which, when added to λ_0^* , p_i^* and t_f^* and used to generate a new trajectory, will produce a decrease in the error term F^T F. That is,

$$\begin{bmatrix} \Delta \lambda(t_{o}) \\ \Delta p \\ \Delta t_{f} \end{bmatrix} = -K \begin{bmatrix} \frac{-\partial F[\lambda(t_{o}), p, t_{f}]}{\partial \lambda(t_{o}), p, t_{f}} \end{bmatrix}_{\lambda_{o}^{*}, p^{*}, t_{f}^{*}}^{-1} F[\lambda_{o}^{*}, p^{*}, t_{f}^{*}].$$
(111)

It can be seen that, as long as the matrix which must be inverted in the above equation is nonsingular, a value for K can be chosen as close to zero as necessary to give a set of corrections $(\triangle \setminus (t_0), \, \triangle p, \, \text{and} \, \triangle t_f)$ which, when used to generate a new trajectory, will make the square root of the error term $(\sqrt{F^T} \ F)$ less than or equal to I- K times the square root of the original error $(\sqrt{F^T} (\lambda_0^*, p^*, t_f^*) \ F(\lambda_0^*, p^*, t_f^*)$. Thus, if equation (III) is used iteratively and the matrix inverse continues to exist, a set of values for $\lambda(t_0)$, p, and t_f can be found which will make $F[\lambda(t_0), p, t_f] = 0$.

To obtain numerical values for the matrices

$$\left[\frac{\partial F[\lambda(t_o), p, t_f]}{\partial \lambda(t_o)} \right]_{\lambda_o^*, p^*, t_f^*} \text{ and } \left[\frac{\partial F[\lambda(t_o), p, t_f]}{\partial t_f} \right]_{\lambda_o^*, p^*, t_f^*},$$

the chain rule is used on the form of F given in equation (109) and results in the following equation:

$$\begin{bmatrix}
\frac{\partial F[\lambda(t_{o}), p, t_{f}]}{\partial \lambda(t_{o})} \end{bmatrix}_{\lambda_{o}^{*}, p^{*}, t_{f}^{*}} = \begin{bmatrix}
\frac{\partial F[X(t_{f}), \lambda(t_{f}), p, t_{f}]}{\partial X(t_{f})} \end{bmatrix}_{*} \begin{pmatrix}
\frac{\partial X(t_{f})}{\partial \lambda(t_{o})} \end{pmatrix}_{*} \\
+ \begin{bmatrix}
\frac{\partial F[X(t_{f}), \lambda(t_{f}), p, t_{f}]}{\partial \lambda(t_{f})} \end{bmatrix}_{*} \begin{pmatrix}
\frac{\partial \lambda(t_{f})}{\partial \lambda(t_{o})} \end{pmatrix}_{*}$$
(112)

$$\left[\frac{\partial F[\lambda(t_{o}), p, t_{f}]}{\partial t_{f}}\right]_{\lambda_{o}^{*}, p^{*}, t_{f}^{*}} = \dot{F}[\lambda(t_{o}), p, t_{f}]_{\lambda_{o}^{*}, p^{*}, t_{f}^{*}}.$$
(113)

The matrix

$$\left[\frac{\partial F[\lambda(t_{o}), p, t_{f}]}{\partial p}\right]_{\lambda_{o}^{*}, p^{*}, t_{f}}$$

is obtained by explicit partial differentiation of the expression for $F[\lambda(t_0),p,t_f]$ given by equation (109). Thus, the expression for

$$\left[\frac{\partial F[\lambda(t_o), p, t_f]}{\partial \lambda(t_o), p, t_f}\right]_{\lambda_o^*, p, t_f^*}$$

can be written by combining the expressions in equations (112) and (113) with the expressions for

$$\left[\frac{\partial F[\lambda(t_o), p, t_f]}{\partial p}\right]_{\lambda_o^*, p^*, t_f}.$$

In equation (112) the matrices

$$\left[\frac{\partial F[X(t_f),\lambda(t_f),p,t_f]}{\partial X(t_f)}\right]_* \quad \text{and} \quad \left[\frac{\partial F[X(t_f),\lambda(t_f),p,t_f]}{\partial \lambda(t_f)}\right]_*$$

can be obtained by explicit partial differentiation, but the matrices

$$\left(\frac{\partial X(t_f)}{\partial \lambda(t_o)}\right)_*$$
 and $\left(\frac{\partial \lambda(t_f)}{\partial \lambda(t_o)}\right)_*$

must be obtained from the numerical integration of the following set of matrix differential equations:

(a)
$$\frac{d}{dt} \left(\frac{\partial X(t)}{\partial \lambda(t_o)} \right) = \frac{\partial \dot{X}(t)}{\partial \lambda(t_o)} = \left[\frac{\partial f(X(t), \bar{u}(t))}{\partial X(t)} \right] \left(\frac{\partial X(t)}{\partial \lambda(t_o)} \right)$$

$$+ \left[\frac{\partial f(X(t), \bar{u}(t))}{\partial \bar{u}(t)}\right] \left(\frac{\partial \bar{u}(t)}{\partial \lambda(t_0)}\right).$$

(b)
$$\frac{\mathrm{d}}{\mathrm{d}t} \left(\frac{\partial \lambda(t)}{\partial \lambda(t_0)} \right) = \frac{\partial \dot{\lambda}(t)}{\partial \lambda(t_0)} = \left[\frac{\partial^2 \lambda^{\mathrm{T}} f(X(t), \bar{u}(t))}{\partial X(t)} \right] \left(\frac{\partial X(t)}{\partial \lambda(t_0)} \right)$$

$$+ \left[\frac{\partial f(X(t), \bar{u}(t))}{\partial X(t)}\right]^T \left(\frac{\partial \lambda(t)}{\partial \lambda(t_0)}\right)$$

$$+ \left[\frac{\partial^2 \lambda^{\mathrm{T}} f(X(t), \bar{u}(t))}{\partial X \partial \bar{u}(t)} \right] \left(\frac{\partial \bar{u}(t)}{\partial \lambda(t_0)} \right)$$

(c)
$$[0] = \begin{bmatrix} \frac{\partial^2 \lambda^{\mathrm{T}} f(X(t), \bar{u}(t))}{\partial \bar{u}(t) \partial X(t)} \end{bmatrix} \begin{pmatrix} \frac{\partial X(t)}{\partial \lambda(t_0)} \end{pmatrix} + \begin{bmatrix} \frac{\partial f(X(t), \bar{u}(t))}{\partial \bar{u}(t)} \end{bmatrix}^{\mathrm{T}} \begin{pmatrix} \frac{\partial \lambda(t)}{\partial \lambda(t_0)} \end{pmatrix}$$

$$+ \left[\frac{\partial^2 \lambda^T f(X(t), \bar{u}(t))}{\partial \bar{u}(t) \partial \bar{u}(t)} \right] \frac{\partial \bar{u}(t)}{\partial \lambda(t_0)} \ .$$

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Note that condition (c) above allows

$$\frac{\partial \bar{\mathbf{g}}(\mathbf{t})}{\partial y(\mathbf{t}^0)} + \lambda(100) \qquad \qquad \text{for } \mathbf{g} = \mathbf{g} = \mathbf{g} + \mathbf{g} = \mathbf{g$$

to be determined at each instant of time because the strengthened Legendre Clebsch condition requires the matrix

$$\begin{bmatrix} \frac{\partial^2 \lambda^T f(X(t), \bar{u}(t))}{\partial \bar{u}(t)} \frac{\partial^2 \lambda^T f(X(t), \bar{u}(t))}{\partial \bar{u}(t)} \end{bmatrix}$$

to be negative definite. Thus, the above system can be integrated numerically along with the system given in equation (107), using the guessed values $(\lambda_0^*, p^*, t_f^*)$ and the initial conditions

$$\frac{\partial X(t_0)}{\partial \lambda(t_0)} = [0] \text{ and } \frac{\partial \lambda(t_0)}{\partial \lambda(t_0)} = [1].$$

This completes the explanation of Newton's method for the solution of the boundary value problem.

When a solution of the boundary value problem by Newton's method is obtained as discussed previously, the sufficiency conditions given by conditions (b) and (c) of equation (95) can be checked very easily. The normality condition will be satisfied if the matrix

$$\frac{\partial F[\lambda(t_0), p, t_f]}{\partial \lambda(t_0), p, t_f}$$

is positive definite when evaluated for values of $\lambda(t_0)$,p, and t_f which satisfy equation (107). Reference 17 gives a very good explanation and a computer program listing for determining the definiteness of a matrix. The proof of this normality condition's contribution to the sufficiency conditions requires a detailed and difficult examination of the second variation as shown in reference 16, and will not be attempted here.

The easiest way to check a trajectory satisfying equation (107) for conjugate points is to generate the feedback guidance matrix. To do $\frac{(1) \cdot (1)}{(1) \cdot (1)} = \frac{(1) \cdot (1)}{(1)} = \frac{(1) \cdot (1)}{(1)$

this the differential equation for the transition matrices

$$\left(\frac{\partial X(t)}{\partial X(t_o)} \right) \quad \text{and} \quad \left(\frac{\partial \lambda(t)}{\partial X(t_o)} \right)$$

are needed. These are obtained as equations (114) were obtained. That is,

(a)
$$\frac{d}{dt} \left(\frac{\partial X(t)}{\partial X(t_0)} \right) = \frac{\partial \dot{X}(t)}{\partial X(t_0)} = \text{same as (114) with } \lambda(t_0)$$
 replaced by $X(t_0)$.

(b)
$$\frac{d}{dt} \left(\frac{\partial \lambda(t)}{\partial X(t_0)} \right) = \frac{\partial \dot{\lambda}(t)}{\partial X(t_0)} = \text{same as (114) with } \lambda(t_0)$$
 replaced by $X(t_0)$.

(c) [0] = same as (114) with $\lambda(t_0)$ replaced by $X(t_0)$.

The initial conditions for these equations are

$$\left(\frac{\partial X(t_o)}{\partial X(t_o)}\right) = I$$
 and $\left(\frac{\partial \lambda(t_o)}{\partial X(t_o)}\right) = [0].$

Thus, for values of $\lambda(t_0)$, p, and t_f which satisfy equations (107), the transition matrices

$$\left(\frac{\partial X(t)}{\partial X(t_0)}\right)$$
, $\left(\frac{\partial X(t)}{\partial \lambda(t_0)}\right)$, $\left(\frac{\partial \lambda(t)}{\partial X(t_0)}\right)$, and $\left(\frac{\partial \lambda(t)}{\partial \lambda(t_0)}\right)$

where ($t_0 \le t \le t_f$) can be obtained by numerically integrating equations (114) and (115). Also needed are the vectors

$$\frac{\partial X(t)}{\partial t_0}$$
 and $\frac{\partial \lambda(t)}{\partial t_0}$

which are defined by differential equations similar to equations (114) and (115). That is

(a)
$$\frac{d}{dt} \left(\frac{\partial X(t)}{\partial t_o} \right) = \frac{\partial \dot{X}(t)}{\partial t_o} = \text{same as (114) with } \lambda(t_o)$$
replaced by t_o .

(b)
$$\frac{d}{dt} \left(\frac{\partial \lambda(t)}{\partial t_0} \right) = \frac{\partial \lambda(t)}{\partial t_0} = \text{same as (114) with } \lambda(t_0)$$
 replaced by t_0 .

(c) [0] = same as (114) with $\lambda(t_0)$ replaced by t_0 .

Note that $\partial X(t_0)/\partial t_0 = \dot{X}_0$ and $\partial \lambda(t_0)/\partial t_0 = \dot{\lambda}_0$.

With all of these transition matrices, a set of trajectories about the trajectory-satisfying equation (107) can be represented by

$$\Delta X(t) = \left(\frac{\partial X(t)}{\partial X(t_0)}\right) \Delta X(t_0) + \left(\frac{\partial X(t)}{\partial \lambda(t_0)}\right) \Delta \lambda(t_0) + \left(\frac{\partial X(t)}{\partial t_0}\right) \Delta t_0. \tag{117}$$

$$\Delta\lambda(t) = \left(\frac{\partial\lambda(t)}{\partial X(t_o)}\right) \Delta X(t_o) + \left(\frac{\partial\lambda(t)}{\partial\lambda(t_o)}\right) \Delta\lambda(t_o) + \left(\frac{\partial\lambda(t)}{\partial t_o}\right) \Delta t_o. \tag{118}$$

Equations (117) and (118) state that small changes in the initial conditions which satisfy equations (107) are mapped by the transition matrices into small changes $\triangle X$ and $\triangle \lambda$ at any time t where $t_0 \leq t \leq t_f$. In the set of trajectories defined by equations (117) and (118), a subset can be defined (all of which satisfy equation (107)) by requiring the $\triangle X(t_f)$ and $\triangle \lambda(t_f)$ produced by $\triangle X(t_o)$, $\triangle \lambda(t_o)$, and $\triangle t_o$ to satisfy condition (d) of equation (107). Thus, $\triangle F$ produced by substituting $\triangle X(t_f)$ and $\triangle \lambda(t_f)$ into equation (109) must be zero. That is,

$$\Delta F = (\partial F/\partial X_f) \Delta X_f + (\partial F/\partial \lambda_f) \Delta \lambda_f + (\partial F/\partial p) \Delta p + \dot{F} \Delta t_f = 0.$$
 (119)

Substituting equations (117) and (118) (evaluated at $t_{\rm f}$) into (119) gives

$$\frac{\partial \mathbf{F}}{\partial \mathbf{X}_{\mathbf{f}}} \left[\left(\frac{\partial \mathbf{X}_{\mathbf{f}}}{\partial \mathbf{X}_{\mathbf{o}}} \right) \Delta \mathbf{X}_{\mathbf{o}} + \left(\frac{\partial \mathbf{X}_{\mathbf{f}}}{\partial \lambda_{\mathbf{o}}} \right) \Delta \lambda_{\mathbf{o}} + \left(\frac{\partial \mathbf{X}_{\mathbf{f}}}{\partial \mathbf{t}_{\mathbf{o}}} \right) \Delta \mathbf{t}_{\mathbf{o}} \right] + \left(\frac{\partial \mathbf{F}}{\partial \lambda_{\mathbf{f}}} \right) \left[\left(\frac{\partial \lambda_{\mathbf{f}}}{\partial \mathbf{X}_{\mathbf{o}}} \right) \Delta \mathbf{X}_{\mathbf{o}} + \left(\frac{\partial \lambda_{\mathbf{f}}}{\partial \lambda_{\mathbf{o}}} \right) \Delta \mathbf{t}_{\mathbf{o}} \right] + \left(\frac{\partial \mathbf{F}}{\partial \mathbf{p}} \right) \Delta \mathbf{p} + \dot{\mathbf{F}} \Delta \mathbf{t}_{\mathbf{f}} = 0.$$
(120)

Equation (120) can be written as

$$\begin{bmatrix} A \end{bmatrix} \begin{bmatrix} \triangle \lambda_{o} \\ \triangle p \\ \triangle t_{f} \end{bmatrix} + B \begin{bmatrix} \triangle x_{o} \\ \triangle t_{o} \end{bmatrix} = 0, \tag{121}$$

where

$$A = \left\{ \left[\frac{\partial F}{\partial X_f} \left(\frac{\partial X_f}{\partial \lambda_o} \right) + \left(\frac{\partial F}{\partial \lambda_f} \right) \left(\frac{\partial \lambda_f}{\partial \lambda_o} \right) \right], \frac{\partial F}{\partial p}, \dot{F} \right\}$$

$$B = \left\{ \left[\frac{\partial X_f}{\partial X_f} \left(\frac{\partial X_f}{\partial X_o} \right) + \left(\frac{\partial F}{\partial \lambda_f} \right) \left(\frac{\partial X_f}{\partial X_o} \right) \right], \left[\frac{\partial F}{\partial X_f} \left(\frac{\partial X_f}{\partial x_o} \right) + \frac{\partial F}{\partial \lambda_f} \left(\frac{\partial X_f}{\partial x_o} \right) \right] \right\}.$$

Note that A is the same matrix which appears in equations (110) and (111) and must be positive definite from the normality condition. Thus, A is nonsingular so that

$$\begin{bmatrix} \triangle \lambda_{o} \\ \triangle p \\ \triangle t_{f} \end{bmatrix} = A^{-1} B \begin{bmatrix} \triangle X_{o} \\ \triangle t_{o} \end{bmatrix}. \tag{122}$$

Equation (122) can be partitioned to give

(a)
$$\triangle \lambda_0 = D_1 \triangle X_0 + D_2 \triangle t_0$$

(b) $\triangle p = D_3 \triangle X_0 + D_4 \triangle t_0$
(c) $\triangle t_f = D_5 \triangle X_0 + D_6 \triangle t_0$ (123)

where

$$A^{-1} B = \begin{bmatrix} D_1 & D_2 \\ D_3 & D_4 \\ D_5 & D_6 \end{bmatrix}.$$

Now either $\triangle t_f$ or $\triangle t_o$ can be chosen to be zero. Usually, for purposes of comparison, it is better to choose $\triangle t_f$ to be zero. Then, from equation (123) part (c), it can be seen that

$$\triangle t_{o} = -(1/D_{6}) D_{5} \triangle X_{o}.$$
 (124)

Equation (124) can be substituted into parts (a) and (b) of equation (123) to give

(a)
$$\triangle \lambda_{0} = [D_{1} - (1/D_{6})D_{2}D_{5}] \triangle X_{0} = D_{7} \triangle X_{0}$$

(b) $\triangle p = [D_{3} - (1/D_{6})D_{4}D_{5}] \triangle X_{0} = D_{8} \triangle X_{0}$. (125)

Now part (a) of equation (125) and equation (124) can be substituted into equations (117). That is,

$$\Delta X(t) = \left(\frac{\partial X(t)}{\partial X_{o}}\right) \Delta X(t_{o}) + \left(\frac{\partial X(t)}{\partial \lambda_{o}}\right) \left[D_{7} \Delta X_{o}\right] + \left(\frac{\partial X(t)}{\partial t_{o}}\right) \left[-(1/D_{6}) D_{5} \Delta X_{o}\right]$$
(126)

$$\triangle \lambda(t) = \left(\frac{\partial \lambda(t)}{\partial X_{o}}\right) \triangle X(t_{o}) + \left(\frac{\partial \lambda(t)}{\partial \lambda_{o}}\right) \left[D_{7} \triangle X_{o}\right] + \left(\frac{\partial \lambda(t)}{\partial t_{o}}\right) \left[-(1/D_{6}) D_{5} \triangle X_{o}\right]. \tag{127}$$

Equations (126) and (127) can be rewritten to give

$$\Delta X(t) = P(t) \Delta X(t)$$
 (128)

$$\triangle \lambda(t) = Q(t) \triangle X(t_0), \tag{129}$$

where

$$P(t) = \left(\frac{\partial X(t)}{\partial X}\right) + \left(\frac{\partial X(t)}{\partial \lambda}\right) D_7 - \left(\frac{\partial X(t)}{\partial t}\right) (1/D_6) D_5$$

$$Q(t) = \left(\frac{\partial \lambda(t)}{\partial X_{o}}\right) + \left(\frac{\partial \lambda(t)}{\partial \lambda_{o}}\right) D_{7} - \left(\frac{\partial \lambda(t)}{\partial t_{o}}\right) (1/D_{6}) D_{5}.$$

The matrix P(t) which appears in equation (128) is the matrix which must be nonsingular for all t (where $t_0 \le t < t_f$) in order to state that no conjugate points exist on the trajectory satisfying equation (107). Thus, this matrix can be computed at each time t and inverted if it is nonsingular (i.e., its determinant is nonzero). If there are no conjugate points on an optimal trajectory, then linear feedback guidance can be accomplished by solving equations (128) for ΔX_0 and substituting the result into equation (129). That is,

$$\Delta\lambda(t) = [Q(t) P^{-1}(t)] \Delta X(t). \tag{130}$$

Also, the solution of equation (128) for $\Delta X(t_0)$ must be substituted into equations (124) and part (b) of (125) to give

$$\Delta p = [D_8 P^{-1}(t)] \Delta X(t)$$
 (131)

$$\Delta t_0 = [-(1/D_6) D_5 P^{-1}(t)] \Delta X(t),$$
 (132)

Then equations (130), (131), and (132) are the linear feedback guidance equations. That is, for a measured or given value of $\Delta X(t)$ (where $t_0 \leq t < t_f$), $\Delta \lambda(t)$, Δp , and Δt_0 can be computed. Note that, with

values for $\triangle X(t)$ and $\triangle \lambda(t)$, equation (105) can be used to compute $\bar{u}(t)$ directly, or if equation (105) is linearized, then $\triangle \bar{u}(t)$ can be computed, which is the usual form of feedback guidance. In the present MASCOT implementations, equations (130), (131), and (132) are not used, but they are now being examined for use in improving the computational speed of the atmospheric portion of MASCOT.

The preceding discussion completes the solution of the boundary value problem by Newton's method and shows how the complete set of sufficient conditions can also be checked with little additional effort. As can be seen, this approach differs from the "sweep" method explained in chapter 6 of reference 16. After examining the computational aspects and flexibility of both procedures, Newton's method (as explained here) has been selected as the most favorable approach for solving the boundary value problem and also for performing the sufficient condition checks. More support for this viewpoint can be found in some of the statements and numerical results of reference 15.

A considerable amount of effort is involved in establishing a computer program to perform a solution of the boundary value problem and make the sufficiency condition checks by Newton's method. Thus, simpler methods are usually used for problems which are in an early and formulative stage of development. One of the most effective examples of these simpler approaches for solving the boundary value problem is a modification of the secant method, which will be explained next.

As before, the boundary values as given by equation (108) must be satisfied. To simplify the notation, a new vector will be defined as

$$X = \begin{bmatrix} \lambda(t_0) \\ p \\ t_f \end{bmatrix}. \tag{133}$$

Note that this X as defined above has no relation to any previous definition of X. Then the solution of the boundary value problem is a vector $X = (x_1, x_2, ..., x_n)$ that will satisfy equation (108) written in the following form:

$$f_{1}(x_{1}, x_{2}, ..., x_{n}) = 0$$

$$F(X) = f_{2}(x_{1}, x_{2}, ..., x_{n}) = 0$$

$$\vdots$$

$$f_{n}(x_{1}, x_{2}, ..., x_{n}) = 0.$$
(134)

In the explanation to follow, for a given set of values of the X's, the f's can be evaluated only by numerically integrating the differential equations with their given initial conditions and the given set of values of the X's completing the initial conditions. If a coasting phase occurs at any point during this numerical integration procedure, very rapid closed-form solutions are available [8, 9, 10, 11] to obtain the trajectory across this coasting arc without the need for time-consuming numerical integration. Then after the integration is complete, the f's can be evaluated. There are many techniques available for numerically integrating ordinary nonlinear differential equations (such as Runge-Kutta and Shanks formulas), but the most effective yet developed are given in references 18 and 19. Thus, with a given numerical integration technique, the functions f can be evaluated for each set of X's. As can be seen in the explanation to follow, the transition matrix differential equations (113) are not needed for this approach, which accounts for most of its simplicity.

This method begins with a reasonable but nonetheless arbitrary first choice of x_1, x_2, \ldots, x_n . A variation in each of the x's must be made. One possibility is to define

$$y_i = k_i x_i, i = 1, ..., n \text{ and } 0 \le k_i < 1$$
 (135)

and then set up the matrix [X]:

$$[X] = \begin{bmatrix} x_{1} & x_{2} & \dots & x_{n} \\ y_{1} & x_{2} & \dots & x_{n} \\ x_{1} & y_{2} & \dots & x_{n} \\ \vdots & & & & \vdots \\ x_{1} & x_{2} & \dots & y_{n} \end{bmatrix} = \begin{bmatrix} x_{11} & x_{12} & \dots & x_{1n} \\ x_{21} & x_{22} & \dots & x_{2n} \\ \vdots & & & & \vdots \\ x_{j1} & x_{j2} & \dots & x_{jn} \end{bmatrix}.$$
 (136)

Note that j = n + 1, and hence [X] is an $n + 1 \times n$ matrix.

Now, for each of the j rows of [X], X_i , evaluate the n f's. This results in a j \times n matrix of f values. Set

$$[F] = \begin{bmatrix} f_{1}(X_{1}) & f_{2}(X_{1}) & \dots & f_{n}(X_{1}) \\ f_{1}(X_{2}) & f_{2}(X_{2}) & \dots & f_{n}(X_{2}) \\ \vdots & & & & \\ f_{1}(X_{j}) & f_{2}(X_{j}) & \dots & f_{n}(X_{j}) \end{bmatrix} = \begin{bmatrix} f_{11} & f_{12} & \dots & f_{1n} \\ f_{21} & f_{22} & \dots & f_{2n} \\ \vdots & & & & \\ f_{j1} & f_{j2} & \dots & f_{jn} \end{bmatrix}.$$

$$(137)$$

In order to make [X] square (for reasons to be seen), make U the jth column of [X], where U is a column vector of j l's, and define

$$[X] = \begin{bmatrix} [X] & U \end{bmatrix} = \begin{bmatrix} x_{11} & x_{12} & \dots & x_{1n} & 1 \\ x_{21} & x_{22} & \dots & x_{2n} & 1 \\ \vdots & & & & & \\ x_{j1} & x_{j2} & \dots & x_{jn} & 1 \end{bmatrix}.$$
 (138)

The next step in the procedure is to try to replace the row of [X] which resulted in the "worst" row of [F] (for example, the one having the maximum sum of the squares of the f_i , assuming proper normalization) by an X_{new} which results in an improved F. To do this, first note that a matrix [A] exists which has the property

$$[X][A] = [F],$$
 (139)

and set

$$\begin{bmatrix} X_{\text{new}} & 1 \end{bmatrix} [A] = F_{\text{new}}, \tag{140}$$

where X_{new} is a vector of the unknowns that should produce F_{new} and

$$F_{\text{new}} = C \cdot F_{\text{old}}, \quad 0 \le C < 1$$
 (141)

and $F_{\rm old}$ is a row of [F] selected by virtue of its having the minimum sum of squares of the f_i . Note here that an $X_{\rm new}$ is desired which will lead to the "worst" row of F being replaced by one better than the "best" row of [F].

From (139),

$$[A] = [X]^{-1} [F],$$
 (142)

and therefore (140) becomes

$$\begin{bmatrix} X_{\text{new}} & 1 \end{bmatrix} [X]^{-1} [F] = F_{\text{new}}. \tag{143}$$

The solution for \mathbf{X}_{new} proceeds as follows: Let

$$P^{T} = \begin{bmatrix} X_{\text{new}} & 1 \end{bmatrix} [X]^{-1}, \qquad (144)$$

where P is a j = n + 1 column vector. Then, using (144) in (143),

$$P^{T}[F] = F_{new} \quad \text{or } [F]^{T} P = F_{new}^{T}.$$
 (145)

Equations (145) are a set of n equations in j = n + 1 unknowns. However, from (144)

$$P^{T}[X] = \begin{bmatrix} X_{\text{new}} & 1 \end{bmatrix} \quad \text{or} \quad [X]^{T} \quad P = \begin{bmatrix} \frac{X^{T}}{1} \end{bmatrix} . \tag{146}$$

Looking back at (138), note that $[X]^T$ has a bottom row of 1's, so that from (146), the following equation is obtained:

$$\sum_{i=1}^{j} P_i = 1. \tag{147}$$

This provides the jth equation needed to solve for the j unknowns above, as a system of simultaneous equations; i.e.,

$$[F]^T P = F_{\text{new}}^T \quad \text{and} \quad \sum_{i=1}^{j} P_i = 1$$
 (148)

are sufficient to obtain the j components of P.

This may also be written

$$\begin{bmatrix} -\frac{\mathbf{F}^{\mathrm{T}}}{\mathbf{U}^{\mathrm{T}}} - \end{bmatrix} \begin{bmatrix} \mathbf{P}_{1} \\ \mathbf{P}_{2} \\ \vdots \\ \mathbf{P}_{j} \end{bmatrix} = \begin{bmatrix} \mathbf{F}^{\mathrm{T}}_{\text{new}} \\ -\frac{\mathbf{T}}{1} \end{bmatrix}, \qquad (149)$$

where U^{T} is a row of vector of j 1's.

The nonexistence of the inverse in (149) does not necessarily imply that the solution as a set of simultaneous equations does not exist, since the rank of the augmented matrix may be the same as the original one.

Once P is known, (147) gives X_{new}, since from (146)

$$[X]^{T} P = \begin{bmatrix} X^{T} \\ -\frac{new}{1} \end{bmatrix} . \tag{150}$$

This completes the discussion of the methods for solving the boundary value problem as given by equation (107). Several computer programs are available from the authors for solving the boundary value problem as given by equation (107). The listing of these computer programs are not included here because they are almost constantly being modified. Some preliminary results on space shuttle type vehicles have been obtained with the secant method (as explained here) and they are discussed in the Results section of this report. In reference 9, a computer program listing for a Newton's method solution of the Vacuum Trajectory Optimization problem is given. This program,

called SWITCH, is available for use. In reference 8 some examples of the application of feedback guidance associated with Newton's method are given to show that feedback guidance matrices can be used for guidance and to check for the satisfaction of sufficiency conditions.

D. Conclusion of Mathematical Development

The mathematical development presented here for the MASCOT concept has of necessity been rather complicated. It is hoped that the reader is able to spend enough time studying the ideas presented so that he can understand them. This understanding of the general idea and the numerical results presented in the next section should convince most readers that the MASCOT concept as outlined here can be developed into an efficient, effective, and flexible guidance scheme for vehicles of the space shuttle type.

To reiterate and emphasize the key mathematical ideas discussed in this section which now make the onboard solution of the trajectory optimization problem (MASCOT) an attractive guidance scheme for space shuttle type vehicles, the following statements are listed:

First, the unified set of guidance equations and performance criteria will reduce the computer storage requirements for onboard implementation.

Second, the techniques for obtaining a solution of the boundary-value problem have been carefully studied and the so-called "shooting method" selected because of its speed and reliability. The shooting method algorithm is easy to program and is compact in size. The alternatives to the shooting method, such as steepest descent and quasi-linearization, must use stored time functions so that the size and complexity of the algorithms are increased.

Third, the development of the Fehlberg-type, Runge-Kutta numerical integration routines has significantly speeded up the numerical integration process. Further improvements to numerical integration techniques, such as the variation of parameters method of reference 20, can also be easily incorporated into the technique.

Fourth, since the boundary value problem can be considered as the problem of finding the solution to a system of simultaneous nonlinear equations, any improvements in these techniques which may occur in the future can again be incorporated easily into the technique.

Finally, the many improvements in computational hardware which have resulted in flight-worthy high-speed digital computers also adds to the attractiveness of the concept.

VII. NUMERICAL RESULTS

The resources for developing the OPGUID, SWITCH, and MASCOT algorithms have been limited. To obtain the maximum benefit from available funds and manpower, the effort has been concentrated in the area of problem formulation and improving the numerical techniques needed to solve the resulting boundary value problem rather than in performing detailed guidance simulations. Therefore, only limited results are available at this time. These will be discussed in the following paragraphs. The results of the detailed guidance simulation studies now being performed will be published at a later date.

A. OPGUID

The feasibility of solving the trajectory optimization problem in real time for onboard guidance was demonstrated in 1966 by Brown and Johnson [7] for an ascent to orbit mission (vacuum). Since these results can be found in the literature, they will only be summarized here.

The mission selected was ascent to a circular orbit with the S-IVB stage of the AS-204 vehicle. To evaluate the stability and optimality characteristics of the real-time optimal guidance scheme (OPGUID) under realistic conditions, a number of simulations were made and compared to results obtained, making the same simulations with the IGM equations. These included thrust and mass rate variations of ±5 percent and engine mixture ratio shift times of ± 30 seconds from nominal. OPGUID used a variable cycle time ranging from 10 seconds initially to one second near the end. In all cases, the OPGUID scheme delivered more payload to orbit than the IGM scheme; however, these differences in all cases were small (2 to 70 kg), and the main point to be made from this study was that it demonstrated the feasibility of using OPGUID as an onboard guidance scheme. The computer speed and storage requirements for OPGUID can be met by the Saturn Launch Vehicle Digital Computer; thus, OPGUID could serve as an onboard guidance scheme for the Saturn V vehicle.

B. SWITCH

Recently, under NASA contract NAS8-21315, a sophisticated multiburn optimization program, SWITCH [9], was developed which appears to have the speed and reliability needed for onboard guidance signal generations. The convergence properties of the SWITCH program were demonstrated by applying it to a multi-burn rendezvous mission. The

target vehicle was located in a synchronous orbit with an altitude of 19,300 n.mi., and the pursuit vehicle was assumed to be in a 100 n.mi. circular orbit. The number of separate burn arcs was set at two (coast-burn-coast-burn) and the initial values of the co-state vector and the lengths of arcs were chosen to correspond to values obtained in a previous study. The initial values of independent variables were extremely close to the required values, and the SWITCH algorithm converged to the solution in one iteration. Since the initialization was essentially equal to the converged solutions, the convergence properties were evaluated by deforming the final orbit into an ellipse with the eccentricity magnitude varying from 0 to .5. The pursuit vehicle orbit, vehicle parameters, and initial estimates of co-state and arc times The results are taken from reference 9 and are shown in were fixed. Table 1. Notice that the worst case required only five iterations.

Table 1. Low Altitude to Coplanar Synchronous Rendezvous Mission

Target Orbit Eccentricity	lst Coast Arc (sec)	lst Burn Arc (sec)	2nd Coast Arc (sec)	2nd Burn Arc (sec)	Number of Iterations to Converge
0	399.83	255.82	18,729.51	129.11	1
.05	401.16	253.47	17,572.70	134.87	3
.1	402.48	251.14	16,541.83	140.57	3
.5	412.62	232.95	11,155.52	184.04	5
First itera- tion speci- fications for all cases	400	255.82	18,727.46	129.11	

Although the SWITCH algorithm has not been subjected to the stringent guidance simulations that are necessary to prove the flight worthiness of an onboard guidance scheme, it is felt that the excellent convergence properties of the SWITCH algorithm and the speed per iteration (one quarter second per iteration on a CDC 6600 computer) of the algorithm make it applicable for onboard guidance. The computer requirements for SWITCH are greater in terms of speed and storage than for OPGUID; however, they are not considered to be excessive. It is estimated that the SWITCH algorithm would require 7,000 storage locations for onboard implementation.

Assuming a state-of-the-art type of flight computer, the guidance cycle time (time for complete converged computation of new optimal guidance command time history) would be approximately 2 seconds.

C. MASCOT

The MASCOT guidance algorithm is an extension of the SWITCH and OPGUID formulations. It can be reduced to the SWITCH algorithm by eliminating the aerodynamic forces, and it can be reduced to the OPGUID algorithm by eliminating both the aerodynamic forces and the multi-burn logic. Therefore, the results presented for OPGUID for ascent to orbit (vacuum), and the orbit transfer and rendezvous results obtained with SWITCH are indicative of MASCOT for these types of missions. Results for atmospheric flight are preliminary and it remains to be shown that the MASCOT scheme possesses the speed and reliability for onboard guidance for atmospheric flight. As mentioned earlier, studies to determine the properties of MASCOT are underway and will be documented as soon as results are available.

The need for a shuttle guidance scheme with the sophistication of MASCOT is demonstrated by the performance results presented in Table 2.

TABLE 2

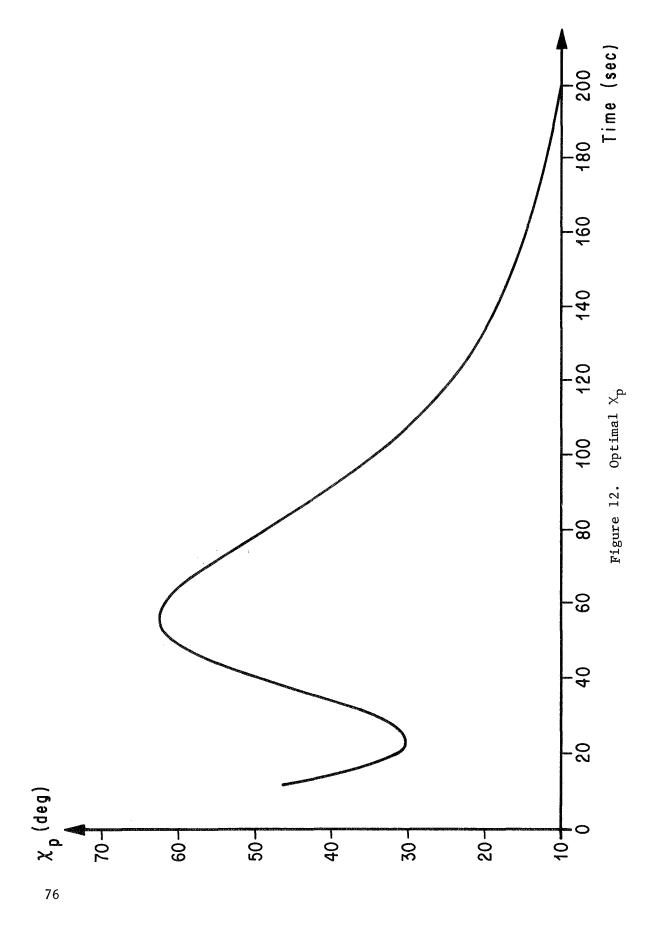
Case	Time of Max Q (sec)	Max Q (kg/m²)	Angle of Attack at Max Q (deg)	Cutoff Weight (kg)	△ Cutoff Weight (kg)
A IGM from Staging*	63	2310	0	122,259	-
B Optimal from 12 sec.	46	4087	8.0	123,380	1121
C Optimal from 70 sec.	63	2310	0	122,519	260
D IGM from 70 sec.	63	2310	0	119,706	-2553

^{*}All trajectories are zero angle of attack until initiation of IGM on optimal shaping.

The data shown in Table 2 indicate the effects on payload of optimally shaping the space shuttle trajectory during the atmospheric region of flight. Case A represents trajectory and vehicle data for a shuttle vehicle that was flown through the atmospheric portion of flight with a zero angle of attack, and the IGM steering logic was used to shape the remaining portion of the trajectory. Case B represents data obtained by shaping the trajectory with the MASCOT logic from 12 sec after lift-off through orbit insertion. This gain in payload of 1121 kg may not be fully obtainable because shaping the trajectory during the atmospheric portion of flight will result in increased structural loads. Case C represents data that were obtained by shaping the trajectory with the MASCOT logic from 70 seconds (7 sec after maximum dynamic pressure) after lift-off through orbit insertion. This increase in cutoff weight of 260 kg is potential payload since the maximum dynamic pressure is the same as in case A. More important than the 260 kg increase in payload is the fact that using MASCOT to guide the vehicle from 70 sec (or earlier) provides closed-loop guidance early in flight, and thus the effects on payload of perturbations (winds, thrust variations, etc.) during the first 70 seconds of flight can be minimized. The results of using IGM for closed-loop guidance at 70 sec is shown in Table 2 as case D. This loss in payload of 2553 kg is due to the following: (1) atmospheric forces are not modeled in IGM, and (2) the optimal steering angle during the atmospheric portion of flight is nonlinear (IGM is a linear steering law). Shown in figure 12 is the optimal steering angle versus time for case B. Notice the nonlinearity from 12 sec to approximately 130 sec. This indicates that linear steering laws are far from optimal and should not be used for guidance in this region of flight even if atmospheric forces are included in the guidance equations.

There are no significant results to report for the reentry phase. Early computations have shown a very high sensitivity of the reentry trajectories to the choice of the initial values of the Lagrange multipliers and consequently a very poor convergence rate. However, recently the approach outlined on pages 25 and 26 has been implemented in order to eliminate this high sensitivity and poor convergence. This method assumes that $\bar{\mathbf{u}}(t)$ could adequately be represented as a linear function of time during the atmospheric portions of flight.

Studies are currently underway to determine whether it will be necessary to use the solutions so obtained as first approximations to the true optimum. Presently, no further corrections appear to be necessary.



VIII. CONCLUSIONS

Fast, efficient, compact trajectory algorithms for a total trajectory from lift-off to landing have been developed using a numerical solution of the optimization boundary value problem. These algorithms use a rapid numerical integration routine and an efficient iterative solution of the simultaneous nonlinear equations involved. The implementation of one of these algorithms (using the available vastly improved on-board flight computers) would accomplish a major advance in guidance techniques. That is, preflight analysis would be reduced to a minimum, thus making it possible to achieve Shuttle launches with airline type of turnaround times. Also, special tuning constants and functions (which have heretofore been necessary to account for approximations introduced to simplify onboard computations) would be eliminated. Thus, this proposed guidance system would produce (on board the vehicle) optimal trajectories for an extremely wide variety of missions and vehicle characteristics.

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APPENDIX I

COMPUTER PROGRAM LISTING
FOR PARAMETER OPTIMIZATION DECK

HAIN PROGRAM

STORAGE USED: CODE(1) 003010; DATA(0) 002321; BLANK COMMON(2) 000000

COMMON BLOCKS:

0003 ATMO 000112
0004 ENDCDN 000054
0005 RKINTG 000554
0007 CONST 000103
0010 AERO 000156

EXTERNAL REFERENCES (BLOCK, NAME)

0011 TANGL 0012 DEQ 0013 PRINT 0014 RK713 0015 PROUND 0017 SIMEQ 0020 NINTRS 0021 NIDCS 0022 NIOLS 0024 DSQRT 0025 DSIN 0025 DSIN 0027 NIOLS STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

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002003	002085	002177	002245	302342	002515	002675	000071	000345	002473	002573	003000	001370	001416	001443	001633
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10046	10326	10676	11266	11706	12306	13616	14156	2146	350L	490L	5536	610F	640F	6716	720F
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ė.		IMEN	SION	50)	0X (5C	¥	13),	BETA	TA(13,12),), CH(13),	, AB(3	=	<	N; (
*		IMEN	SION	(S)									⋖ '	r) :			
មា		IMER	S10N	1(3)	U(3)	, ALB(3),	m	, c	(3)	000(3)			⋖ ·	3 * (
9		IMEN	NOIS)B(3),	χ. ×	08(3), RVR(3)	(3)						⋖ •	n ·			
7		ME	SION	0 (3)	× >	1(3) VRV		:	•		. (1991)			0 r			
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7		ME	2015	XI(6);	UXEC	JXE(3), UYE(3	=						< •				
~	_	MEN	NO S	- 1	, AL,	10(7)		:					∢ •	- :			
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AI7,AI8,A19,A20,A21,A22,A23,B0,B1,B2,B3,B4,B5,B6,B7,B8,D1,D		COMMON /ENDCON/ RC, AMC, C.HC, RCIHC, SKAD, SCRAD, RUB, KX, UB, RK, UTE, UTE		COMMON /RKINTG/ BETA, ALPH, CH	COMMON /DIFERS KYR.PRES,VRM,DB.ETA,RE,U.ALB.CA,ACH.WKG,ALT,RHO.A.	IFA, BEDA, CLAST WAR, VS	COMMON /CONST/ GM.PHIL. AZ. KCONV. AREA. BE. UM. AA.F. U. FH.FU. KISP. KMD. E.	14,UG,UGD,TO,FS,PG,WKGG,HEATC,CKI,CKZ,CK3,RCURV,AB,RLGU,ICNVG	COMMON /AERO, ACLA,ACA,AETA	IO READ 790, GM, TI	READ 790, (XI(1), Im1, 6)	READ 790, TF. DTP. FPT	ALGO SHOULD BE THE LONGITUDE OF THE LAUNCH SITE WHEN TI IS REFEREN	RARILY SET	SITUDE	READ 790, PHIL, AZ, RLGO	READ 790, FS. RISP. RCURV	FS MUST BE IN NEWTONS#KG.M./SEC2	READ 790, WKGO,AREA,EXA	READ 790, ALFG, BETG, HEATC	READ 790, UOD	READ 790, CK1, CK2, CK3	READ 790, RC, AMC, THC		PRELIMINARY COMPUTATIONS AND DEFINITION OF CONSTANTS		20 X (1) = X (1)	TEATCATC ACCAV	N. G. B. W. G. D. S. C.	C. C		LOTAL ALBERT OF		RCONV = 1745329252E-01		RCTHCHRC+CTHC	SINADBSIN (RAD*RCONV)	CRAD#COS(RAD#RCONV)	OVANDA MANA WARANA WARA		>	アンチョン・インシャン・ファン・アン・アン・アン・アン・アン・アン・アン・アン・アン・アン・アン・アン・アン	FIX. 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	FDE7.875E-06	POW1.01328E+05	CONSTANTS FOR ATROSPHERIC SUBROUTINE	039E	A1=6356•77	•		-	A5#284.01768
													U	, ,	, ,	•		U							Ü																					U						
16*	*/-	* 60 (*	20*	51*	22*	23*	24*	25*	56*	27*	28*	29*	30*	3.	32*	33*	* T C	35	36*	37*	38*	39*	*0	*	45*	4 3 *	\$ T	4. 10.	* :	* C	* *	• 4 • C	* * ·	25	53*	5.4 *	* 53	\$ 9 I	57		1 4	* *	*24	63.	* * 9	9.59	*99	67.	68	•69	40
91100	00116	21100	21100	00120	00121	00121	00122	00122	00123	00124	00130	00136	00136	00136	00136	00143	00150	00150	00155	00162	00167	00175	00202	00200	00201	0021.3	00216	00220	00221	00222	00223	00226	06200	00230	00232	00233	00234	00235	00236	00237	00240	11700	00243	2004	00245	00245	00246	00247	00250	ıΩ	00252	4000

D4=+A0187430086E+03 CONSTANTS FOR INTEGRATION SUBROUTINE D2=+.2021698826JE=01 D3=+.58033445891E+01 86##3.550162735E#08 82==1.266010595E=01 84mm5.104746533E-04 B7m1.014102927E-10 B8m1.124449619Ew13 D1m3483.6763560 80=2.824793081E+02 81=5.240572992 B3#1.873293836E#02 85*6.050186406E-06 A21=1.2844040E-04 A22=0.025387008 A12#1.6002310E-04 415=1,1637071E-03 418=5.5628920E-05 49=8.3168074E-04 CH(12)#410/8400 CH(13)#CH(12) ALPH(2)#20/270 ALPH(3)#10/90 BETA(2,1)=2./27. 3ETA(3,1)*1./36. A10=0.037777365 A16m0.038184967 A17m3.6184094 411=0.56467830 ALPH(4)=1./6. ALPH(5)#5./12. ALPH(9)=2./3. ALPH(10)=1./3. CH(6) #34,/105. A13=189.52010 A19#420.11368 420=45675.466 A23#5.3327146 DO 60 181,12 00 50 481,12 8ETA(1,0)*0. ALPH(1)*0. CH(9) #9./280. CH(10)#CH(9) ALPH(7)=5./6. 4LPH(8)=1./6. A14m9665.295 18=924 13600 A7=29.895060 4LPH(11)=1. CH(8)=CH(1) ALPH(13)=1. ALPH(6) = .5 50 0,9 u 102* 0 4 + 0 5 + 0 6 + 22. 101 110* 194 0.8 *601 118* 00260 00261 00262 00264 00264 00265 00270 00270 00272 00273 00301 00303 00304 00304 00306 00306 00310 00331 00333 00334 00334 00336 00336 00256 00257 00312 00316 00321 00323 00324 00326 00327 00342 00343 00344 00345 00350 00347

00352	128*	ETA(4,1)=	
00353	129*	ETA(5,1)=	-
00354	130*	8ETA(6.1)**05	-
LC I	131*	ETA(751)	
00356	132*	8,118	
an .	* * * * * * * * * * * * * * * * * * *	•	-
00360	***	DELACTO 10 0 10 10 10 10 10 10 10 10 10 10 10 1	
0 4	136	ひにしてしていると、「これのできなっている」というでは、これのできない。「これのできない」とのでは、「これのできない」とのできない。「これのできない」というできない。「これのできない」というできない。	•
00363	137*	0711-7 (13-1) 21-177 - (4100 -	-
36	138*	BETA(3,2)=10/12	-
036	139*	BETA(4,3) ml./8,	
00366	*0+1	SETA (50.3) #1250 / 16.	۰.
00367	* * * * * * * * * * * * * * * * * * * *		
00370	1124	Dr C.O L B C. B	•
00372	* * * * * * * * * * * * * * * * * * * *	のは、これでは、これでは、これでは、これでは、これでは、これでは、これでは、これで	-
00373	45*	BETA(10.4) #23./108.	
00374	146.	11,41=341./16	A 145
00375	147*	BETA(13,4)#BETA(11,4)	
00376	+80+	BETA(6,5)=.2	
00377	+6+	BETA(7,5) = -65-/27	# P 0
00400	05.	ONLAN (0.00) (0.00) (0.00) (0.00) (0.00) (0.00)	-
00401	# C	u	
20400	* * * * * * * * * * * * * * * * * * * *	CC1/40/ATT/C10	•
70700	9 7 11	### ### ##############################	• =
		A12/10/10/10/10/10/10/10/10/10/10/10/10/10/	-
20400	*95	ウロー・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・	
00400	157*	BMTA (9.9.) 11 10 10 10 10 10 10 10 10 10 10 10 10	_
00410	158*	BETA(10,6)#3110/54.	_
00411	159*	DETA(*1.6.5)#1301*/82*	
21400	160*	2,6) ==6./41.	
U	161*	BELIA: 6.0 # 1286 - 782.	
*****	162*		• •
51400	1634	56776(40,000,000,000) 86778(40,000,000,000)	107 103 103
2 7 7 7 7	454	print (1 - 2) # 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	7
00420	*991	?	
00421	167*	DDTA(10+7)#2190+/4100+	_
00422	168	00 x 00 00 00 00 00 00 00 00 00 00 00 00	
00423	169*	00F14	•
17700	1710		
00426	172*	BELY (1919) - (907)	
00427	173*	BETA(10,9) 4+1./12.	_
00430	174*	BETA(11:9) #45./164.	⊸ .
00431	175+	BETA (12.9) #3./41.	
~ 6	176*	ETA(13:9)#33:/164	
7	177	1	• •
00434	178*	SETA(12+10)#6+/*!*	-
7 6	• 6 6 6		-
2 4		1211211	
2 4	• •	AFTA(1) #+ 52824387840394170+0	_
4	183.		_
) -		

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ACLA(10) =+915755148355840+00

ACLA(12) =+072129518952596290-02

ACLA(13) =-12294753407821840-02

ACLA(14) =+07212951981620-04

ACLA(14) =+07638625991981620-05

ACLA(16) =+0928566013174290-07

ACLA(16) =+092866013174290-07

ACLA(19) =+1640220159045380-12

ACA(1) =+1640220159045380-12
                                                                                                                                                                                                                                                                                                                                                                                COMPUTATION OF UNIT NORTH VECTOR
                                                                                                                                                                                                                                                                                                              ACA(12)=-,16272810574930570+01
ACA(13)=+,54856065063887020+00
ACA(14)=-,11125040668147750+00
ACA(15)=+,13269270447635840=01
AETA(4)=+.10024147200441290+00
                AETA16) =- . 2636214482473858D=01
                                                                                                                                                                                                                                                                                                                                                ACA(16) == 8560501350938220D=03
                                                                                                                                                                                                                                                                                                                                                       ACA (17) 0+.22986787609456220-04
                                                                                                                                                                                                                                                                                                                                                                 ACA(18184,35797751349875750-08
        AETA(5)=+.5419612944522060D=01
                                                                                                                                                                                                                                                                                               ACA(10) == .26711392560709270+J1
                                                                                                                                                                                                                                                                                                      ACA(11) =+.28669953597117300+01
                                                                                                                                                                                                                                                    ACA(5) =+,7095634473294292D-02
ACA(6) =-,1385831579493185D-02
ACA(7) =+,1624012522715024D-03
ACA(8) =-,103985092539231D-04
ACA(9) =+,2789363503859551D-06
                                                                                                                                                                                                                                                                                                                                                                         ACA (19) #+.21465237039583810-1
                                                                                                                                                                                                                            ACA(2)=-,43698023555896010-01
ACA(3)=+,44065632282319390-01
ACA(4)=-,22608357082153220-01
                                                                                                                                                                                                                                                                                                                                                                                          RPHIL*PHIL*RCONV
                                                                                                                                                                                                                                                                                                                                                                                                                          SIP=SIN(RPHIL)
                                                                                                                                                                                                                                                                                                                                                                                                                                                   AB(2)##COP#SIA
AB(3)#COP#COA
                                                                                                                                                                                                                                                                                                                                                                                                 RAZ = AZ * RCONV
SIA = SIN(RAZ)
                                                                                                                                                                                                                                                                                                                                                                                                                   COASCOS (RAZ)
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1 239	1 240	1 241	1 242	1 243	1 244	245	9+2	/ 2 /	249	250	1 251	1 252	1 253	254	662	4 257	1 258	1 259	A 260	7 261	262	246	265	A 266	A 267	7 268 268	270	271	1 272	A 273	274	1 276	1 277	278	280	1 281	282	283	285	4 286		288	289	290	262	1 293	1 294
VECTORS NEEDED FOR DOWN RANGE AND CROSS RANGE IN PRINT SUBROUTINE A	(XC) **(5) *X(5) *X(5) *X(3))	RXVOR(1)#X(2)#X(3)#X(5)	AN CONTRACTOR OF THE CONTRACTO	7X VOB (3) 4X (1) 4X (2) 1X (1) 4X (2)	RXVO=SQRT(RXVOB(1)++2+RXVOB(2)++2+RXVOB(3)++2)	DO 70 I#1+3			7VR(「	COMPUTATION OF UD BAR IN TERMS OF ALFG AND BETG		VRO(2) #X(5) = OM = (AB(3) = X(1) = AB(1) = X(3))	VRO(3) #X(6) +OM+(AB(1) +X(2) = AB(2) +X(1)	VRDDESGRT(VRD[1]*VRD(1)+VRD(Z)*VRD(3)*VRD(3)*	CEC>\\\ CEC>\\\\ CCC\\\\ CCC\\\ CCC\\ CCC	-	VXRO(2)=VRO(3)+X(1)=VRO(1)+X(3)	VXR0[3]=VR0[1]+X(2)=VR0(2)+X(1)	VXRMD=SQRT(VXRO(1)*VXRO(1)+VXRO(2)*VXRO(2)+VXRO(3)*VXRO(3)		_	XXVU(1)=VXXU(Z)=VXVU(3)=VXXU(3)=VXXU(Z)=VXVU(Z)	VRVO(3)=VXRO(1)=VRO(2)=VXRO(2)=VRO(1)	ALTERBALTGERCONV	ETGR#BETG+RCONV	THE TOTAL OF US DAY CORTONALIONS		× × × × × × × × × × × × × × × × × × ×	STEL STEL STEL STEL STEL STEL STEL STEL	24-10-12 cm-10-12 cm-		I CNVG=0				00	SNOCT A FILL OF SOUTH	20 (S0#51\C0ETGR\				CO	NNG	CNATHUC(:)+VRO(:)+UB(2)+VRO(2)+UB(3)+VRO(3)	SNAL#SQRT(1CNAL@CNAL)
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240*	241*	242#	243	244	245*	246*	247*	248	2494	25.14	252*	2534	254*	255*	256	257*	259*	260+	261*	262	263*	** 97	265	267*	268*	269*	270*	27.2	273*	2740	275*	277	278*	279*	280*	282*	283*	28 t	20 0 20 0 20 0 20 0	287*	288	289*	290*	291*	292	294	295*
00527	0.500	00831	00532	00533	00534	00535	00540	00541	00543	1 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	00545	94500	00547	00520	00551	00552	00557	09500	19500	00562	00563	00564	07500	00572	00573	90574	1,400	2/500	00577	00900	00601	20900	90900	50900	00000	20900	21900	00615	00013	00620	00621	00622	00623	92900	00630	00632	00633

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344
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                                                                                                                                                                                                                                                                                                                                                                      347
                                                                                                                                            START OF NEWTONS ITERATION WITH LOGIC FOR WEIGHTING FACTORS
                                                                                                                                                                                                                                                                                                                                                                             PUWU(1,1)=CSA+(CB+VRVO(1)+SB+VXRO(1))=SA+VRO(1)
PUWU(1,2)=SA+(CB+VXRO(1)+SB+VRVO(1))
                                                                                                       CALL RK713 (T.TF, DTP, TOL, X, X, SO, 300, M)
                                                                                                                                                 CALL BOUND (X,TF,DX,B,ERR)
PRINT 600
PRINT 610, B,ERR
PRINT 620, RC,AMC,THC,RAD,XRAD
IF (ERR-BTOL) 430,430,140
IF (NT-MAXNT) 150,580,580
                                                                                                                                                                                                                                                                                                                                            710, VPRI, VPRZ, VPR3, VPR4
      CALL TANGL (SNAL, CNAL, ALFGR)
CALL TANGL (SNBE, CNBE; BETGR)
                                                                                                                                                                                                                                                                                                                                                                 CALL PBOUND (X,TF,DX,PBUAT)
                                  SB=SIN(BETGR)
CSA=COS(ALFGR)
CB=COS(BETGR)
END OF UO BAR COMPUTATIONS
                                                                                                                                                                                                                                                                       UGD(1)*UGDS(1)-DU(1+2)•AK2
                                                                                                                                                                                                   IF (ERR-ERRP) 170,190,190
                                                                                                                                    END OF TRIAL INTEGRATION
                                                                                                                                                                                                               IF (AK-AKU) 230,230,180
                                                                                                                                                                                                                                            IF (AK+AKL) 200,210,210
                                                                                                                                                                                           IF (NT-1) 230,230,160
                                                                                                                                                                                                                                                                                     ALFGR=AFGRS=DU(1) *AK2
BETGR=BTGRS=DU(2) *AK2
                                                                                                                                                                                                                                                                                                  PRINT 630, AK, TOL, WF
VPR1=AFGRS/RCONV
                                                                                           CALL PRINT (TI,X,DX)
T#TI
                                                                                                                              CALL PRINT (TF, X, DX)
                                                                                                                                                                                                                                                                                                                                                          PRINT 630, AK, TOL, WF
                                                                          CALL DEG (X,TI,DX)
                                                                                                                CALL DEG (X,TF,DX)
              ALFGR = ALFGR * RCONV
                    BETGR .. BETGR .. RCONV
                                                                                                                                                                                                                                                                              TF=TFS-DU(6) *AK2
                                                                                                                                                                                                                                                                                                                 VPR2=ALFGR/RCONV
VPR3=BTGRS/RCONV
                                                                                                                                                                                                                                                                                                                              VPR4=BETGR/RCONV
                             SAMSIN(ALFGR)
                                                               00 130 1=1,6
                                                                                                                                                                                                                                                                                                                                                                        00 240 1=1,3
                                                                                                                       PRINT 810, M
                                                                                                                                                                                                                                                                DO 220 1=1,3
                                                                                                                                                                                                                                                                                                                                                                                            00 250 1=1,5
                                                                      X(1)=X1(1)
                                                                                                                                                                                                                                                                                                                                     PRINT 700
PRINT 710,
                                                                                                                                                                                                                              GO TO 230
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                                                                                                                                                                                                                                                         AK2#AK*AK
                                                                                                                                                                                                          AK=2.+AK
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                                                                                                                                                                                                                                                                                                                                                       THE COMPUTED CORRECTIONS ARE ADDED HERE AND THEN A NEW TRIAL START
AT 100
                   PBU(6,1) = X(44+1) = WF
PBU(6,7) = (CK1 = RMD + CK2 = DX(7) + CK3 = DX(8)) = WF
                                                                                            PRINT 640
PRINT 690, ((ACM(1,J),J#1,6),1#1,5)
BBM(6)#(CK1*WKG+CK2*X(7)+CK3*X(8))*WF
                                                          ACM(I.J)=ACM(I.J)+PBU(I.K)+PUWU(K.J)
DO 290 Imi.6
                                                                                                                                                                                      DO 360 1#1.6

AM(1.4)#0.

AM(1.4)#0.

BO 360 34 Kin.6

AM(1.4)#AM(1.4)+ACM(K.1)+ACM(K;J)
                                                                                                                                                                          ACM(6,0)=ACM(6,0)/ABS(BBM(6))+1
                                                                                                                                                      IF (ABS(BBM(6))-1) 350,350,330
BBM(6)-1888M(6)/ABS(BBM(6))
                                                                                                                                         ACH(1,0)=ACH(1,0)/ABS(B(1))#+1
                                                                                                                      IF (ABS(B(I))=1) 320,320,300
B(I)=+1+B(I)/ABS(B(I))
                                                                                                                                                                                                                                                 DO 380 J=1,6
0 BM(I)=BM(I)+ACM(J,I)*BBM(J)
CALL SIMEQ (AM,DU,BM,6)
PRINT 650
PRINT 690, AM
PRINT 640
PRINT 640
                                                                                                                                                                                                                                                                                                                                BM(I)#BM(I)+WW.I,J)+DU(J)
                                                                              ACM(1, J+2) #PBU(1, J+3)
ACM(1,6) #PBU(1,7)
       PBU(1,4) #PBUAT(1,4)
                                                                                                                                                                                                                                                                                                                                      PRINT 680
PRINT 690, BM
                                 DO 270 1m1,6
DO 270 Jm1,2
ACM(1,J)#0,
DO 270 Km1,3
                                                                                                                                                                                                                                                                                                     PRINT 690, DU
DO 390 I=1,6
                                                                                                               DO 320 Im1,5
                                                                                                                                                                                                                                    00 380 1#1,6
              00 260 1=1,6
                                                                         00 280 3=1,3
                                                                                                                                     00 310 J=1+6
                                                                                                                                                                    00 340 Jal,6
                                                                                                                                                                                                                                                                                                                         DO 390 J=1.6
                                                                                                                                                                                                                                                                                                                                                                        400 1=1,3
00 250 J=1,7
                                                                                                                                                                                                                               88M(1)=8(1)
                                                                                                                                                 CONTINUE
                                                                                                                                                                                                                                                                                                                                                     AK2=AK+AK
                                                                                                                                                                                                                                            BM(1)=0.
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ALSO THE MATRIX PARTIAL OF X WITH RESPECT TO XO IS OBTAINED BY
NUMERICAL INTEGRATION SO THAT SOME LAMBDAS CAN BE COMPUTED WHICH
BE USED AS FIRST GUESSES FOR AN OPTIMIZATION PROGRAM
PRINT 730
                                                                                                                                                                                                                                                                                  CALL RK713 (T.STEP.DTP,TOL,X.X,50,100,M)
IF (LCH) 530,530,540
                                                                                   PRINT 710, VPR1,VPR2,VPR3,VPR4
IF (ERR-.05) 410,410,420
TOL*.5E--06
       UOD(1)=U0D(1)-DU(1+2)*AK2
                                                                                                                                                                                                                                                                  IF (TF-STEP) 510,510,520
                                                                                                                                                                                                                         F (TF-FPT) 470,480,490
                                     ALFGR#ALFGR*DU(1)*AK2
Betgr#betgr*du(2)*AK2
                                                                                                                                                                                                        CALL PRINT (TI,X,UX)
T#TI
                                                                                                                                                                                                                                                                                                          PRINT 740. M
CALL PRINT (T.X.DX)
                                                                                                                                                                                                                                                                                                                                  CALL DEG (X,TF,DX)
                                                                                                                                                                                             CALL DEG (X,TI,DX)
                                                                                                                                                                                                                                                                                                    CALL DEQ (X,T,DX)
                                                      VPR1=AFGRS/RCONV
VPR2=ALFGR/RCONV
                                                                  VPR3=BTGRS/RCONV
                                                                        VPR4=BETGR/RCONV
                               TFETF-DU(6) *AK2
 (1) don=(1) sdon
                                                                                                                                                   1CNVG#1
DO 440 [#1,6
X(1)#XI(1)
                                                                                                                                                                      00 450 I=7,50
                                                                                                                                                                                 00 460 1*1,6
             AFGRS=ALFGR
                    BIGRS=BETGR
                                                                                                                                                                                       X(2+7+1)=1.
                                                                                                                                                                                                                                                            STEP #T+DTF
                                                                              PRINT 700
                                                                                                                                                                                                  PRINT 800
                                                                                                                                                                                                                                                                                                                       GO TO 500
                                                                                                           GO TO 100
                                                                                                                                                                                                                                                      GO TO 520
                                                                                                                                                                                                                                     LCH#1
CONTINUE
                                                ERRPMERR
                                                                                                     CONTINUE
                                                                                                                                                                                                                                                                                                                             CONTINUE
                                                                                                                                                                                                                                                 STEP=FPT
                                                                                                                                                                           X(1)=0.
                                                                                                                                                                                                                                                                              STEP#TF
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                          TFS#TF
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SUBROUTINE PRINT ENTRY POINT DOIZOL

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EXTERNAL REFERENCES (BLOCK, NAME)

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STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

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899 99 SCHI=(U(1)+VXR(1)+U(2)+VXR(2)+U(3)+VXR(3))/VXRM CCHI=((U(1)+X(1)+U(2)+X(2)+U(3)+X(3))+VRM2+VDX+UP3)/VXRXV CALL TANGL (SCHI,GCHI,BEDA) SCHI=(SCHI+SCHI+CCHI+CCHI) 1F (SCHI) 120,130,130 CCHI=ROB(1)*X(1)+ROB(2)*X(2)+ROB(3)*X(3)
CALL TANGL (SCHI,CHIR)
CCHI==(X(1)*RXVOB(1)+X(2)*RXVOB(2)+X(3)*RXVOB(3))/R CALL TANGL (SCHI, CCHI, PANG)
RANGE WILL BE WRONG IF RANGE ANGLE > 180 DEGREES
SCHI=RVR(1)*X(1)*X(1)*RVR(2)*X(2)*X(3)*X(3) CALL TANGL (SCHI, CCHI, ALFA) CCHI=(X(1)+0X(1)+X(2)+0X(2)+X(3)+0X(3))/(R+V) AJ=CK1+WKG+CK2+X17)+CK3+X18) COMPUTATION OF VECTORS NEEDED FOR LONGITUDE UP3#U(1)*VR(1)+U(2)*VR(2)+U(3)*VR(3) IF ((PHIR=360.)+.5E=04) 190:180:180 CD=CA+2.*ETA*CLA*(1.*CCHI)*CLA UXE(2)=COA+SIWT+SIA+SIP+CWT UYE(2) #COA+CWT-SIA+SIP+SIWT UYE (3) #SIA #CWT +COA #SIP #SIWT UXE(3)#SIA#SIWT*COA#SIP#CWT SCHI#(1,#CCHI#CCHI) IF (SCHI) 140,150,150 IF (SCHI) 160,170,170 PHICEATAN (CCHI/SCHI) SCHI=(I+=CCHI+CCHI) RANG=RCONV+RE+PHIR VXRXV-SQRT (VXRZX) RPHIL=PHIL+RCONV UYE(1) == COP + SIWT SCHI = SQRT (SCHI) SCHI - SQRT (SCHI) SCHI # SGRT (SCHI) SIPESIN(RPHIL) COP=COS(RPHIL) UXE(1)=COP+CWT CCHI #UP3/VRM SIAMSIN(RAZ) COAMCOS(RAZ) XRNG PHIC * RE RAZ=AZ*RCONV WT=0M*(T-10) SIWT=SIN(WT) CL=CLA * SCHI CWT *COS (WT) CONTINUE CONTINUE CONTINUE CONTINUE SCHIMO. SCH 1 *0. SCHI #0. 140 180 u v 92* 100 103* 5 00 00 10 00 00 * 49 924 * 69 70* 71* 72* 73* 15 76* 82* 85 86. 90. 96 97 98 98 * 02 *09 *99 18 464 00 88 * 7 6 95 *66 00215 00216 00216 00252 00262 00271 00177 00214 00225 00226 00227 00230 00242 00250 00267 00270

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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    290 FORMAT (6H WKG meile:11,2X,5HVRX meile:11,2X,5HVRY meile:11,2X,5HVRZ

1 meile:11,6H VR meile:11,2X,5HUX meile:11,2X,5HUY meile:11,2X,5HUZ

2 meile:11,6H VR meile:11,2X5HUX meile:11,2X,5HUY meile:11,2X,5HUZ

3 meile:11,7,6H ALFAmeile:11,2X,5HUZ meile:11,2X,5HUY meile:11,2X,5HUZ

4 HDFZ meile:11,7,6H RRAmeile:11,2X,5HCZ meile:11,2X,5HUZ meile:11,2X,5HUZ meile:11,7X,5HUZ meile:11,7X,5HUZ meile:11,2X,5HUZ meile:11,7X,5HUZ meile:11,2X,5HUZ meile:11,2X,5HUZ meile:11,2X,5HUZ meile:11,7,6H RRAmeile:11,2X,5HYZ meile:11,2X,5HYZ meile:11,2X,5HZ meil
                                                                                                                                                                                                                                                                                                                                                                                                                               PRINT 290, WKG, (VR(I), I=1,3), VRM, (U(I), I=1,3), ALFA, (ALB(I), I=1,3), 18EDA, (DB(I), I=1,3), AREA, CL, CD, ETA, RHO, GQ, AA, BE, OM, FJ, FH, FB, F, (AB(I 2), I=1,3), RISP, RMD, CHIP, CHIY
PRINT 300, RANG, XRNG, PANG, DCEL, PRES, UD, ACH, UDD
                                                                                                                                                                                                                                                                                                                                                         CLATESGRT(CLAT)
RLATEATAN(SLAT/CLAT)/RCONV
PRINT 280, T.R.V.GM.(X(I),I=1,3),PHIL,(X(I),I=4,6),AZ,(DX(I),I=4,6
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |=E18,11,/,6H CK1 *E18,11,2X,5HCK2 =E18,11,2X,5HCK3 =E18,11,2X,5HRC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      FORMAT (6H CDD #E18.11,2X,5HCLA #E18.11,2X,5HEXA #E18.11,2X,5HHTC
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               RANG, XRNG, PANG, DCEL, PRES, UD, ACH, UDD
CA, CLA, EXA, HEATC, CKf, CK2, CK3, RCURV, AJ, X(7), DX(7), X(8)
DX(8), RLAT, RLNG, RLGO
                                                                                                RI "GERLGO+360.- (RLNG+RCONV=0MeTO)
Ir (RLNG) 220,230,230
                                                                             CALL TANGL (SLNG, CLNG, RLNG)
                                                                                                                                                                               250,250,240
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   PRINT 340, (DX(I), 1#9,50)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            PRINT 340, (X(1), 1#9,50)
                                    CLNG*CLNG+X(I)+UXE(I)
                                                           SLNG-SLNG+X(1)+UYE(1)
                                                                                                                                                                                                                                                                            CLAT#(1.~SLAT*SLAT)
1F (CLAT) 260,270,270
                      SLAT-SLAT+X(I)+AB(I)
                                                                                                                                                            GO TO 210
IF (RLNG#360.) 2:
RLNG#RLNG#360.
                                                                                                                                          LNG=340.+RLNG
0 TO 210
   DO 200 I=1,3
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161	163	165	167	
ZRV=E18.11./.6H J =E18.11.2X.SHHT! =E18.11.2X.5HDHT]=E18.11.2X.5H B 161	320 FORMAT (6H D2 =E18-11,2X,5HLAT =E18-11,2X,5HLONG=E18-11,2X,5HLNGO = =E18-11)	BUGO PORMAT (1HO.50X.14HPXF/PUG MATRIX)	*!SHOPXF/PUD:MATRIX)	NO DIAGNOSTICS.
2RV#E18.11,7,6H J	20 FORMAT (6H D2 m 1#E18.11)	30 FORMAT (1H0,50X,	SO FORMAT (1HO, SOX,	
		166* 33		END OF COMPILATIONS
00521	00522	00523	00525	

ENTRY POINT 000336 SUBROUTINE RK713

STORAGE USED; CODE(1) 000375; DATA(0) 003033; BLANK COMMON(2) 000000

COMMON BLOCKS:

RKINTG 000554

EXTERNAL REFERENCES (BLOCK, NAME)

NEXPAS NERR35 0000 9000 STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

120L	1416	170L	2126	¥¥	DTi	7	TOUM	
	7,0000							
	1000			Ω	۵	-	٥	
1206	1401	1706	200L	«	DT	SACNI	_	
	922000							
0001	1000	1000	1000	0000	0000	0000	0000	
1126	1366	1656	20L	2416	HU		Z	
000024	940000	000154	000027	000000	000522	002740	002742	
1000	1000	1000	1000	0001	0003 0	0000	0000	
110L	1306	1606	1801	2301	BETA	is.		X D C M
741000	000054	000146	000274	516000	000000	000000	002746	002424
0001	0001	1000	1000	1000	0003 0	0000	1 0000	0000

1766 220L ALPH ER

000172

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002570

000047 1256

000130 000313 000410 002751 002741

> 9878542200987854W2 00000000000000 P(I) IS IN F(I+1,J)
> PARAMETERS FOR DEQ SUBROUTINE MUST BE STORED IN COMMON
> DIMENSIONS MUST AGREE WITH NUMBER OF DIFFERENTIAL EQUATIONS AND
> NUMBER OF CONSTANTS IN THE PARTICULAR FEHLBERG FORMULA USED
> DIMENSION F(13,50), XDUM(50), TE(50), XI(50), ALPH(13), BETA(13,12 M IS THE NUMBER OF STEPS NEEDED NISTHE NUMBER OF DIFFERENTIAL EQUATIONS KT IS MAX NUMBER OF ITERATIONS ARRAY F STORES THE 13 EVALUATIONS OF THE DIFFERENTIAL EQUATIONS SUBSCRIPTS FOR ALPHA, AND CH ARE +1 GREATER THAN FEHLBERGS FOOL IN FEHLBERGS REPORT IS IN F(1, J) IMPLICIT DOUBLE PRECISION(A-H,0-Z) SEVENTH ORDER RUNGE-KUTTA INTEGRATION WITH STEPSIZE CONTROL TF CAN BE GREATER THAN TI OR LESS THAN TI AND RK713 WILL WORK SUBROUTINE RK713 (TI,TF,DTG,TOL,XI,X,N,KT,H) COMMON /RKINTG/ BETA,ALPH,CH 00104 00103

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A=X(I)
TE(I)=DT+(F(1,1)+F(11,1)+F(12,1)+F(13,1))+41./840./A
ER=ABS(TE(1))
                                                                             DO SO JEI,NN
XDUM(I)=XDUM(I)+DT+BETA(K,J)+F(J,I)
TDUM=T+ALPH(K)+DT
                                                                                                                                                                                                                                                                                                         IF (ABS(DT)-ABS(TF-T)) 170,170,160
                                                                                                                                                                                                                             TE (ABS(TE(1))-ER) 140,140,130
FR#ABS(TE(1))
CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                     DIAGNOSTICS.
                                                                                                                                                 D0 90 I=1.N
D0 90 L=1.13
X(I)=X(I)+DT+CH(L)+F(L,I)
                                                                                                                                                                                                                                                                                   DT=AK*DTI*(TOL/ER)**.125
IF (ER-TOL) 150:150:180
                                                                                                   CALL DEG (XDUM, TDUM, TE)
DO 60 1 mi, N
                                                                                                                                                                                                                                                                                                                                                190 X(1)=XDUM(1)
200 IF (M-KT) 210,220,220
210 IF (T-TF) 20,230,20
220 IF#T
230 RETURN
                                                                                                                                                                                 IF (X(1)) 110,100,110
                CALL DEQ (X,T,TE)
                                                                                                                                                                                                                                                                                                                                                                                                     o
Z
                              F(1,1) #TE(1)
50 70 K#2,13
50 40 I=1,N
                                                                                                                                                                         DO 120 I*1.N
                                                                                                                                                                                                                                                                                                                                        N.1-1 061 00
                                                      XDUM(I) #X(I)
                                                                                                                    F(K,1)=TE(1)
CONTINUE
                                                                                                                                  DO 80 1#1,N
XDUM(1) = X(1)
                                                                     Nº 1#1 05 00
Nº 1-1 01 00
                        00 30 I=1,N
        X(1)=X1(1)
                                                                                                                                                                                                €0 TO 120
                                                                                                                                                                                                                                                                                                                                  GO TO 200
                                                                                                                                                                                                                                                                                                                           CONTINUE
                                                                                                                                                                                                                                                                                                   T#T+DT1
                                                                                                                                                                                                                                                                                                                   DT=TF-T
                                                              NN=K-1
                                                                                                                                                                                                                                                              DT1=DT
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END OF COMPILATION:

SUBROUTINE DEG ENTRY POINT 002130

STORAGE USED; CODE(1) 0021571 DATA(0) 0005561 BLANK COMMON(2) 000000

COMMON BLOCKS:

EXTERNAL REFERENCES (BLOCK, NAME)

0005 ATMOS 0006 AEROD 0007 DSGRT 0010 NERR3\$ STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

000406 001372 000174 001120 001246 001476	0000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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	000000	D 000022 D 0000224 D 00003454 D 00003454 D 00003426 D 0000226 D 0000226 D 0000226 D 0000226 D 0000226 D 0000226
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000000000000000000000000000000000000000		
	000 4 4 6 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
000504 000511 001421 001002 0011437	001726 001726 001726 0000172 0000172 0000172	D 0000014 0 0000402 0 0000420 0 0000425 0 0000404 0 000000 0 0000300 0 0000300
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- 20 W W W 4 4 A	できょう 押り こうりょ	2
000534 000727 000727 0001164 0011250		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
		000110100000000

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DIMENSION VR3), U(3), ALB(3), DB(3), UO(3), UOD(3)

DIMENSION P(6,6), PHI(6,6), PAXB(3), PVXB(3,3), PJXB(6), PMXB(6)

COMMON /DIFEO/ R,VR,PRES,VRM,DB,ETA,RE,U,ALB,CA,ACH,WKG,ALT,RHO,AL

IFA,BEDA,CLA,F,QQ,VS

COMMON /CONST/ GM,PHIL,AZ,RCONV,AREA,BE,OM,AA,FJ,FH,FD,RISP,RHD,EX

IA,UQ,UOD,TO,FS,PQ,WKGQ,HEATC,CKI,CK2,CK3,RCURV,AB,RLGO,ICNVG

R2=X(1)+X(2)+X(2)+X(3)+X(3)*X(3)
                                                                                                                                                                                                                                                                                                                        C9m(12.eFD*A&(3.eE2-1.)*B+3.eFH*BB$(1.e-7.*E2)-10.eFJ*A)*R2I
C!Om(2.eFJ+12.*FD*(1./7.e=E2)*B+4.eFH*A*BB)*RI
                                                                                                                         A=(AB(1)*X(1)+AB(2)*X(2)+AB(3)+X(3))*RI
       IMPLICIT DOUBLE PRECISION(A-H,0-Z)
                                                                                                                                                                                                              REMA*BE/SGRT(C6)
C12mRE*A*C5/C6*R1
C13mC12*A*R1
D0 50 Im1,3
PVX8(1,1)m0,
D VX8(1)m(3)*X(1)+C12*AB(1)
PVX8(1,2)m0M*AB(3)
                                                                                                                                                                                                                                                                                                            C7#(2.5#GR+1.5+B+(C1+.5#C2))*RI
             DIMENSION X(SO), DX(SO), AB(3)
                                                                                                                                                    C1=3.+FD+(1./7.+2.+E2+3.*E4)+B
                                                                                                                                                                                                                                                                                              GR#8+(FJ*(1**5**E2)+C1+C2)
GP#8+(2**FJ*A+C3+3**C4)
                                                                                                                                                                 C3#4.4FD*A*(3./7.=E2)*B
SUBROUTINE DEG (X,T,DX)
                                                                                                                                                                                                                                                                                                                   C8=2.*GP+B*(C3+1.5*C4)
                                                                                                                                                         C2=FH+BB+A+(3+-7+E2)
                                                                                                                                                                                                                                                             PVXB(1,3)#=OM+AB(2)
PVXB(2,3)#OM+AB(1)
PVXB(2,1)#=PVXB(1,2)
PVXB(3,1)#=PVXB(1,3)
                                                                                                                                                                                                                                                                                        PVXB(3,2)=-PVXB(2,3)
                                                                                                                                                                        C4=FH+88+(E2-1./5.)
                                                                   IF (R2) 10,20,20
                                                                                                                                                                                            IF (C6) 30,40,40
                                                                                                                                                                                                                                                                                                                                        C11=(1.+GR)*R1
                                                                                                                                                                              C5=AA+AA=BE2
                                                                                CONTINUE
R#SQRT(R2)
                                                                                                                                                                                                                                                                                                                                                                        60 Im1,3
                                                                                                            BEAA*AAET
                                                                                                                                                                                                                                                                                                                                                            CC2*CC1+C11
                                                                                                                                                                                                                                                                                                                                                     CC1=GM+R21
                                                                                                                                                                                                                                                                                                                                                                  CC3#CC1#GP
                                                                                                     R21=1./R2
                                                                                                                              BE2=BE*BE
                                                                                                                   BB=AA*RI
                                                                                                                                              E4mE2+E2
                                                                                                                                                                                                         CONTINUE
                                                                                                                                                                                                                                                                                                                                              C12=A+R1
                                                                                              R1=1./R
                                                                                                                                       E2=A+A
                                                                          R2=0.
                                                                                                                                                                                                  C6 # 0 .
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                           P(1+3,J)=CC1*(2.*R2[*(C7*X(1)+C8*AB(1))*X(J)=B*(C9*X(I)+C10*AB(I))
                                                                                                                                                                                                                                                                                                           CALL ATMOS (ALT.TEMP,PRES,RHO,VS,DVS,DRHO,DPRES)
ACH=VRM/VS
CALL AEROD (ACH.CLA,CA,ETA,DCLA,DCA,DETA)
F=FS+EXA*(PO_PRES)
                                                                   VR(1) = X(4) = Ome(AB(2) = X(3) = AB(3) = X(2))
VR(2) = X(5) = Ome(AB(3) = X(1) = AB(1) = X(3))
VR(3) = X(6) = Ome(AB(1) = X(2) = AB(2) = X(1))
VRM2 = VR(1) = VR(1) + VR(2) = VR(3) = VR(3)
IF (VRM2) BO,90,90,90
                                                                                                                                                                                                                                                                                                                                                                                WKGI=1./WKG
VDU=VR(!)*U(!)+VR(2)*U(2)+VR(3)*U(3)
QQ=*5*RHO*AREA*VRM2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             DO 150 Jml,3
P(1,J)=(U(1)+VR(J)+2.=VR(1)+U(J))+C7
                                                                                                                                                                                        U(1)=U0(1)+(T-T0)+U0D(1)
UM2=U(1)+U(1)+U(2)+U(2)+U(3)+U(3)
IF (UM2) 110,120,120
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       ((D)D+60+(D) # (C8 # KB (D) + C6 # C(D))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      CS=QQ+(C3/VRM+C4+VDU/VRM2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      ALB(I)=C1*U(I)+C2*VR(I)
DB(I)=C5*VR(I)
DO 150 I=1*3
                                                       P(1+3,1)=P(1+3,1)-CC2
                                                                                                                                                                                                                                                                                                                                                                   WKG#WKGO-RMD*(T-TO)
                             1+(AB(J)-C12+X(J)))
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   CCIUMC7*VDU
DO 160 [M],3
P(1,1)#P(1,1)+CCIO
                                                                                                                                                                                                                                                                                                                                                                                                                                                               C3#CA+2.*ETA*CLA2
                                                                                                                                                                                                                                                                                                                                                                                                                                   CI#QQ#CLÄ
C2##C1#VDU/VRM2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                            C4=-2.*ETA*CLA2
                                                                                                                                                  CONTINUE
VRM=SQRT(VRM2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       DO 170 Jm1,3
PHI(1,143)#0,
P(1+3,143)#0,
DO 170 Km1,3
                                                                                                                                                                               DO 100 [m1,3
                                                                                                                                                                                                                                                                                                                                                                                                                         CLA2=CLA+CLA
                                                                                                                                                                                                                                                                         DO 130 [=1,3
U(1)=U(1)/UM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CB#C6+C3/VRM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           00 140 1=1,3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             DO 170 [#1,3
                                                                                                                                                                                                                                                           UM=SQRT (UM2)
                                           DO 70 [#1,3
60 J#1,3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       C6=00/VRM2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    C7=C6+CLA
                                                                                                                                                                                                                                UM2#0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            40*62#63
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                                                                                                                                     VRM2=0.
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                                                                                   P(1+3,J)=P(1+3,J)+WKGI*(PHI(1,J+3)=P(1+3,J+3)+((ALB(I)=DB(I))/RHO*
1DRHO+ClO*U(I))*PAXB(J)*CS*PVXB(I,J)
P(I+3,J+3)=(P(I,J)=P(I,J+3))*WKGI
PHI(I+3,J+3)=*WKGI*(C7+C9)*VR(I)*VR(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    PHI(1+3,1+3)=PHI(1+3,1+3)+(T+TO)/UM
DX(1+3)==CC2+X(1)=CC3+AB(1)+(ALB(1)+DB(1)+F*U(1))*WKGI
                  P(I+3,C+3)#P(I+3,C+3)+P(I,K+3)+PVX8(K,L)
                                                                                                                                                                                                                                                                                                                                                              DX(1+3)=WKG1+(ALB(1)/CLA+DCLA+C12+VR(1))
C7=1+/(VS+VRM)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                P(1+3,0)#P(1+3,0)+DX(1+3)+PMXB(J)
P(1+3,0+3)#P(1+3,0+3)+DX(1+3)*PMXB(O+3)
PHI(1, 0+3) #PHI(1, 0+3)+P(1,K) *PVXB(K, 0)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    PHI(I+3,4+3)=1./UM=U(I)=U(J)
PHI(I+3,4+3)=(T=TG)*PHI(I,4+3)
                                                                                                                                                                                                                                                                                                             CII=C6+VRM
C12=C9+DCLA+C10+DETA+C11+DCA
                                                                                                                                                                                                                                                                                                                                                                                                                                                              DX(I)=DX(I)+VR(J)+PVXB(J*I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 PMXB(1)=C7+DX(1)-C8+PAXB(1)
D0 230 [#1]-3
D0 230 J=1]-3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        PHI(1,1+3) #PHI(1,1+3)+1./UM
                                                                                                                                                                                                  P(I+3,I+3)=P(I+3,1+3)=C12
PHI(I+3,1)=PHI(I+3,1)+C11
C7=VRM-VDU
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  PMXB(1+3) =C7+VR(1)
                                                                                                                                                                                                                                                             C8mC6*C7*2*
C9mC8*ETA*2**CLA
                                                                                                                                                                                                                                                                                                                                                                                               C8mVRM/VS*DVS/VS
                                                                                                                                                           C111=(C1+F)+WKG1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             PHI (1+3, 3+3) #0.
                                       CIO=-EXA+DPRES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              PHI (1, 1+3) #0.
                                                         DO 180 [#1,3
DO 180 J#1,3
                                                                                                                                                                                                                                                                                                                                                00 200 1=1,3
                                                                                                                                                                                                                                                                                                                                                                                                                   DO 220 I=1,3
                                                                                                                                                                                                                                                                                                                                                                                                                                                  00 210 Jali3
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                                                                                                                                                                                            00 190 1#1,3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       DO 250 I=1,3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    0 1 (7°C) HO.
                                                                                                                                                                          C12=C5+WKG1
                                                                                                                                                                                                                                                                                                C10=C8+CLA2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       P(1,1+3)=1+
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C11=C7/VRM2/VRM2
C12=VRM+(CK3+C11+(C6+4.+VRM+3.+VDU+C5)+CK2+3.*HEATC+C8)
C1=2.*CLA+(DCLA+CLA+(DETA+CA+ETA+DCA)+2.*ETA+CA+DCA)
                                                                                                                                                                                                                                                                                                    PUXB(1)=C10+PAXB(1)+C12+DX(1)+C2+PAXB(1)
PUXB(1+3)=C12+VR(1)+C2+PAXB(1+3)
DO 360 1#153
                                                                                                                                  PHI(I.C.) #PHI(I.C.) +PHI(I+0,K) #PHI(K,C+0)
P(I.C.) #P(I.C.) +PHI(I+0,K) #PHI(K+0,C+0)
DO 330 IHI.8
                                                                                               DX(I+44)=DX(I+44)+C9+VR(J)+PHI(J,1+3)
DX(I+47)=DX(I+47)+C9+VR(J)+PHI(J+3,I+3)
                                                                                                                                                                                                                                                                                      C2#CK3#C7#2*#(CA*DCA+C1#VDU/VRM+C1)
                                                                                                                                                                                                                                                                                                                                                   PUXB(1)#PUXB(1)+C9*DX(1)
PUXB(1+3)#PUXB(1+3)+C9*U(1)
                                                                                                                                                                                                                                                                                                                                      DX([) = DX([) + U(J) = PVXB(J, [)
DO 370 [= [, 3]
                                                                                                                                                                                                                                              DX(7) *HEATC+C8+VRH2+VRH
                                                                                                                                                                                                                                        DX(L) #DX(L)+P(1,K)+X(M)
                                                                                                                                                                                                                                                     DX (8) #C7 + C6 + VDU + C9 / CK3
                             C7=QQ+QQ+WKGI+WKGI
IF (RHO) 290,300,300
                                                                                                                                                            PII(I+0.C)#PII(I.C)
PII(I+0.C)#PII(I+0.C)
PII(I+0.C)#PII(I+0.C)
PII(I+0.C)#PII(I+0.C)
                                                      C9#=C5/VRM*C7*CK3
D0 310 I#1:3
C3=1.+2.+ETA+CA
                                                                                                                                                                                        PMI(1.0+3) ED.
DO 340 IN1.6
DO 340 UN1.6
                                                                                                                                                                                                                   DX(L)=PHI(I,J)
                                                                                                            DO 320 Im1,3
DO 320 Jm1,3
DO 320 Km1,3
                                                                           DX(1+44)#0.
DX(1+47)#0.
DO 310 J#1.3
              C5=CLA2*C3*2.
                                                                                                                                                                                                                                                                                              00 350 1=1,3
                                                                                                                                                                                                                                                                                                                                                                  DO 380 Im1,3
                                                                                                                                                       00 330 3=1,3
                                                                                                                                                                                                                                                                                                                                50 360 Jal,3
                                                                                                                                                                                                                                                                                                                                                                        00 380 J#I,3
                                                                                                                                                                                  PHI (1, J) =0.
                                                                                                                                                                                                            L=6+I+J+2
                                                                                                                                                                                                                                  N#4*X+7+2
                                                                                                                                                                                                                                                                                                                        DX(I)*0.
                      C6=C4+C5
                                                 CONTINUE
        C4=CA+CA
                                          RHO=0.
                                                                                                                                                                                                                                                                                                                                                                               C * 9 * X
                                                                                                                                                                                         330
                                                                                                       310
       187*
                                                                                                                                                189*
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191*
192*
193*
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                                                                                                                           186*
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        10472
                     9444
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                                                                                                                                                                                                                                                                                                                                                                  00631
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D 223
D 225
D 225
D 227
D 227
D 229
D 230
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```
00642 225* Limk+20+1
00643 226* Limk+53+1
00644 227* DX(I+44)=DX(I+44)+PUXB(J)*X(L)+PUXB(J+3)*X(H)
00644 227* DX(I+44)=DX(I+44)+PUXB(J)*X(L)+PUXB(J+3)*X(H)
00645 228* 380 DX(I+47)=DX(I+47)+PUXB(J)*X(L)+PUXB(J+3)*X(H)
00650 229* DO 390 Imi,3
00651 230* RETURN
00652 231* RETURN
00655 231* RETURN
00656 232* END
```

SUBROUTINE ATMOS ENTRY POINT 000427

STORAGE USED: CODE(!) GOOS12: DATA(O) GOO117: BLANK COMMON(2) GOODDO

COMMON BLOCKS:

0003 ATMO 000112

EXTERNAL REFERENCES (BLOCK, NAME)

0005 DATAN 0005 DATAN 0006 DEXP 0007 DSGRT 0010 NERR3\$ STORAGE ASSIGNMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)

							e N
80L A0	A 13	A 2 2		9 8	<u>.</u>	E 2	Z
0000413	0000032	000054	290000	000074	000102	900000 0	000072
33	50	55		5	33	9	0
0001	000	000	88	000	8	60	00
5 60L 5 AAD							
000375	00003	20000	90000	00007	00003	,00000	0000
		90		٥	0	٥	٥
0000	000	000	000	000	000	000	3000
15 40L 24 AAC							
000015	0000	0000	0000	0000	0000	0001	0000
2 00	500		. 6	33.0	00	33.0	5
0000	00	000	6	00	Ö	00	00
20L A A B	A 10	N 6	? 60 ₹ ₹	83	88	03	E 4
0007	0024	40000	02000	99000	00100	00100	000012
00	000	66	ō	O	0	0	00
۵	00	0	9 6	۵	٥	۵	0 0 0000

000034 A14 000046 A19 000056 A23 000016 A7 000016 B7 000010 E3

00003 00003 00003 00003 00003

D 0000020 A

0000

おいいし くちょうりょう COMMON /ATMO/ AO.al.a2.a3.a4.a5.a7.a8.a7.a8.a9.alo.all.al2.al3.al4.al 15.al6.al7.al8.al9.a20.a21.a22.a23.80.81.82.83.84.85.86.87.88.01.02 NOTE THAT FORMULAS ARE NOT ACCURATE FOR ALTITUDE OUTSIDE Ø TO 200 DRHO, DPRES, AND DVS ARE IN SAME UNITS AS RHO, PRES, AND DVS OVER SUBROUTINE ATMOS (ALT, TEMP, PRES, RHO, VS, DVS, DRHO, DPRES) IMPLICIT DOUBLE PRECISION(A-H,0-Z) VS IS IN METERS PER SECOND ALT MUST BE IN METERS TEMP IS IN DEGREES KELVIN PRES IS IN NEWTONS/M2 RHO IS IN KG/M3 Z=ALT*.001 IF (Z) 10,20,20 0 000000 00101 00103 00104 00104 00104 00104 00107 00107 00107

00112	16*	20 CONTINUE		ш	15
00113	17.	IF (Z-200.) 40.4	40,40,30	w	9 !
00116	***************************************			ш	17
00117	*6"			W	8
00120	20*			W	19
00121	21*	E1=Z+A1		u	20
00122	22*	E2=2+A3		w I	7 .
00123	23.	E3#Z-A5		W 1	22
00124	24*	E4=Z2-A70Z+A8		1	5.3
00125	25*	ES=Z2-A13+Z+A14		الطا	54
00126	26*	E6mZ2-A19+Z+A20		ועו	52
00127	27*	A=A0/E1+A2+L0G(E	A=A0/E1+A2+L0G(E2)-A4+L0G(-E3)+A6+L0G(E4)+A94ATAN(A10+Z+A11)-A1Z+L	1	97
00127	28*	10G(ES)+A150ATAN(G(ES)+A150ATAN(A16*Z-A17)+A18*LOG(E6)+A21*A1AN(A22*Z-A23)	L	/ 7
00130	29*	AAB=.018031036		نا ليا	8 6
00131	30*	AAC=+060803123		4	7 7
00132	31+	AAD=-028429767		ما لد) r
00133	32*	DAMMAD/ELOPA	DARFAD/(FIREL)+AZ/EZHA4/E3+1/+***********************************	ية ل	
00133	33*	1 A 18 * Z + A A D) / E 6		u L	7 .
00134	3.4*	DA=DA*.001		1	
96100	35+	TEMP=80+2+(81+2+	TEMP=80+Z+(81+Z+(82+Z+(83+Z+(84+Z+(85+Z+(86+Z+(87=88+Z))))))	الية	ع ا
00136	*98	DTEMP#B1+2*(2.+8	DTEMPEB1+Z*(2**B2+Z*(3**B3+Z*(4**B4+Z*(5**B5+Z*(6**B6+Z*(7**B7-8**	ш	S S
00136	37*	188*2111111		LL)	36
00137	38*	OTEMP = DTEMP + . DOI		ш	37
00140	39.	PRESHEXP(#DI*A)		نعا	8
00141	*0+	RHO=D2+PRES/TEMP		تعا	39
00142	41.4	PRESH03*PRES		ш	4
00143	42*	VS=SORT (D4+TEMP)		LL	-
00144	434	DRHO=-RHO+(D1+DA+DTEMP/TEMP	+DTEMP/TEMP)	w	42
00145	***	DVS#.S+D4+DTEMP/VS	S>	ندا	ش
00146	4.0°	DPRES=+D1+PRES+DA		w	4
00147	494	IF (ALT-200./.001)	1) 60,60,50	النا	T
00152	47*	50 AMALT-200./.001		ial :	•
00153	400	RHO*RHO+DRHO*A		1	41
00154	*6+	PRESHDPRESOA+PRES	(Sr)		3 0
00155	50 *	VS=VS+DVS+A		w	4
95100	5 1¢	60 1F (ALT) 70,80,80	•	ندا	
00161	52*	70 RHO=RHO+DRHO+ALT		W	<u>.</u>
00162	53*	PRES *PRES + DPRES • ALT	ALT	w	25
00163	54.	VS=VS+DVS+ALT		انعا	رن دن
00164	÷ ហ	80 CONTINUE		44	4.
00165	± 94	RETURN		lui '	ស ស
99100	57*	END		ш	26.
	END OF COMPILATION:	PILATION: NO	DIAGNOSTICS.		

SUBROUTINE TANGL ENTRY POINT 000124

STORAGE USED! CODE(1) 000154; DATA(0) 000031; BLANK COMMON(2) 000000

EXTERNAL REFERENCES (BLOCK, NAME)

		000	1000	
		000112 130L	0001 000037 60L	1 000000
		000	000	0000
		120L	SOL	INCP S
	E E	000103	000033	910000
	SCATION, NA	1000	1000	0000
	IVE LO	1104	401	106
	E, RELAT	000017	000021 40L	090000
	GOMMENT (BLOCK, TYPE, RELATIVE LOCATION, NAME)	0001	0001	000
	F N	1001	301	80L
DATAN Nerras	ASSIGNM	00000	210000	108 090000
0003	STORAGE ASSIC			0001

000011 20L

6 Z ± C
SUBROUTINE TANGL (SINA, COSA, A) IMPLICIT DOUBLE PRECISION (A=H, 0=Z) IF (SINA) 10,20,30 IF (SINA) 10,20,40 IF (COSA) 40,50,60 IF (COSA) 100,110,120 IF (COSA) 100,110,120 IF (COSA) 100,110,120 A=A+PI GO TO 130 A=1.5ePI GO TO 130 A=2.*PI=A GO TO 130 A=E0. A=E0. GO TO 130 A=E0.
SUBROUTINE TANGL (SINA, COSA, A) IMPLICIT DOUBLE PRECISION(A=H, PI=3,1415927 IF (SINA) 10,20,30 IF (COSA) 40,50,60 IF (COSA) 40,50,60 IF (COSA) 100,110,120 A=47PI GO TO 130 A=57PI GO TO 130 A=57PI GO TO 130 A=57PI GO TO 130 A=5PI A=5
S S S S S S S S S S S S S S S S S S S
E TANGL (S 200BLE PRE 10.20.30 40,50.60 70.80.90 100.110.1 100.110.1 100
SUBROUTINE TANGL (SI IMPLICIT DOUBLE PREC PI=3.1415927 IF (SINA) 10.20.30 IF (COSA) 40.50.60 IF (COSA) 70.90.90 IF (COSA) 70.90.90 IF (COSA) 100.110.11 Amatana (SINA/COSA) Amatana (SINA/COSA)
SUBROUTINE T THPLICIT NE T IF (SINA) 10 IF (COSA) 40 IF (COSA) 70 IF (COSA) 70 I
SUBROUTINE TANGL (SI IMPLICIT DOUBLE PREC PI=3.1415927 IF (SINA) 10,20,30 IF (COSA) 40,50,60 IF (COSA) 70,80,90 IF (COSA) 100,110,12 Amatan (SINA/(-COSA) Amatan (SINA/COSA)
11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
000 000 000 000 000 000 000 000 000 00

NO DIAGNOSTICS.

END OF COMPILATION:

SUBROUTINE AEROD ENTRY POINT 000437

STORAGE USEDI CODE(1) ODOSIOI DATA(0) ODO1711 BLANK COMMON(2) ODODOD

COMMON BLOCKS!

0003 AERO 000156

EXTERNAL REFERENCES (BLOCK, NAME)

9004 NERR35

	0000 000013 20L 0000 0 000064 A1 0000 0 000054 C2 0000 0 000060 DC1 0000 1 000050 NMC	
	0001 000306 1616 0003 D 000120 AETA 0000 D 000056 C1 0000 D 000102 DB2 0000 D00102 DB2	
ATION, NAME)	0001 000233 1526 0003 D 000000 ACLA 0000 D 000076 B2 0000 D 000100 DB1 0000 I 000053 I	
(BLOCK, TYPE, RELATIVE LOC	0001 000024 1206 0001 000057 1316 0001 0003 00005 0000 00004 00005 000050 ACA 0003 D 0000 D 0000 <td></td>	
STORAGE ASSIGNMENT	0001 000024 1206 0001 000421 80L 0000 0 000066 A2 0000 0 000070 DA1 0000 0 000062 DC2	

-	~	. m) 3	9	s S	•0 •0	r 9	æ	о	و ت	=	6 12	€	4	£ 15	6 16	6 17	6. 18	61 9	6 20	6 21	6. 22	6 23	6 24
	TO SMEROVE																							
	20																							
SUBROUTINE AEROD (ACH, CLA, CA, ETA, DCLA, DCA, DETA)	INTERCL DOUBLE PRECISION (A11) 011/2	CALL AND OF AREA CREATER.	TOWARD TOWARD A CONTRACTOR	CINTENDED STOLE ST	COMMON /AERO/ ACLA, ACA, AETA	CHURC	IF (ACH-23.0) 20,10,10	IO XSEACH	ACH#23.0		20 611)=1+0	G(2) BACH	DO 30 1*3,20	30 6(1)=6(1+1)+6(2)	C2=1.+ACA(19)+6(11)+ACA(18)+6(10)	C. BACA (9) & G (9)	001#0	DC2#10.*ACA(19)*G(10)+9.*ACA(18)*G(9)	00 CF 00	C2=C2+ACA(1+9)*G(1+1)	C. #C. + ACA(1) * G11)	DC1#DC1+1+ACA(1+1)+G(1)	40 DC2#DC2+1+ACA(1+9)+G(1)	CA#C1/C2
		, (,																					
,	* *	1 4		s	* 9	7.	80	•	•	=	12*	134	1 40	15	+9=	17*	*8	*61	20*	21+	22*	23*	2#	
10100	0000			100	20100	00100	00100	00112	00113	4 1 100	00115	00116	00117	00122	00124	00125	00126	00127	00130	00133	00134	00135	00136	00140

SUBROUTINE SIMEQ ENTRY POINT 000447

STORAGE USED: CODE(1) 000500; DATA(0) 000231; BLANK COMMON(2) 000000

			0001 000324 140L 0001 000334 170L 0000 0000000 D 0000 1 000133 1P1 0000 1 000126 NM1	
			1256 2056 300 300 300 300 300 300 300 300 300 30	6 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
			0000116 0000213 0000164 0001134	
			00000	S THE CAND T
			000001	FORM ABEC WHERE B IS THE A AND THE VECTORS B AND C
			MR 1121	AB
			0000070 0000152 0000130 000130 000131	TA POST A
		NAME	000000	hi
		RELATIVE LOCATION, N	00001	SUBROUTINE SIMEQ (A,B,C,N) IMPLICIT DOUBLE PRECISION(A*H,0~Z) DIMENSION A(6,6), B(6), C(6), D(6,6), E(6) THE EQUATION TO BE SOLVED MUST BE IN THE FORM ANSWER RETURNED A STATE RETURNED THE ROUTINE WORKS WHEN A IS SINGULAR IF THE S) DO 20 I=1,N DO 130 I=1,N IF (RECOMM) 90,50,90 DO 60 J=1,N IF (E(1)) 200,60,200 CONTINUE DO 80 J=1,N DO 70 L=1,N DO 10,20,D=1,0
		VE LO	1526 2006 2006 1526 1	O
		E, RELATI	000044 1 0000151 1 0000274 2 0000375 5 0000132 C	1NE SIMEG (A,B,C,N) T DOUBLE PRECISION(A,ON A(6,6), B(6), C(6) ATION TO BE SOLVED MY ATION TO BE SOLVED MY TUNE WORKS WHEN A IS TINE WORKS WHEN A IS THIN WHEN
CK NAME		CK, TYPE,	0001 0001 0001 00001 10000 0	1011 DOUBLE PRE NSION A (6.6) BE FRETURE PRE THE DOUBLE PRE THE DOUBLE PRE THE DOUBLE PRE THE DOUBLE PRE SOUTINE WORKS WE COLLIEN MINDERONN 90 SD 90 COLLIEN MINDERONN 90 SD 90 COLLIEN MINDE COLLIEN
18100		(BLOC	ב סטוגט ט סטוגט ט	11 HE R NOLT HE
ENCES		F Z	1 1 1 2 2 7 2 7 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
REFERENCES	N 10 2 10 10 10 10 10 10 10 10 10 10 10 10 10	ASS I GNMENT	000043 000137 000340 000127 000125	
N 8	m . m .n	E	o=	
EXTE	0000	STOR	00000	00101 00104 00104 00107 00107 00113 00113 00113 001134 001144 001144

NO DIAGNOSTICS.

END OF COMPILATION:

				١	0003 D 000044 0000 D 000002 0000 D 000015 0004 D 000016 0004 D 000022 0000 D 000036	
					000147 50L 00 000052 CRAD 00 000006 1 00 000000 RC 00 0000030 RVR 00 000026 U 00	
0					00001 00004 0 000001 000001 00004 0 00003 0	SUBROUTINE BOUND (X,TF,DX,B,ERR) IMPLICIT DOUBLE PRECISION(A"H,O-Z) DIMENSION X(50), DX(50) DIMENSION X(50), DX(50) DIMENSION PRECISION(A"H,O-Z) DIMENSION PRECISION(3), V(3), V(4), V(4), V(4), V(4), V(5), V(5), V(6),
COMMON(2) 000000				NAME)	000113 1376 0 000050 ALT 0 000062 F 0 000000 R 0 000052 RH0 0 000013 SRAD	RE,U,ALB,CA,A AD,SCRAD,ROB,
BLANK				LOCATION,	00003	(X,TF,DX,B,ERR) RECISION(A=H,O=Z) DX(50) U(3), ALB(3), DB(3) RXV08(3) VE,PRES,VRM,DB,ETA,VR,PRES,VRM,DB,ETA,VR,VR,PRES,VRM,DB,ETA,VR,VR,PRES,VRM,DB,ETA,VR,VR,VR,VR,VR,VR,VR,VR,VR,VR,VR,VR,VR,
0ATA(0) 000035		NAME)		TYPE, RELATIVE	000072 1306 000054 ALFA 0 000052 ETA 0 000064 99 0 000024 RE 0 000012 SCRA 0 000002 VR	SUBROUTINE BOUND (X,TF,DX,B,ERR) IMPLICIT DOUBLE PRECISION(A=H,00= DIMENSION X(50), DX(50) DIMENSION VR(3), U(3), ALB(3), DIMENSION PRE(3), UYE(3), UY
(1) 0002131	1070 1054	S (BLOCK,		(BLOCK.	A 00003	SUBROUTINE BOUND IMPLICIT DOUBLE P DIMENSION X(50), DIMENSION ROF(3), DIMENSION ROF(3), DIMENSION ROF(3), COMMON / DIFES / R, ITA, BEDA, CLA, F, 69, COMMON / DIFES / R, ITA, BEDA, CLA, F, 69, COMMON / DIFES / R, ITA, BEDA, CLA, F, 69, COMMON / DIFES / R, ITA, BEDA, CLA, F, 69, COMMON / DIFES / R, ITA, BEDA, CLA, F, 69, COMMON / DIFES / R, ITA, BEDA, CLA, F, 69, COMMON / DIFES / R, ITA, BEDA, CA, CA, RCZ HARRYRACZ-I, RCZ HARRYR
E USED: CODE	DIFEG	AL REFERENCE	DSGRT Nerr3\$	E ASSIGNMENT	000047 1216 0 000034 ALB 0 000014 08 0 000010 PRES 0 000010 PRES 0 000014 PCB 0 000044 WKG	- 2 w 4 w 4 v 8 v 0 - 1 w 4 v 8 v 0 + 1 w 4 v 8 v 0 + 1 w 4 v 8 v 0 + 1 w 4 v 8 v 0 + 1 w 4 v 8 v 0 + 1 w 4 v 0 v 0 + 1 w 4 v 0 v 0 + 1 w 0 v 0 v 0 v 0 v 0 v 0 v 0 v 0 v 0 v 0
STORAGE	0000	EXTERNAL	9000	STORAGE	000000000000000000000000000000000000000	000100 000100 000100 000100 00011111111

	20 B(4) #B(4) +X(1) + (ROB(1) + SRAD #RVR(1) + CRAD)				*RXV08(1)	28.0	ERR#(8(1)*8(1)+8(2)*8(2)+8(3)*8(3)+8(4)*8(4)+8(5)*8(5))	0.50					NO DIAGNOSTICS.
DO 20 1#1,3	20 B(4) #B(4) +X(1) *	B(4)=B(4)/RC	8(5)=0.	00 30 1=1,3	30 8(5) #8(5) +X(1) +RXV08(1)	8(5)=8(5)/RC-SCRAD	ERR=(B(1)+B(1)+	IF (ERR) 40,50,50	40 ERRH-ERR	SO ERR=SORT(ERR)	RETURN	END	END OF COMPILATION: NO
21*	22*	23*	24*	25*	26*	27*	28*	29*	30*	31*	32*	33*	ENDOF
00127	00132	00134	00135	00136	00141	00143	00144	00145	00150	15100	00152	00153	

STORAGE	USEDI	CODE(1)	0005331	0ATA(0)		0002611 BL	BLANK COM	COMMON(2)	000000								
COMMON	BLOCKS:																
0003 0004 0005	DIFEQ ENDCON CONST	0000070 000054 000103															
EXTERNA	L REFEREN	NCES (B	LOCK.	NAME)													
0006 0007 0010	ATMOS DSGRT NERR3S																
STORAGE	ASSIGNM	ENT	BLOCK, TY	TYPE, REI	RELATIVE	E LOCATION	_	NAME)									
0001	000370	1101	1000	000111	_	366	1000	000460		000	000170	_	•	1000	0001	7	-
000	00000	20L	1000	000262	~	016	1000	000270	202	1000	000351	~	* (1000	0003	4 1	2
1000	000374	2406	0001	000401	~ ~	4 5 0	0001	000420	252G	0001	000422	N «		1000		000044	N «
	000034	o 1-0 1-0 1-0 1-0 1-0 1-0 1-0 1-0 1-0 1-0	0003			FA		_	< <	000			ñ	0000			₹.
	0000010	AREA	0005	000004			0000	000130	88	000	0 000012		BE CK2	0003	0000	0000056	<u>ت</u> ت
	0000134	8 F Z	2000			ΨD				0000			!	0000			Ü
	000146	C13	0000			<u>.</u>				0000				0000			Ü
	000014	e :	0000	000157		DPRES		000155	ORHO O	0000	0 000153	<u>د</u>	м C	5000		000022	u i
	000000	د ا د د	0000							0000		=	EATC	0000			_
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90100	* * r in	O O		8(3)	RXVOB	ROB(3), RXVOB(3), RV	7(3)	R(3)	· · · · · · · · · · · · · · · · · · ·			רי	a				

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7
               DIMENSION PBXAT(5,6), UXE(3), UYE(3)
COMMON /DIFEG/ R.VR,PRES,VRM,DB,ETA,RE,U,ALB,CA,ACH,WKG,ALT,RHO,AL
FA,BEDA,CLA,F,00,VS
COMMON /ENDCDN/ RC,AMC,CTHC,RCTHC,SRAD,SCRAD,ROB,RXVOB,RVR,UXE,UYE
                                                       COMMON /CONST/ GM.PHIL,AZ,RCONV,AREA,BE,OM,AA,FJ,FH,FD,RIBP,RMD,EX
1A,UD,UDD,ID,FS,PD,WKGD,HEATC,CK1,CK2,CK3,RCURV,AB,RLGD,1CNVG
                                                                                                                                                                                                                                                                                                                                                                                                              PBXAT(2,1)#(PBXAT(2,1)#2.*VRM2*DVS*PAXB(1)/VS)*C3
PBXAT(2,1+3)#2.*VR(1)*C3
                                                                                                                                                                                                                                                         CALL ATMOS (ALT.TEMP, PRES, RHO, VS, DVS, DRHO, DPRES)
RC2=RC+RC
AMC2=AMC+AMC
                                                                                                                                                                                                                                                                                                                                                                                                      PBXAT(2,1)#PBXAT(2,1)+2. *VR(J)*PVXB(J,1)
                                                                                               A=(AB(1)+X(1)+AB(2)*X(2)+AB(3)+X(3))+RI
                                                                                                                                                                                                                                                                                                                                                                                                                                              PBXAT(4,1)=(ROB(1)=SRAD-RVR(1)+CRAD)/RC
                                                                                                                                                                                                                                                                                                                                                                                                                                       PBXAT(3,1+3)#C4+(X(1)+C1+X(1+3)/V2)
                                                                                                                                                                                                                                                                                                                  V2=X(4)+X(4)+X(5)+X(5)+X(6)+X(6)
                                                                                                                                                                                                                                                                                                                                                        C1=X(1)*X(4)+X(2)*X(5)+X(3)*X(6)
C3=1./(VS*VS*AMC2)
                                                                                                                                                                                                     PAXB(1)=(R1=C13)=X(1)+C12*AB(1)
PVXB(1,2)=(OM+AB(3)
         DIMENSION PVXB(3,3), PAXB(3)
                                                                                                                                                                                                                                                                                                                                                                                         PBXAT(1,1)=2.+X(1)/RC2
                                                                                                                                                                                                                                                                                                                                                                                                                                 PBXAT(3,1)=X(1+3)+C4
DIMENSION PBUAT(5,7)
                                                                                                                                                                                                                             PVXB(2,3)=0M+AB(1)
PVXB(2,1)==PVXB(1,2)
                                                                                                                                                                                                                                            PVXB(3,1) #*PVXB(1,3)
                                                                                                                                                                                                                                                    PVXB(3,2)=-PVXB(2,3)
                                                                                                                                                                                                                    PVXB(1,3)=-0M+AB(2)
                                                                                                                                                               RE=AA+BE/SQRT(C6)
                                                                                                                                                                       C12=RE+A+C5/C6+R1
                                                                                                                                       F (C6) 10,20,20
                                                                                                                                                                                                                                                                                                                           IF (V2) 50,60,60
                                                                                                                                                                                                                                                                                                                                                  VI=1./SGRT(V2)
                                                                                                                                                                                                                                                                                                           PBXAT(1,J)=0.
                                                                                                                                                                             C13*C[2*A*RI
                                                                                                                                                                                      DO 30 1#1,3
PVX8(1,1)#0.
                                                                                                                                                                                                                                                                                  VRM2=VRM+VRM
                                                                                                                       CS#AA*AA-BE2
                                                                                                                              C6#BE2+C5+E2
                                                                                                                                                                                                                                                                                                                                                                                                 50 70 J#1,3
                                                                                                                                                                                                                                                                                            DO 40 Imi,5
                                                                                                                                                                                                                                                                                                    00 40 Jais6
                                                                                                                                                                                                                                                                                                                                                                                  DO 80 1#1,3
                                                                                                                                                                                                                                                                                                                                                                          C4=1./RC+VI
                                                                                                        BE2-8E+8E
                                                                                                                                                      CONTINUE
                                                                                         BB * A A * R 1
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                                                                                 RI#1./R
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                                                  1,CRAD
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BU PBXAT(5,1)=-RXVDB(1)/RC THIS PART IS USED ONLY FOR THE CONVERGED CASE PRINT OUT		90	PBUAT(1,1) in 0		100	GO TO 140	110 CONTINUE	DO 120 1m1,5	PBUAT(1,7)=0.		120 PBUAT(1,7)=PBUAT(1,7)+PBXAT(1,J)+DX(J)		00 130 Ja1,6	POLAT (1°C) #0	DQ 130 K=1.6			140 RETURN	END	
90	ı														_					
62*	7 9	• 5 9	•99	67.	*89	*69	10*	71.	72*	73*	74*	75*	16*	77*	78*	19*	8 0	*18	82*	
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BE CH17 CH17 CH17 CH10 CH17 CH17 CH17 CH18 CH18 CH18 CH18 CH18 CH18 CH18 CH18	. 17365993+11 . 64850344+11 . 16830305+11 . 25436544+07 . 52893657019+07 . 36989493+07	-,25436544+07 -,52887019+07 -,36989493+07 -,29566947+05 -,13349536+06 -,20986251+05	0-01 84 #	100000000+01	47564427+02 15599601+04 .15345900+04 .31799275+04 .28076839+03	.11628687+06 25680687+03 .13210424+08 .46568884+08 .14981474+08
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.49343836744+06 .16234500072=02 .47881444528+00 .0000000000000000000000000000000000	.98342724+07 46151582+08 .13933855+08 18552648+04 46208261+04 88027928+04	18552648+04 46208261+04 28122149+04 26679047+02 -10854584+03 21191355+02	-,92836582746+OU .10191698013+O1	.100000000+03	42918537+02 14256861+04 .14553857+04 .28006736+04	•10512553+06 •12385795+03 •12301070+08 •42061574+08 •13210424+08
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RHO = .60945999612-01 OM = .72921150604-64 F = .00000000000000000000000000000000000	.13692268+08 40279997+08 .83156542+07 14075018+04 39367513+04 21151182+04	-,14075018+04 -,39367513+04 -,21151182+04 -,2417891+02 -,18172865+02	81 = .21798652271-03 85 =4740806391U-01	•64000000+07 AK = •100	40325544+00 13835402+02 .12765253+02 .23689026+02	.91639606+03 67053699+00 .1051253+06 .36541649+06

		.18084757+03	.18000000+03	.35765747+02	•36000000+02
	ERS	ITERATION PARAMETERS			
.95934308-04	27104676+03	78598056+03	20212599+03	.22777431-01	17422791+01
		CHECK			
46830849+03	26142098-02	.27553783-04	-+64402471-03	14792876+01	.40884972+00
		ANSWER			
+95934308-04	-,27104676+03	-,78598056+03	20212599+03	.22777431-01	17422791+01
		RIGHT HAND SIDE			
•34066726-05	10+60005586.	.12340734+02	.36330542+01	10944760-05	.33673040-01

TRIAL NUMBER 2

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BE FD OMZ CHIZ UDDZ HTC CCELY HTC CCELY HTC CCELY HTC CNC BE	.17669323+11 66368177+11 .17274407+11 24944428+07 54419514+07 33127823+07	24944428+0754419514+0738127823+0733875908+0513436969+0622553772+06	84 = 00000000000000000000000000000000000	+0348010799+02 +0416041626+04 +04 -15189638+04 +05 -32526422+04 +03 -29560428+03 EQUATION MATRIX	.12100805+06 11027835+04 .13710481+08 .48440491+08
AE = .63781660000139-05 CMY = .87791612754+00 CMIP= .22801704669+03 PANG= .1036670591+03 U0Y = .37533991285+00 U0DY= .27553783201-06 EXA = .600000000000 CK3 = .5000000000000 DHTI= .60441483102-02 LONG= .13882490366+03	PXF/PUD MATRIX -73446418+10 -18660900+11 -30682794+10 -51540632+06 -15005869+07 -98084243+09 -38165332+09	DPXF/PUD MATRIX51540632+0615005869+0798084243+0611427889+0553054345+0453054331+05 80UNDARY CONDITIONS	B3 =62637508931-01 DESIRED VALUES .60000000+021	- 40 4 4 P	.38132669+06 29041708+04 .43774193+08 .15254367+09 .48440491+08
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O F O C C C C C C C C C C C C C C C C C	.38943146+08 .14603915+09 .38151877+08 .52337965+04 -14659737+05 -84121101+04 .28453258+07		82 m ERR m DOUDOO+D1	.33210501-02 .11563472+00 .92286848-01 -19890311+00	-,72973621+01 .25482425+00 -,62714148+03 -,29041708+04
RHO = .60037444046=01 OM = .72921150604=04 F = .0000000000 1SP = .400000000000 PRES= .94030150436+07 PRES= .36832361630+04 MACH= .36832361630+04 CCD = .17507191005=01 CK1 = .0000000000	. 13939542+08 . 41209776+08 . 85426812+07 . 13534443+04 . 40720322+04 . 21805343+04	-,13534443+04 -,40720922+04 -,21805343+04 -,27487910+02 -,96244388+02 -,19552160+02	B1 = .24695075417-03 B5 =4677975558-01 .64000000+07 .20	41119337+00 14457181+02 .24214451+02 82657845+00	.95731129+03 .72973621+01 .10947435+06 .38132669+06 .12100805+06

.34640114-05		•10341988=D3		-+44642429+03		.10341988-03		
39087579+01		-27383222+03		17834832-02		27383222+03	ERS	
.12617794+02	RIGHT HAND SIDE	79051408+03	ANSHER	~.29268690-03	CHECK	79051408+03	ITERATION PARAMETERS	.18408598+03
+36973342+01		20357807+03		32362240-04		20357807+03		.18084758+03
23874504-03		.34678743-01		14130187+01		.34678743-01		,34965221+02
.34630874-01		-,17322119+01		,34929550+00		17322119+01		. 5765747+02

.39860319000415 .286080000000000000000000000000000000000	000000000 000000000 000000000 00000000		7EFS TAKEN • 39860319000+15 • 28608000000+02 • 90000000000+02 • 7440781379+05 • • 62145743229+00 • • 47797983136+06 • • 47348621796+06
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• 79182741874+04 • 12244760000+07 • 58346132000+09 • 17679955706+01 • 17140022624+04 • 26227239752+02 • 3729667500000 • 3781660000+07 • 5750000139-05 • 5750000139-05 • 5750000139-05 • 5750000139-05 • 5750000139-05 • 5750000139-06 • 5750000139-06 • 5750000139-06 • 5750000139-06 • 57500000000000000000000000000000000000			*52657613591+03 GM = .3948179072690+07 PH1 = .2823094342271+03 AZ = .9015850313214+01 AZ = .9716908374250+00 UZ =7631625889314+06 LFZ = .44710469918129+07 ETA = .54
2 0 0 2 0 0 2 0 0 2 0 0 2 0 0 2 0 0 0 0	PXF/PUO MATRIX - 000000000 - 000000000000000000000000	**************************************	V V V V V V V V V V V V V V V V V V V
• 65000732772+07 • 62981421000+07 • 17667557000+04 • 9118277523+01 • 949783056909+04 • 91182775233+01 • 57776010730+02 • 15414244730+02 • 15414244730+02 • 15414244730+02 • 154144528+00 • 16234500072-02 • 143853650623+00 • 16234500000000 • 88986254448-12 • 57776010798+00 • 77347366038-05 • 55000000000000 • 55000000000000 • 560000000000000	000000000 000000000 000000000 00000000	.00000000 .00000000 .90000000 .1155425-03 .23143636-04	.64020328194+07 .3039914465+03 .23356698047+01 .30361889046602 .64062806983+00 .48591352368+06 .19601021167+06
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. 000000000000000000000000000000000000	000000000 • 000000000 • 0000000000 • 000000	• • • • • •	.18225400562+04 -36665593875+07 .33879782708+03 .44399773215+00 .13280731000+06 .18184310569+03 .88050985834+02 .54982535361+00
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BE FD OMZ OMZ CHIY # # # UDZ FL # # # HTC CELE # # TC CELE # B # TC CELE	.17571968+11 -70056702+11 .17545814+11 -1737466+07 -64474798+07 -39508797+07	-,17367466+07 -,64474798+07 -,39506797+07 -,72746940+05 -,53827211+05 -,48903817+06	84 = 000000000000000000000000000000000000		-,47600462+02 -,19293414+04 ,16957337+04 ,33828159+04	*13064994+0645719106+0445719105+0415002515+0816489603+08
AE = .6378166000+07 FH =57500000139-05 OMY =87791612754+00 CHIP= .22412976812+03 PANG= .10402677658+03 UOY = .37596755030+00 UDDY= .11431938207-04 EXA = .00000000000 CK3 = .5000000000000 OHTI= .81326617914-02 LONG= .13879811464+03	PXF/PUD MATRIX • 19611029+11 • 29941704+10 • 279941704+06 • 17000802+07 • 10335427+07	DFXF/PUG MATRIX27894944+0617008802+0710335427+072227359+0537200305+0512980879+05130158899+06	83 =68804062680-01 DESIRED VALUES .60000000+021	PBWU MATRIX	-,15536746+03 -,64689004+04 -,36350362+04 -,10534924+05 -,30556531+03	SIMULTANEOUS EQUATION MATRIX .41859134+06 .1306499 13988565+054571910 .47069636+08 .1451192 .16616229+09 .5200251 .52002515+08 .1648960
.53444503413+06 .16234500072-02 .47881444528+00 .0000000000000000000000000000000000	.9769863+07 -49560568+08 -14503513+08 -11257959+04 -56990824+04 -28896136+04	11257959+04 56990824+04 528896136+04 62552222+02 -10950605+03	-,90435060373+00 -,10034019144+01	.4999999814-01	43251651+02 18010441+04 .10858093+04 .29699531+04	•11852325+06 •37323859+04 •13580602+08 •47069636+08
49109960147=01 q = = 72921150604=04 FJ = = 00000000000000000000000000000000	.38834145+08 .15385712+09 .38572722+08 -30210995+04 .17752561+05 .8463933+04 .26778358+07	30210995+0417752561+0584639373+0419981157+0334359340+0315693634+03	.63535696360-03 B2 # .42891373138-01 ERR # 00000407 .20000000+01	10F =	*14494849-01 *63173888+00 -28474173+00 -85405717+00 -43465976+00	-,35485432+02 -,13987247+01 -,37323859+04 -,13988565+05
RHO = .49109960147 OM = .72921150604 F = .00000000000 ISP = .40000000000 DRNG= .94981208952 PRES= .30317452425 MACH= .61854473166 CO = .17639245764 CKI = .000000000 J = .73435100618 D2 = .63165369020	.14039499+08 -,43442009+08 .85494708+07 -,73017974+03 -,48904411+04 -,22022003+04	-,73017974+03 -,48904411+04 -,22022003+04 -,56584765+02 -,43203972+02 -,43203972+02	B1 = .4289137 B5 =4289137	AK * .400	-,42713388+00 -,18704446+02 -,89130836+01 -,25143339+02	.10623135+04 35485432+02 .11852325+06 .41859134+06

		.19686521+03	.18408598+03	,33596029+02	.34965221+02
	ERS	ITERATION PARAMETERS			
•17935044-03	-,23569480+03	64370019+03	16678768+03	.60475579-01	12229921+01
		CHECK			
35204379+03	-,17115697-02	.10707028-03	13304343-03	13939971+01	.14935571+00
		ANSWER			
•17935044-03	-,23569480+03	64370019+03	16678768+03	,60475579-01	12229921+01
		RIGHT HAND SIDE			
•44716270*05	43630738+01	.14729802+02	.41660542+01	13813399-02	+41999441-01

TRIAL NUMBER 4

.2860819000+15 .28608000000+02 .90000000000+02 .14030918564+06 8613936515+04 91811994171+01 1520103196+02 .1799863636+01 .8557840000+07 .77140676824+08 .19361199573+02 .25790657133+03 .25790657133+03 .25790657133+03 .257906000000000000 .000000000000000	000000000000000000000000000000000000000	.00000000 .00000000 .00000000 .00000000 .00000000	.39860319000+15 .28608000000+02 .90000000000+02 .37479460788+05 .3521155838+05 .3521155838+05 .35795251156+06
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- 12244760000 - 122447600000 - 17680305521 - 17140022624 - 33152231170 249235619844 - 35932880757 - 67500000139 - 67500000139 - 6750000139 - 6750000139 - 6750000139 - 6750000139 - 6750000139 - 6750000139 - 6750000139 - 675000000000000000000000000000000000000	PXF/PUG MATKIX	0PXF/PUD MATRIX	- 115013 - 495047 - 780870 - 9701969 - 581324 - 113866 - 484242
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AE = .63781660000+07 FH =57500000139-05 OMY =87791612754+00 CHIP= .1939636870+03 PANG= .93543531565+02 UUV = .33152231170+00 UUDY= .56993162631-05 EXA = .000000000000 CX3 = .5000000000000 CX3 = .500000000000000000000000000000000000	PXF/PUD MATRIX •28674307+10 •14215110+11 •11446476+10 •25950661+05 •1408273+07 •21327929+09	DPXF/PUD MATRIX25950661+0514088273+0735215524+0711855435+04 .28558074+05 .10015135+05 .46507945+05	83 = 0 0 E S I R E D 0 0 6 0 0 0 1 T E R A T I 0 0 1 8 7 2 2
.23354509330+07 .16234500072-02 .47881444528+00 .0000000000000000000000000000000000	40852214+07 38799701+08 .67571009+07 .13732333+04 1854479+05 8904963+04	.13732333+04 18264479+05 89049634+04 .40462553+02 .91917897+02 .17039311+01	.21254166956+01 .22263183955+01 .10000000+03 .4999999814-01
57338248897-02 q = 7 72921150604-04 FJ = 000000000000	.24492481+06 -12673737+09 .10938126+08 .88623785+04 6153195+05	.88623785404 61531650+05 32742195+05 .13095944+03 .284533844+02	10516-02 ERR = 10516-02 ERR = 10516-02 ERR = 10516-030 = 10516-03 = 10516-03 = 10516-03 = 10516-03 = 10516-03 = 10516-03 = 10516-030
RHO # .57338248897. OM .72921150489. F00000000000000000000000000000000	.40911574+07 35608696+08 23989252+06 .18642205+04 15392506+05	.18642205+04 15392506+05 90421476+04 .31608194+02 .80734030+02 .10922502+02	* 44438732216-02 * -,95812900516-02 * 640000000+07 * .200 * .200

TRIAL NUMBER 5

	.2860800000+15 .28608000000+02 .14030918566+06 56813936515+04 74612880398+00 67086116528+01 17269257234+02 .17269257234+02 .17369257234+02 .17369257234+02 .1740676824-08 .21547444532+02 .2154744532+02 .2154744532+02 .2154744532+02 .21547441111-03 .21547441111-03 .215200000000	000000000000000000000000000000000000000	00000000.	**************************************
	Р Н 1			
	• 12244760000+07 • 12244760000+07 • 12244760000+07 • 17680047873+01 • 17140022624+04 • 25853498499+02 • 36727154758+00 • 38022686099+00 • 38022686099+00 • 5709090139-05 • 5700000139-05 • 57500000139-05 • 575000001407 • 57500000000000000000000000000000000000			
INITIAL VALUES		.0000000000000000000000000000000000000		.53073 48288 22414 22414 18690 48239 26506 10120
AITINI	2 Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	PX Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	00. 00. 00. 00. 00.	FINAL VALUES V =530 V =530 DZ =224 DDZ =224 DVY =186 UY =265 LFY =265 CD =177
	-62981421000+07 -17567557000+04 -9182739768+01 -94783081626909+04 -94783081626909+04 -12451407462+01 -12451407462+01 -12451407462+01 -12451407462+01 -12451407462+01 -12451407462+01 -13624500072-02 -47881444528+00 -1362450007000000000000000000000000000000000	000000000000000000000000000000000000000	.00000000 .00000000 .00000000 99595625-04 .11336659-03 .21098649-03	.64U31746432407 -19906180161403 -35551029281403 -2597475166401 -14982769578402 -67382911546400 -67482577506406 -91126965050406
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	000000000000000000000000000000000000	00000000	.00000000 .00000000 .00000000 .3184887-03 .97552027-04 63041496-04	. 183662 . 370414 . 371416 . 87116 . 132807 . 204850 . 804745
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.63567840000+07 .78750000512-05 .77140676824-08 .28841928987+02 .10248513945+0274612880398+00 .16594421411-03 .5135200000000000000000000000000000000000	.29367928+10 23355207+11 .75647530+10 60835513+06 13101743+07	60835513+06 20206112+07 13101743+07 28453875+05 -37574666+05 26117855+05	-•44074550527+00	40326543-04 2542944-02 25074085-03 35180095-04	•55210610-01 •32408942-02 •48580418401 •18192085+02
5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	.16935250+11 .72442459+11 .17515239+11 .461974637+06 .69478569+07 .39131413+07	-,61974637+u6 -,69478569+u7 -,39131413+u7 -,11214909+u6 -,12302523+u6 -,85657672+u5 -,747u5514+u6	84 = noncoco	44715052+02 20950268+04 .50997462+03 .34457526+04 .41865498+03	.13638U85+U6 8248U417+J4 .14635751+08 .53524226+U8
AE = .63781060000139-05 OMY = .67751012754+00 CHIP= .21971325509+03 PANG= .104064991,16+03 UODY = .34727154758+00 CK3 = .500000000000 CK3 = .5000000000000 CK3 = .50000000000000 UMTI = .10591852449-01 LONG = .13872379484+03	+ 73923163+10 - 20179283+11 - 28213662+10 - 33690978+05 - 17278579+07 - 10527991+07	DPXF/PUD MATRIX33490978+U517278579+U710527991+U73240U347+U53637811+U519979238+U5 .20255942+U6	03 =69494654863-01 0ESIRED VALUES .60000000+021	15151807+034471505 75055644+042095026 .16402834+045099746 .10753727+05 .3445752 23430606+03 .4186549 SIMULTANEOUS EQUATION MATRIX	.4486U559+U6 26346136+U5 .48556U26+U8 .17474453+U9
.\$6288108140+06 .16234560072-02 .47881444528+00 .60000000000000 -36349549825+06 -3634981266+00 .13056473939-04 .14209474936-01 .500000000000000 .43593837496+05	.91624136+0751112566+08 .14569193+0812767179+03527292706+04	-12767179+03 -62940763+04 -27292706+04 -96262025+02 -99654664+02 -79796713+02 -58925099+03	87951640196+00 -,98701532788+00 -,10000000+03	40858953+02 20058701+04 .56259708+03 .30159956+04	• 12425578+06 • 70373194+04 • 13789020+08 • 46556026+08 • 14635751+08
2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.37685578+08 .38380491+08 .31366111+03 .178992466-04	*31366111+03 -*19859392+05 -*79992466+04 -*31144850+03 *31469033+03 -*25153784+03	62 = EKR = DOUUDUU+D1	.25243130-01 .13282630401 -144089680400 -15107579401	66580395+02 -42658523+01 70373194+04 26346136+05 82480417+04
HO #	.13882347+08 -444980321+08 .83605424+07 .1899976+03 -54113396+04	.18999976+U3 54113396+O4 20899697+U4 87349717+02 .878U6529+02 68519023+D2 52109124+O3	1 = .99232206338=03 5 =39535604200=01 .64000000+07 .20 K = .400	-,42547815+00 -,22468714+02 -,28434687+01 -,25578945+02 -,71550905+00	.11679039+04 68580395+02 .12425578+06 .44860557+06

195+ull •64516298+05		20+03 •27594774-03		26-0229852421+03		120+03 •27594774-03		
.5U197895+U1		16710920+03		10628926-02		18710920+03	TEKS	
.18192085+02	RIGHT HAND SIDE	-,42969413+03	ANSWER	11273035-03	CHECK	42969413+03	ITERATION PARAMETERS	.20040725+03
.48560418+D1		11675796+03		.40348805-03		11675796+03		.18728080+03
-,32408942-02		.45689019-01		14318742+01		10-61068956.		*34126871+02
.55216610-01		-+48076311+00		.54110942-01		-,48076311+00		,34622923+02

.3986u319uu0+15 .2860eu0uu0u0+02 .90eu0u0u0u00+02 .14030918566+06 56813936515+04 82473153945+00 102389965/0+02 16807622399+02 .1799863334+01	77140676824-08 19202869820+02 26.323828562-03 62473153945+00 33600702445-03 61031971743-08 00000000000000	00000000000000000000000000000000000000	\$
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.79182741874+04 .12244760000+07 .58346132000+04 .317680348461+01 .32891394984+00 .24099259549+00 .24099259549+00 .370062789559549 .370062789559540	. 877916.12754+00 - 24084716449+03 - 91500009418+02 - 32891394984+00 - 25185983385-04 - 600000000000 - 15884027431+00 - 15884027431+00		ALUES 42 INTEGRATION 9144895U892+03 GM 50151931616+07 PH1 20481414922+02 AZ 95233975644+00 ALT 73879962280+03 VKZ 99485884007+00 UZ 99485884007+00 UZ 99485884007+00 UZ 99485884007+00 UZ 99485884007+00 UZ 99485884007+00 UZ
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7	CHIPPANGE #### UDDY ##### CEXA CK3	7 X Y Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q	FINAL V Z Z D D Z D D Z V K K Y K Y B H H H H H H H H C D D Z C D D Z C D D F Y C D F Y C D F Y C D F Y C D F Y C D F Y C D F X C D F
•65000/32772+07 •1756754000+07 •1756754000+04 •91182597192401 •9783056909+04 ••46003641316+00 •33878162102+01 •14727633283+02 •4537721324+02	.4781444528+00 .0000000000000000000000000000000000	.00000000 .00000000 .00000000 .00000000	44127852883+07 37110247858+06 91390860629+03 75211512206+01 29571571131403 79689517927+00 84016894110+06 40949533881+06
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• 63567840000407 • 78750000512-05 • 77140676824-08 • 32574290119+02 • 12193810843+02 • 182473153945+00 • 33600702405-03 • 61031971743-08 • 731520000000000 • 72139112630+05	35361948+10 16010144+11 -40656905+10 81767535406 47050874+07 19451700+07	81767535+06 47050874+07 19451700+07 19451700+07 4969958405 496963186+05	-•65680735780+00
6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	10857716+10 50808328+11 .48714737+10 35966928+07 165533708 10139592+08	.33966928+U7 16553370+U8 10139592+U8 .11124402+U5 .13484267+U5 .12484267+U5	- 10+000,000+01 - 1000,000,001
.63781660000+07 .57500000139-05 .87791612754+00 .19897654085+03 .95310255866+02 .32891394984+00 .25185983385-04 .25185983385-04 .31458089383+00	11 11	1 1	.80914546118-01 VALUES GUGGG+U21 N PARAMETERS 6241+03
.63781660000+0757500000139-0587791612754+00 .19897654085+03 .95310255866+02 .25185983385-04 .00000000000000000000000000000000000	PXF/PU0 MATRIX • 25534805+10 • 13463022+11 • 98410629+09 • 73226835+06 • 74508203+07 • 24508203+07 • 28195431+09	0PXF/PUD MATRIX	63 = .80914546118 0ESIRED VALUES .600000000000 ITERATION PARAMETERS .19056241+03
AE CHIPH H H H H L L L L L L L L L L L L L L L	PXF/PUC 255 134 735 245 245	0PXF/PU -733 -724 -724 -724 -724 -724 -724 -724 -724	833 = 0ESIREE 0 • 66 1 TEMAT 1 1 96
.17040187941+07 .16234500072-02 .47881444528+00 .00000000000 27372814251+06 46004171278+00 .86804171278+00 .5000000000000000 .38120602586+05	39966184+0734815360+0859644229+073090472+0415385718+0569201689+09	.30309472+04 15385718+05 69201689+04 -14294014+02 .105578011+03 -17352833+03	.83889913126+00 .10688140068+01 .10000000+63 .49999999814-01
TTOCCOX 30 TE TT	85343117+06 11564275+09 .99650972+07 12868061+05 5234771876+05	.12868061+05 52344729+05 24771876+05 .40012223+02 .33481497+03 .23379742+03	1-02 82 = 2-01 ERR = •20000000401 10L = 134498910+02
6117-02 0604-04 0000 0000+03 7818+08 0646+03 3406+01 3155-01 7608+05	8534 156 9965 5234 52477	1286 1.5234 1.52477 1.024701 3.3484 1.95337	3602-01 3602-01 • 200 • 3449
.72281466117-U2 .72921150604-U4 .U0000000000 .4600000000000+U3 .11241387818+U8 .50279200646+U3 .39176123155-U1 .39176123155-U1 .000000000000000 .55129857608+U5	.36266498+07 33234326+08 22152969+06 .3273460+04 13910766+05 69652952+04	.32733460+04 13910766+05 69652952+04 .10128778+02 .99954677+01	
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6M ALT W H H H ALT W H H H H H H H H H H H H H H H H H H	000000	S NO I	######################################
7		.00000000 .00000000 .00000000 .00000000	.5315663624+03 G48428319635+07 P21616910023+03 A40390508915+00 A .20755203467+03 V .50152264605+00 U .21021529831+06 L .95855573443+06 L
79182741874 1244760000 58346132000 17680126773 1714002624 5574626913 55749269613 55767379397 55760000139 55760000139 55760000139 55760000139 55760000139 557600000000000000000000000000000000000	PXF/PUG MATRIX	.00000000 .00000000 .00000000 .00000000	
V V V V V V V V V V V V V V V V V V V	PXF/P	FINAL COOL	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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######################################	000000000000000000000000000000000000000	00000000 00000000 27267718-03 37689776-03 67877153-03	2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
.0000000000000000000000000000000000000		• • • • •	.18485627762+04 .37385475411+07 .30655153419+03 .13694712828+01 .13280731000+06 .22595861587+03 .74122250844+02 .10837236683+01
1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		.00000000 .00000000 .00000000 .3537246-03 .95705448-04 .951893398-04	184 1373 136 136 136 136 136 136 136 136 136 13
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.63567840000+07 .78750000512-05 .30100788517+02 .99380307313+01 -7683116556+00 -20845991660-03 .61031971743-08 .7315200000000000 .10232198691+06	.23505826+10 23420542+11 .75108580+10 38017642+06 19546279+07 12522774+07	38017642+06 19546279+07 12522774+07 33275705+05 -34037072+05 -30188831+05	-•45527980991+00	39655168-04 29596055-02 10589769-02 38134479-04	.78118309-01 67013436-02 6117661+01 4578713+02 62579403+01
BE OMZ CH17 CH17 UGDZ H10 RCRV RCRV RCRV	.15620576+11 -72761614+11 .16981394+11 .62915994+06 -70418074+07		3=01 84 #	40459878+02 21450668+04 62107859+02 .34068234+04 .48236784+03	.14007194+06 12181370+05 .14363257+08 .53934918+08
AE63781660000+07 FH57500000139-05 OMY87791612754+00 CHIP21539420488+03 PANG 10380204179+03 UDY36025770161+00 UDY36025770164-04 EXA000000000000 CK35000000000000 CK3500000000000000 DHT1 13139211324-01 LONG +13857940348+03	PXF/PUD MATRIX • 70644546+10 • 20182775+11 • 25916648+10 • 33159147+06 • 16405776+07 • 10425844+07 • 40575846+07	0PXF/PUG MATRIX • 33159147+06 • 16405774-07 • 10425844+07 • 37962780+05 • 28436434405 • 22899869+05 • 2341624+06	BOUNDARY CONDITIONS B3 =65073722883-01 DESIRED VALUES .60000000+021	14185280+03404598782379889+04214506655742680+036210785 .10651571+05 .340682313371569+03 .4823678 SIMULTANEOUS EQUATION MATRIX	.47902850+06 -40790941+05 -49064708+08 .18166915+09 .53934918+08
• 58512405792+06 • 16234500072-02 • 47881444528+00 • 0000000000000000000000000000000000	.81588318+07 .51190163+08 .14207630+08 .9805564+03 .64963869+04 .24698750+04	.9805564+0364963869+0424698750+0411796373+0397030240+0297030240+02	**85448658741+00 *97109360886+00 *1000000+03	21021927+04 21021927+04 24242566+02 29740264+04 57644925+03	•12833209+06 •10646903+05 •1369297+08 •49064708+08 •14363257+08
34821731231-01 Q	.35061470+08 .1599724+09 .37064341+08 .40425479+04 .207152404	.40425479+04 .020715240+05 .72237529+04 .28223753+03 .30849596+03 .30849596+03	.12906753354-02 82 = .36871513881-01 ERR = 00000+07 .20000000+01	*34619181=01 *21643132+01 *38017787+00 **21410366+01 **45531117+00	10993869+03 -96213311+01 10646903+05 40790941+05
RHO = .34821731231- OM = .72921150604- F = .00000000000000000000000000000000000	. 13224613+08 . 45282117+08 . 79319975+07 . 11887924+04 - 558828969+04 - 19012667+04	.11887924+04 .558289494 .10734476+04 .10734476+03 .83131054+02 .63034796+03	B1 = .12906753354-02 B5, =36B71513881-01 .64000000+07 .20	40351195+00 25274515+02 39925133+01 .25203702+02	.12904497+04 10993869+03 .12833209+06 .47902850+06

		.20344942+03	.19056241+03	.34658723+02	,34498910+02
	ERS	ITERATION PARAMETERS			
*37077993-03	-,13997192+03	20033715+03	-,67554114+02	-,10234551-01	.28719314+00
		CHECK			
26285163+03	90716546-03	95805157-04	.48103374-03	14057539+01	17432891-01
		ANSWER			
.37077993-03	-,13997192+03	20033715+03	67554114+02	10234551-01	.28719314+00
		RIGHT HAND SIDE			
+98871093-05	.62579403+01	.24578713+02	•61175861+01	6/013436-02	10-10-01197.

TRIAL NUMBER 8

.39860319000+15 .2860800000000+02 .100000000000+02 .1115702127+04 .1115702127+02 .1730279540+02 .1730279540+02 .1730279540+02 .1730279540+02 .1730279540+02 .1730279540+02 .1730279540+02 .1730279540+02 .1730279540-03 .353606824-08 .353606824-08 .3536068281239-03 .353606882906-03 .00000000000000000	000000000000000000000000000000000000000	**OOOOOOOOO INTEGRATION STEPS TAKEN 911+03 GM ** *39860319000+15 609+07 PH I ** *28608000000+02 185+02 AZ ** *90000000000000 170+03 ALT ** *35131827646+05 170+03 VRZ ** *29809919288+03 318+00 UZ ** *-23992112143+00 176+05 LFZ ** *-73743575718+06 825+06 DFZ ** *42938796788+06 919+00 ETA ** *11881097911*01
		.000000000 FEGRATION S +03 GM # +07 PH1 # +02 AZ # +01 AKZ # +01 UZ # +06 UZ # +06 OFZ #
. 79182741874+04 . 12244760000+07 - 58346132000+04 - 17680380302401 - 17140022624+01 . 32597155814+00 - 52300486384402 - 52300286388401 - 538068969402 - 5250028638801 - 53701612754+00 - 5750000139-05 - 67791612754+00 - 67791612754+00 - 67791612754+00 - 67791612754+00 - 67791612754+00 - 677916123-04 - 677916123-04 - 677916123-04		ALUES 43 INTEGR. • 8424998911+03 • 50351794609+07 • 11639475047+01 • 64586278170+03 • 52629806318+00 • 52629806318+00 • 52629806318+00 • 52629806318+00 • 68029085919+00
7 7 7 7 8 1 8 2 8 1 8 7 8 1 8 7 8 1 8 7 8 1 8 1 8 1 8 1	PXF/PUD MATRIX -00000000 -000000000 -000000000 -000000	**************************************
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.104164160000 .50566950000000 .15169271601+01 .13280731000+04 .77459386217+04 .20344942194+03 .20344942194+03 .2034496217+04 .2034496217+04 .2034496219+03 .2034496219+03 .2034496219+03 .2034496219+03 .2034496219+03 .2034496219+03 .20346900000000000000000000000000000000000	w 4. 4	190373 756800 436495 554814 731000 818570 9119893
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*63567840000+07 *78750000512-05 *3175566923+02 *12021576552+02 *84039352697+00 *35360538906-03 *61031971743-08 *731520000000000	15239639+11 15239639+11 15239739410 72347394406 37679784+07 183199784+07	72347394+06 37679764+07 18319978+07 -59271513+04 -43382973+05 63427274+04	-,65599794908+00		27053553-04 27265451-01 1292655-02 90065015-04	.57506875+01 10920827+01 .28129746+03 .17238983+04
PF FD CHIV CHIV CHODZ FL HHTC PCC CCLI	18245336+10 48282245+11 52584137+10 35236814407 13241295+08 96153688+07	.35236814+07 13241295+08 96153688+07 .23720839+04 .10889915+06	1=01 B4 x	100000000+01	-,16287811+02 -,12149260+05 -,33364355+03 ,17793472+04 ,86277011+03	**************************************
AE63781660000+07 FH57500000139-05 OMY87791612754+00 CHIP196.38919685+03 PANG*95886763349+02 UUT *26887166123-04 EXA *00000000000 CK3 *500000000000 CK3 *5000000000000 DHT1:27149853883+00	PXF/PUD MATRIX	0PXF/PUD MATRIX •62670570+06 •17339391+07 •25911065+07 -31475119+04 •23755816+05 •70950954+04	BOUNDARY CONDITIONS B3 = .70892852161=01	DESIRED VALUES . LOUGOOOD+02	54519277+02 58841326+05 18405956+04 .57023554+04	\$IMULTANEOUS EQUATION MATRIX 11636794+08
.16725824793+07 .16234500072-02 .47881444528+00 .000000000000 -30712723096+06 -4329916585+00 -89755427797+00 .50000000000000000000000000000000000	44018923+07 32921370+08 -61117606+07 -32443788+04 12928482+05 66408845+04	•32443788+04 •12928482+05 •66408845+04 •66966842+01 •86750515+02 •86750515+02 •86750510401	•61579205150+00 •90306180652+00	.10000000+03	94805270+01 96097867+04 15541220+03 15434023+04	•19071889+07 ••36179441+06 •94884627+08 •57427432+09
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RHO = .81444458945-02 OM = .72921150604-04 F = .00000000000 ISP = .4000000000000 DRNG= .11236587264+08 PRES= .56166061025+03 MACH= .25422761860+01 CCO = .40766139973-01 CK1 = .56117755345+05 02 = .93909059620+02	.32317709+07 .32263554+08 .56307365+05 .3457236+05 .11902036+05 .44565221+06	.34572376+04 11902036+05 68067188+04 .3778650+01 .81705601+02 18902410+00	81 x .37605161625-02 85 x30781951544-01	.64000000+07 AK = .800	-,16965371+00 -,1962283+03 -,71921326+01 ,13464347+02	.38737498+05 73555764+04 .19071889+07 .11636794+08

		+23635068+03	+20344942+03	.49005538+02	.34658724+02
	គ ន	ITERATION PARAMETERS			
30097892-02	14431326+04	66077314+04	11152611+04	.40962834+01	-,21510852+02
		CHECK			
•10747320+03	-,13259974-02	.98544597-03	18533670-03	-,89724252+00	39124867+00
		ANSWER			
30097892-02	-,14431326+04	66077314+04	11152611+04	+40962834+01	-,21510852+02
		RIGHT HAND SIDE			
+85816363-03	.35582834+03	.17238783+04	•28129746+03	10720827+01	10+6/8006/4.

.39860319000415 .2860000000402 .9000000000402 .14030918566406 56813936515+04 5681401732+00 52791423398402 3303254664-02 .17999863636401 .179998636401 .179998636401 .179998636401 .179998636401 .17140676824-08 .1508694101732+00 .1508694101732+00 .150844690000000 .1502244690000000	000000000	000000000	TEPS TAKEN .39860319000+15 .28608000000+02 .90000000000+02 -7266872163+04 .78416441058+02 .82418724802+06 -47795448575+06 .23245444575+06
9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9			ATION S GM PHI # ALT # ALT # UZ # UZ # LFZ # ETA #
**19182741874404 **12244760000407 **58346132000+04 **17680071879+01 **1740022624+04 **1908957872420 **190895787240 **1908957814996+01 **72731157803+00 **57500000139-05 **57500000139-05 **57500000139-05 **5750000013418+02 **56048084878+00 **56048084878+00 **56048084878+00 **56048084878+00 **5604808000000000000000000000000000000000			ALUES 113 INTEGRATION STEPS *33299936288+D3 GM = *39 *34869944280+07 PH1 = *28 *22360810323+D3 A2 = *90 *25492698189-D1 PKI = *70 *35467889844+D2 VRZ = *78 *56477354501+D0 UZ = *82 *11202446525+D7 LFZ = *47 *11202446525+D7 LFZ = *47 *14757124954U-01 ETA = *53
• 79182741874 • 12244760000 • 58346132000 • 17680071879 • 1740022624 • 26048084878 • 19089579272 • 99657014996 • 72731157803 • 57800000139 • 57800000139 • 578000000000000000000000000000000000000	PXF/PUD MATRIX • 000000000 • 000000000 • 000000000 • 00000000	.UD MATR1	.33299 .33299 .34869 .22360 .25492 .36467 .11202 .11202 .11202
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. 65000732772407 . 17567557000+07 . 91182588562+01 . 49783056909+04 . 19437831481402 . 19437831481402 . 19437831481402 . 19437831481402 . 19437831481402 . 192272213+00 . 16234500072-02 . 47881444528+00 . 61922721324+02 . 16234500072-02 . 18585998302-02 . 8565998302-02 . 8565998302-02 . 8565998302-02 . 8665998302-02 . 8665998302-02 . 8665998302-02 . 8665998302-02 . 8665998302-02 . 8665998302-02 . 8665898302-02		.00000000 .00000000 .3664800-04 .10274509-03 .69256257-04	.63649668035+07 -949211157825+07 .85282963610+02 -940576738564-02 .83160286277+01 .41515283525-01 -39047801961+06 .24651690378+05
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• 6367840000+07 • 78750000512-05 • 77140676824-08 • 3438796268402 • 98283069135+01 • 96544101732+00 • 12022446900-02 • 12022446900-02 • 112160563879+06	- 30717132+09 - 11482516+10 - 179823573+05 - 12941943-06 - 12941943-06 - 12941943-06 - 12941943-06 - 179823573+05 - 179823573+05 - 179823573+05 - 179823573+05 - 179823573+05 - 17038323+01 - 17038323+01 - 17038323+01 - 17038323+01	•11685537155+00
7 8E 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	-10580041+10 -48221473+09 -35105750+05 -3475680+06 -47925755+08 -47925755+06 -35105750+06 -35105750+06 -97118174+01 -13863740+03 -13863740+03	+00 B+ M
AE 63781660000+07 FH 57500000139-05 OMY 68771612754+00 CHIP 887116381495+02 PANG 72998931571+02 UDY 26048084878+00 UDY 2600000000000 CK3 5000000000000 CK3 50000000000000 DH71 59086049447-02 LONG 14751760615+03	PK/PUD MATRIX .36081838+10 .29516003+10 .29516003+10 .295146473+05 .25699070+04 .25699070+08 .25699070+08 .25699070+08 .25699070+08 .25699070+08 .314473+05 .42008007+04 .23051047+05 .31570508+02 .17969762+01 .35670508+02 .17969762+01 .35670508+02 .17969762+01 .35670508+02 .17969762+01	B3 = .12161729752+00 DESIRED VALUES .60000000+0211 ITERATION PARAMETERS .21167474+03
• 54138711290+07 • 16234500072-02 • 47881444528+00 • 00000000000 • -75841127427+06 • 8565598302-02 • 38667041930-04 • 13670155365+01 • 5000000000000000000000000000000000000	* 54167745+06 * 12851397+07 * 15142825+07 * 10142589+03 * 324131165+05 * 32131165+05 * 32461123+02 * 97189711+01 * 7882936-02 * 77882936-02 * 77831415-01 * 78882936-02 * 77631415-01 * 11735043+00	**,98541031446+00 *10048512474+01 *100000000+03 *4999999814-01
101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-43239224+07 -182022359+07 -11821640+07 -28113260+02 -24153706+03 -77221498+02 -24153706+03 -24153706+03 -24153706+03 -31741222-03 -91820766-01 -12569087+01	6-01 B2 = 9+00 ERR = •20000000+01 TOL = 138245427+02
RHO		B5

*3986319000+15 *2860800000+02 *9000000000+02 *14030918566+06 **56813936515+04 **14257416137+02 **20814749272+02 **20814749272+02 **20814749272+02 **20814749272+02 **20814749272+02 **20814749272+02 **20814749272+02 **20814749272+02 **20814749272+02 **2081444000000000000000000000000000000000	00000000. 00000000. 00000000. 00000000	000000000	TEPS TAKEN *39860319000+15 *286080800000+02 *9808080808000000000000000000000000000
6M AZ VRZ VRZ VRZ OLFZ ONZ ONZ ONZ ONZ ONZ ONZ ONZ ON			INTEGRATION STEPS 177+03 GM 3 .39 172+07 PHI 8 .28 172+03 AZ 8 .90 203+01 ALT 8 .27 547+03 VRZ 8 .46 258+00 UZ38 006+06 LFZ 8 .91 043+06 DFZ 8 .37
• 79182741874+04 • 12244760000+07 • 12244760000+07 • 17680349311+01 • • 1749022624+04 • • 233882676375+00 • 62795380028+01 • 647953800139-05 • 637801612754+00 • 637801612754+00 • 5780000139-05 • 13068118842=03 • 13068118842=03 • 13068118842=03 • 1306810000000000000000000000000000000000			44 27985 27985 15629 79937 19057 19057 19057 30748
V C C C C C C C C C C C C C C C C C C C	**************************************		FINAL VALUES V V V V V V V V V V V V V V V V V V V
*65000732772+07 *1567557000+04 *91182690155+01 *14978305650016 *19562717768401 *182384979952400 *1923271774+00 *19234570072=02 *19234570072=02 *1923457000000000000000000000000000000000000	000000000 • 00000000 • 000000000 • 000000	**DDDDDDDDDDDDOODDO*******************	.64050807571+07 54253737370+06 .36100920422+03 15424729029+01 54178456404+03 54178456404+03 90354062584+00 43898093313+06 43898093313+06
HESSONE COLCECTOR SEES TO COLC	00000 00000 00000 0000	00000000 00000000 23296881-03 332943709-03 32543709-03	
.0000000000000000000000000000000000000	000000000 00 00 00 00 00 00 00 00 00 00	0000 0447	• 18734233256+04 • 38463119954+07 • 21575045739+03 • 13280731000+06 • 73604938558+03 • 17522649762+02 • 39852763927+01
- X O Z > 4 C C C C C C C C C C C C C C C C C C	000000000000000000000000000000000000000	.00000000 .00000000 .46438965=03 .9189865=04 .66594316=04	× 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

•63567840000407 •7875000512-05 •77140676824-08 •11394284404-02 •10425718058+02 •87899748755+00 •561031971743-08 •7315200000000 •99605516854+05	50820570+10 10988062+11 -50251053+10 31134358+07 -33683086+06 -17470161+07	- 31134358+07 • 33683086+06 • 17470161+07 - • • 46413409+04 • 95560364+04 • 84679865+04	-•63459025741+00		**18319701**04 **14520539**01 **68728934**03 **39347439**04	.48812725+00 12534273+00 21151231+03 35622094+03
PE FD CH17 CDCEC CODZ HTC CCCLI	63672131+10 24476945+11 .73030642*10 45881885+07 .56778051+07 .15701941+07	4581885+07 .50778051+07 .15701941+07 .61359803+04 24849145+05 .13859589+05	7-01 84 #		,40643414+01 -15718111+05 -10078289+04 -12817348+04 -1104534+04	51645286406 .13219838406 .23030180*09 .39104043*09
AE = .6378166000+07 FH = .575000139-05 OWY = .8779161275400 CHIP= .15717687497403 PANG= .97238239995+02 UOY = .33882676375+00 UOY = .13068418842-03 CK3 = .500000000000 CK3 = .500000000000000000000000000000000000	• 77056174+09 • 77056174+09 • 90024588+10 • 36751310+09 • 27206160+07 • 14212295+07 • 12286566+09	DPXF/PUD MATRIX 29206160+07 -14212295+07 20892449+04 23795574+04 -11975140+05	BOUNDARY CONDITIONS B3 = .47552869757-01 DESIRED VALUES	• • • • • • • • • • • • • • • • • • •	.28169482+02,4064341 .24401446+05 .1571811 .21243786+04 .1007828 .28864614+04 .110453 .14905611+04 .1110453	79586334+06 .20418317+06 .35903306+09 .61049779+09
.45418887288407 .16234500072-02 .47881444528+00 .0000000000000000000000000000000000	-63937184+07 -17851047+08 -67547594+07 -33090207463 -14580245+04	.84407188+03 33090207+03 14580245+04 52869583+01 .71640014+01 .31044719+01	•51775091288+00 •82186311960+00	.10000000+03	.23769197401 .14508458405 .91263008403 .10917047404	-,47947727+06 -,12348331+06 -,21252328+09 -,35903306+09 -,23030180+09
25473158449-01 q = = 72921150604-04 FJ = 900000000000000000000000000000000000	86988940+07 63079481+08 .13317071+08 .65399835+04 .86076032+03	.65399835+04 .86076032+03 87612847+04 10497266+02 84617237+00 .13069717+02	8198-02 B2 == 8821-01 ERR ==	.20000000+01 ToL =	16897517-03 -86126285+01 -33678836+00 16932413+01 12112276+01	30512176+03 •78624934+02 •12348331+06 •20418317+06
RHO	.176D5141+D724578995+D8 .13260268+D7 .13689899+04 .1128775+D3	.13689899+04 .11286775+03 .28958188+04 .66528684+01 .65274104+01	81 x .15883668198-02 85 x49238058821-01	•64000000+07 AK # •800		011936478+04 03051276+03 047947727+06 079586334+06 051645286+06

		.20215892+03	.21167474+03	.37012806+02	.38245428+02
	FRS	ITERATION PARAMETERS			
14918871-02	.14368798+04	+21791712+04	.13878622+04	.11062404+01	43028956+01
		CHECK			
+27883775+02	.15405960-04	.11290472-03	24809465-03	,25950372+00	,33614553-01
		ANSWER			
14918871-02	.14368798+0'	.21791712+04	.13878622+04	.11062404+01	-,43028956+01
		RIGHT HAND SIDE			
•21161094-03	-,22911399•03	35622094+03	21151231+03	-,12534273+00	.48812725+00

.39860319000415 .286080000000402 .1403018566406 -56813936515404 -82929393520400 -11464946514402 -1577433044602 -17799863636401 .277140676824-08 .21482320204402 -271406183034 .2148232020400 .2930615001-03 .55590615001-03 .61031971743-08 .73152000000000	00000000000000000000000000000000000000	.39860319000+15 .286080000000+02 .90000000000000000 .182548225005 .44030959848+03 .67473540504+00 -61448854301+06 .55348481089+06
63 7		ATION S GM AAZ BHI BH A VRZ BHI BH B UZ BETA BETA BETA
• 179182741874+64 • 12244760000+07 • • 58446132000+07 • • 17460222624+04 • • 17140022624+04 • 34621411167+00 • 25549560151+02 • 43097893381+00 • 43097893381+00 • 43097893381+00 • 43097893381+00 • 43097893381+00 • 43097893381+00 • 57500000139-05 • 4307811763+03 • 243021411167+00 • 243021411167+00 • 243021411167+00 • 260000000000000000 • 15884027431+00	* * * *	ALUES 59 INTEGRATION STEPS .24881858855+03 GM = .39 .16513664870+03 AZ = .90 .26490486340+01 ALT = .94 12399499952+02 VRZ = .44 .34574641077-01 UZ = .67 .21428191525+06 LFZ = .81 .15586612034+05 DFZ = .55
	**************************************	FINAL VALUES V = 2488 Z = 16515 DZ = 165100 VRY = 1239 VRY = 1245 LFY = 2142 CFY = 5224
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	X Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	FINAL 2 2 2 0 2 0 0 2 0 0 0 0 0 0 0 0 0 0 0 0
62981421000+07 1756755700+04 49783056909+04 420886085409+04 420886085409+04 420886085401 17151953315+02 45751127402+00 45751127402+00 45751127402+00 45781127402+00 422086608000000 422088608544+00 42208860860000000 108386000000000 1083860000000000000000000000000000000000	.00000000 .00000000 .00000000 .00000000	.6395625833+0772680086638+06 .16270456487+033925854832+0041143275307+0353724943362+0086519639500+065171855912+06
	00000000 00000000 00000000 00000000 0000	1
.0000000000000000000000000000000000000	•••••	.1855777100+04 39019278346+07 90375855348+02 3335586039+01 .13280731000+06 60274638151+03 -45464876380+01 -3438134471+01
1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	.00000000 .00000000 .00000000 .00000000	
	0000000 0004644	A A C & D D X + A A C & C D D X A A A A A A A A A A A A A A A A A

.63567840000407 .78750000512-05 .77140676824-08 .1073331178+02 .62789393520+00 .5520615001-03 .51031971743-08 .73152000000000000000000000000000000000000	49890456+10 15378263+11 -63135696+10 -195696+10 20176550+06 11140248-07	• 19569691+07 • • 20176550+06 • • 11140248+07 • 52897317+05 • 66650262+04 • • 64582041+05 • 49245647+06	61152563236+00	28993300-04 15111063-01 44474803-02 10974225-04	.26343631+00 .32447014-01 .10774251+03 55159155+03
8 E F D O M Z C H I I I I I I I I I I I I I I I I I I	65747659+10 31016818+11 .94588265+10 72528428+07 .34526849+07 .52978230+07	-,72528428+07 ,34526849+07 ,52978230+07 ,52409514+05 -,37449429+05 -,25173916+05 ,13503543+06	0+00 84 •	-,49758325+02 -,68634485+04 -,41989609+04 ,18856968+04	*IION MATRIX • 14528929+06 • 14322507+05 • 63492040+08 • - 26371147+09 • 69808735+08
AF = .63781660000+07 FH =5750000139-05 OMY = .87791612754+00 CHIP= .13753505395+03 PANG= .11190886902+03 UOVY = .36621411167+00 UOVY = .20294320973-03 EXA = .00000000000 CK3 = .5000000000000 DHTI= .46546310687+00 LONG= .13471231113+03	PXF/PUD MATRIX • 17137424+10 • 10445648+11 • 39582897+09 • 18023302+07 • 21628017+06 • 46869443+06 • 17390353+06	DPXF/PUU MATRIX • 1802302+07 • 1802302+07 • 1802302+07 • 46869443+06 • 59817006+05 • 39442112+04 • 59155501+05 • 48003835+06	83 =19922813270+00 DESIRED VALUES .6000000000001	PBWU MATRIX 37148574+02 33472344+05 1029665405 37810374+04	SIMULTANEOUS EQUATION MATRIX54164821+06 .146289281129435+05 .143225023648950+09 .634920426371147+09 .6980873
.14502973830+08 .16234500072-02 .47881444528+00 .00000000000 33349065501+06 42208860854+00 .1083860005-03 .1083860005-03 .294000000000000000000000000000000000000	62745318+07 25233603+08 .85893255+07 .22038094+04 54559710+02 24550798+04	.22038094+04 54559710+02 24550798+04 58948245+00 .12188320+01 15566779+02	.64703059877+00 .64703059877+00 .10000000+03	52739051+02 54759306+04 56240689+04 -13225988+04	.11698169+06 .17488699+05 .63395432+08 23648950+09
12129644019+00 Q = 1 .72921150604=04 FJ # # .000000000000000000000000000000000000	67960261+07 78968011+08 -16527597+08 -12911285+04 -22637642+04 -43663061+06	.12911285+04 .22637642+04 .646159460+04 .54636443+02 .27230301+02 .38985680+02	99630-02 B2 ** 50697-01 ERR ** .20000000+01	20321069-01 15820154+01 19237066+01 16591945+01	.1075366402 .10415859402 .17488699405 81129435405 .14325607405
KHO = .12129644019 OM = .72921150604 F = .0000000000 ISP = .4000000000 DRNG= .10884726086 PRES= .74132937334 MACH= .20605771000 CD = .453020000000 J = .68030834481 DZ = .11475975819	.34619250+07 26959995+08 .13329275+07 .33177332+04 .89945730+02 33161096+04	.33177332+04 .89945730+02 .33161096+04 .13583245+02 .17765065+01 .21769057+02	81 =13664599630-02 85 =34780850697-01 .64000000+07 .20	.26403645-01 16839178+02 20311512+01 .10362819+02	.39970178+03 .10753464-02 .11698169+06 -54164821+06

.24812602-03		48432280-03		.24087942+02		48432280-03		
.12240351+03		-,23344057+03		-,23842875-04		-,23344057+03	ERS	
55159155+03	RIGHT HAND SIDE	.59025967+03	ANSWER	.54837643-05	CHECK	.59025967+03	ITERATION PARAMETERS	,20330028+03
•10774251+03		•99238522+02		+38966403-04		+99238522+02		.20215893+03
,32447014-01		*30304555+00		19920304-01		.30304555+00		.37897984+02
.26343631+00		19435557+01		15449281-01		19435557+01		.37012806-02

	. 39860319000402 . 286080000000402 . 14030918566406 . 56813936515404 . 8339863066406 . 12010656746402 . 179986306402 . 1799986306402 . 1799986306402 . 1799986306402 . 1799986306402 . 1799986306402 . 1799986306402 . 1799986306402 . 17140676824-08 . 17140676824-08		000000000000000000000000000000000000000	**************************************
	64 4 A L 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
IES	. 79182741874+04 . 12244760000+07 . 58346132000+04 . 1740022624+04 . 3747027993+00 . 25851207215+02 . 4551465652+00 . 4551465652+00 . 4551465652+00 . 457500000139-05 . 57500000139-05 . 57500000139-05 . 57500000139-05 . 57500000139-05 . 57500000139-05 . 57500000139-05 . 57500000139-05 . 575000001000000000000000000000000000000			ALUES 48 INTEGRATION -20991752038+03 GM -47534981021+07 PHI -87776855872+02 AZ -102121197588+01 ALT -11246710158+02 VRZ -19558165775-01 UZ -37456997407+06 LFZ -11648163763+05 DFZ
INITIAL VALUES		PXF/PU0 MATRIX .000000000 .0000000000000000000000000	. OUDDDDDD . OUDDDDDD . OUDDDDDD . OUDDDDDD . OUDDDDDD . OUDDDDDD . OUDDDDDD	FINAL VALUES V = -209 Z = -475 DZ = -212 VRY = -195 LFY = 1-374 OFY = -175 CC = -374
INITI	V V V V V V V V V V V V V V V V V V V	7 X Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	7 X Y O	F I N A L L L L L L L L L L L L L L L L L L
	- 65000732772+07 - 62981421000+07 - 17567557000+07 - 91182812133+01 - 94783056909+04 - 9406533575179+01 - 9406533199+01 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 17929429376+02 - 179294297602-04 - 179294297502-04 - 179294297502-04 - 179294297502-04 - 179294297502-04 - 179294297502-04 - 179294297502-04 - 179294297502-04 - 179294297502-04 - 179294297502-04 - 179294297502-04		.00000000 .000000000 .00000000 .8990587-04 .12099343-03	.63987587438407 15584129631407 1721842740403 535704554340403 37469874318403 77319859776400 8786362898406 38807369095406
	HINNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN	200000	7 - 0 3 3 4 - 0 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	* * * * * * * * * *
	FIGOSSOS XXX XX		.00000000 .00000000 .00000000 .25815855-03 .37496945-03	C C C C C C C C C C C C C C C C C C C
	.104164160000000000000000000000000000000	••••	• • • • •	.18314897676404 .39899521665407 .70386193035402 .23873946405401 .13280731000406 .54646897962403 .77061345705401 .32824864451401
	0 1 3 1 1 1 1 2 2 3 3 3 3 3 3 3 3 3 3 3 3		.00000000 .00000000 .00000000 .42396018-03 .4775642-04 .26078376-04	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	X X X X X X X X X X X X X X X X X X X	2000000	000 000 000 000 000 000 000 000 000 00	A K K K K K K K K K K K K K K K K K K K
	TYDAY A HARMEN A KANA A			A RELEASES

• 6356784000407 • 78750000512-05 • 77140676824-08 • • 11206718023+01 • 10381050293+02 • 83399863066+00 • 57974902527-03 • 61031977743-08 • 73152000000000000000000000000000000000000	- 40434698+10 - 16940430+11 - 90439949+10 - 13569314+07 - 13497914+07 - 13497914+07	13569314+07 38896978+06 .13497914+07 .17768023+05 .75794004+03 18268257+05	5032030037+00		20145953-04 9890207-02 23804270-02 17569209-04	.2377612+00 42319290-01 60061113+02 24341445+03 66753718+02
8 E F D O M Z O M	37190983+10 37997087+11 .15462483+11 59937772+07 .29012383+07 .35242085+07 .43843933+09	59937722407 .29012383+07 .35242085+07 .19349301+05 29227790+05 67045737+04	# +9 00+0	-•10000000+01	-,22323037+02 ,69200398+04 -,71566513+03 ,23535047+04 ,13967282+04	13066811+06 .23822446+05 .50058952+08 .16917545+09
AE	PXF/PUD MATRIX -21720861+10 -11587239+11 -20870639+10 -11854584+07 -2782404+06 -14962772+07	DPXF/PUD MATRIX11854584+0729782404+06 .14967772+07 .19040690+0512429393+0411744563+05	BOUNDARY CONDITIONS B3 =13345838170+00 DESIRED VALUES	.60000000+02 PBWU MATRIX	.27016265+022232303 .22959898+05 .6920039 .68383079+047156651 .52613368+04 .2353504 .20075469+04 .1396728	47725645+06 .80673428+05 .14543571+09 .60563202+09
• 80191900135+07 • 16234500072-02 • 4788144528+00 • 000000000000 • 98075989691+05 • 40552357517+00 • 5941857502-04 • 11691040303401 • 50000000000000000	39845548+07 30531071+08 -13382413+08 -13644317+04 19818109+03	+13644317+04 -1.9818109+03 -2.3292432+04 -3.27670218+00 -4176600401 -20573959+02	12602466098+00 .53564081828+00	*10000000+03	25862826+02 -65046391+04 -18063730+04 +16227344+04	13399716+06 .26805648+05 .48209473+08 .14543571+09
81594275674=01 Q H 72921150604=04 FJ H 900000000000000000000000000000000000	.37262862+06 91715645+08 .29675744+08 .35319278+04 .1700158+04	.35319278+04 .17001584+04 27296576+04 22729658+02 18023271+02 .15423764+02	3462-03 82 # 2458-02 ERR #	.20000000+01 TOL =	11226690-01 .45041052+01 92612009+00 26057784+01	14613777+03 .29739799+02 .26805648+05 .80673428+05 .23822446+05
RHO = .81594275674=01 OM = .72921150604=04 F = .00000000000000000000000000000000000	.50478206+0728663020+08 .52441439+07 .13649068+0411984271+03	.13969068+04 11984271+03 22100786+04 .44573870+01 20397436+00 18425767+01	81 • • 38785493462-03 85 * • 20787902458-02	*64000000+07 AK = 1*000	.45591685-02 23989969+02 29333694+00 .1333875+02	.76070219+03 14613777+03 13399716+06 47725645+06

		19869991+03	.20330028+03	.36914250+02	.37897985+02
	ERS	ITERATION PARAMETERS			
• 12288645-02	-,85287577+03	-,35017915+04	63218803+03	-,10000912-00	.11000084•01
		СНЕСК			
84632800+02	,10516412-03	44953432-04	**87118683-04	.76800960-01	.171.69418-01
		ANSWER			
.12288645-02	85287577+03	-,35017915+04	63218803+03	10000912+00	.11000084+01
		RIGHT HAND SIDE			
10348370-03	66753718+02	24341445+03	60061113+02	-, 42319290-01	*23777612+00

.39860319000+15 .28608000000+02 .1403091856406 5681393615+04 10542703428+02 10542703428+02 .17998636364+01 .53567840000+02 .179998636364+01 .53567840000+02 .2714067684+08 .2714067684+08 .2214957331+02 .27140676824+08 .27140676824+08 .27140676824+08 .27140676824+08 .27140676824+08 .27140676824+08 .2714057931+02 .2714057931+02 .2716200000000000000000000000000000000000	00000000 00000000 00000000 00000000 0000	00000000 • 0000000 • 000000000 • 0000000	7EPS TAKEN • 39860319000+15 • 286080000000002 • 900000000000000000000000000000000000
GA AZ AZ LLZ ALT LLZ CHZ CHZ CHZ CHZ CHZ CHZ CHZ CHZ CHZ CH			6M. # 6M. # 8 ALT # # ALT # WRZ # LFZ # LFZ # ETA # ET
583441874+0458344132000+0758344132000+0417140022624+0426046334025875800133+025750000139+055750000139+0557500003418+0257500000000000000000000000000000000000			ALUES 61 INTEGRATION STEPS -32118715296+03 GM. = .39 -45907798355+07 PHI = .28 -12390043338+03 AZ = .95 -11425140490+00 ALT = .15 -12738566033+03 VRZ = .19 -33395893393+00 UZ = .55 -52203336758+06 LFZ = .66 -1666414237+06 DFZ = .25 -71905175652-01 ETA = .66
779182 112681444 117680 117680 117680 117680 117680 117680 117680 117680 117680 117680 117680 117680 117680	PXF/PUD MATRIX • 000000000000000000000000000000000000	DPXF/PUD MATRIX .00000000 .00000000 .00000000 .00000000	FINAL VALUES V = 32118 Z = 45907 DZ = 112390 DZ = 12738 VRY = 12738 VRY = 52203 FY = 52203 FY = 52203
2 Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	, , , , , , , , , , , , , , , , , , ,	7 X Y O	F I N A L C C C C C C C C C C C C C C C C C C
• 65000732772+07 • 62981421000+07 • 91182804430+01 • 91182804430+01 • 4875208100+00 • 10646549460+01 • 17066361408+02 • 4564672978+00 • 61922721324+02 • 1623450072-02 • 18986254448=12 • 1663828013-03 • 15653828013-03 • 15653828013-03 • 1663828013-03		.00000000 .000000000 .000000000 95082033-04 .11977354-03	.63936971567+07 .28998212124+07 .2876595499+03 75285949919+09 22281520483+03 78500176723+00 87397679795+06 29151872293+06
H H H H H H H H H H H H H H H H H H H		.00000000 .00000000 .26638305-03 .37521213-03	の
.104164160000000000000000000000000000000			.19161225673+04 .33756689366+07 .71080340123+02 .76755413941+00 .13280731000+06 .32140071341+03 .78476412895+01 .43223641677+01
X	000000000	.00000000 .00000000 .39523802-03 .98521091-04 78162776-06	X X X X X X X X X X X X X X X X X X X

• 63567840000407 • 7875000512-05 • 19509243583+02 • 96796309671+01 • 8104557671601 • 47458490507-03 • 47458490507-03 • 47458490507-03 • 47458490507-03 • 47458490507-03	• 45107039+10 • 31578559+11 • 17102158+11 • 55038633+06 • • 20649634+07 • 14196329+06		29601216691+00	<u>.</u>
BE FD	.30125512+11 .37660041+11 .74756737+06 74913845+07 2848345+07	.74756737+06 74913872+06 62848345+07 17054390+06 .54563673+05 .79170291+05	- 0 1 B4 B	
.63781660000+07 .57500000139-05 .87791612754+00 .14638907754+03 .10424594684+03 .10424594684+03 .10424594684+03 .16347354199-03 .000000000000000 .84039863544-01	301 301 301 301 301 301 301 301		7400	TERS
5750000139-05 87791612754+00 .14638907754+03 .10424594684+03 .3765408600400 .16347354199-03 .00000000000000000000000000000000000	**************************************	DPXF/PUD MATRIX81990314+0526451827+0627580168+0616715016+05167150140519535489+0515522700+05	83 = -,72194130097-01 DESIRED VALUES ,60000000+02 =-1	ITERATION PARAMETERS
######################################	PXF/PUC 1111 1255 1626 1626 1770	DPXF/PU 819 276 1676 198 198 198	83 = DESTRE	ITERAT
.58480127937+07 .16234500072-02 .47881444528+00 .000000000000 45851660936+06 44875208100+00 .15653828013-03 .15653828013-03 .15613913220+01 .500000000000+00 .4319519607+05	.18768153+08 .68448767+08 .3010559+08 .1872462+04 -34447772+04 -39303752+04	.18272462+04 34447177+04 39303752+04 18099384+03 .60248432+02 .702834822+02	-,70152147498+00 ,7667598002+00	. 499999999814-01
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.72584743+08 .782229+09 .79821399+08 .71001689+04 75972485+04 14824232+05	-71001689+04 75972485+04 14824232+05 63502446+03 -19465033+03 -25342554+03 -44119838+03	-02 B2 # -01 ERR # -01 ERR # -000	TOL =
8143+00 00604-04 00000 00000+03 9793+07 8595+05 77555-01 0000 8672+06 8672+06	. 7258 . 7982 . 7100 . 7100	. 7 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	64550-02	3765
.17201838143+00 .72921150604-04 .0000000000000 .400000000000+03 .86023959793+07 .10630828595+05 .10926637635+01 .43487837525-01 .00000000000	.24960868+08 59190950+08 .19466391+08 .1745976+04 2154705+04 32973143+07	.17745976+04 32973143+04 15924531+03 49610394+02 69225323+02		* .500
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.39860319000415 .286080000000000000000000000000000000000	000000000000000000000000000000000000000	.00000000 .00000000 .00000000 .000000000	.39860319000+15 .286080000000+02 .900000000000+02 .20725915184+03 .38727860947+03 .62343427873+00 79962830258+06 .40281318862+06
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. 12244760000+004 . 12244760000+004 . 1244760000000000000000+004 . 17660197907+01 . 17140022624+04 . 25918376546000 . 25918376451+000 . 60980882581+01 . 44504746547+00 . 57600000139+05 . 576000000000000000000000000000000000000	**************************************	DPXF/PUG MATRIX .00000000 .00000000 .00000000 .00000000	644 2006 2007 2007 2007 2007 2007
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•63567840000+07 •7875000512-05 •1852828-08 •185282018+01 •10351664246+02 •82816159425+00 •5345799522-03 •61031971743-08 •73152000000000 •11568578304+06	35537739+10 19276320+11 10293953+11 17998181+07 46721195+06 17089009+07	17998181+07 48721195+06 -17089009+07 -22429105+05 -54131017+03 20953384+05 -12877425+06	47375804241+00		20772186-04 95709152-02 19751786-02 2284056-04 -16241494-04	.44132085+00 85507736-01 70320593+02 15935207+03 78996992+02
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AE63781660000+07 FH57500000139-05 OMY14190874214+03 PANG10667873918+03 UOY37554827136+00 UODY37554827136+00 EXA00000000000 CK3500000000000 OHTI27681712582+00 LONG14005738527+03	PXF/PUD MATRIX	DPXF/PUD MATRIX15447200+0715160919+06 -1778333+07 -22392409+0534932843+041181297D+05	BOUNDARY CONDITIONS B3 #11330451666+00 DESIRED VALUES	.6000000+02	**B**B**B**B**B**B**B**B**B**B**B**B**B	60687158+06 12158061+06 12398060+09 31664884+09 14790433+09
. 78920681819+07 • 16234500072-02 • 47881444528+00 • 0000000000000000000000000000000000	15501162+07 37124732+08 15256243+08 23450940+04 6181279+03 36561281+04	.23450940+04 61812709+03 36561281+04 20057414+01 .33717659+01 36175974+01	14278231319+00 50761543015+00	.10000000+03 .4999999814-01	31292029+02 .77898861+04 21670900+04 .19497528+04	32158415+06 .68884973+05 .69194024+08 .12398060+09 .74209797+08
62-01 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	.91841052+07 -11210068+09 .34355825+08 .79822221+04 .749602221+04 -13815448+05	.7982221+04 .74496022+03 13815448+05 25928919+02 67600375+01 .23975553+02	60 mg 57 57 11 18	•20000000+01 TOL ==	26336123-02 .94717317+01 55376206+00 31987266+01	-,48963192+03 -,10172492+03 -,68884973+05 -,12158061+06
RHO = .81873058082-01 OM = .72921150604-04 F = .0000000000 1SP = .400000000000 PRES = .49954152712+04 PACH = .18517210231+01 CD = .49954152712+04 CK1 = .00000000000 J = .76800693035+05 D2 = .10566079878+03	.73220895+07 3539738+08 .65710570+07 36904310+03 31399208+04	.20619943+04 38904310+03 31399208+04 .56719472+01 .17237192+01 33838948+00	81 =36452122307-03 85 =13808861672-02	•64000000+07 AK * 1•000	35632504-01 45846900+02 14488648+01 .16751172+02	.23892391+04 48963192+03 32158415+06 60687158+06

+0-0+6+0556+		•11568229-02		75660532+01		•11568229=02		
-,78996992+02		-,10026168+04		.12481750-04		10026168+04	ERS	
15935207+03	RIGHT HAND SIDE	27288075+04	ANSWER	21274615-04	CHECK	27288075+04	ITERATION PARAMETERS	.20360934+03
70320593+02		75708662+03		.72384085*05		75708662+03		.20220019+03
89507736-01		57024756+00		24594288-01		57024756+00		.37939891+02
.44132085+00		.30515111+01		50237477-02		.30515111+01		.37652051+02

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######################################	PXF/PUD MATRIX .00000000 .000000000 .000000000 .000000	**************************************	
• 65000732772+07 • 62981421000+07 • 91182810306+01 • 9182810306+01 • 4978305699404 • 4978305699404 • 492767309422401 • 1796624752402 • 46727030079+00 • 16234500072=02 • 47881444528+00 • 00000000000000 • 88986254448=12 • 40215994202+00 • 8996254448=12 • 40215994202+00 • 8996254448=12 • 40215994202+00 • 899600000000000000 • 899600000000000000000000000000000000000		.00000000 .00000000 .89679086-04 .12088529-03 .14044834-03	.63981629237+07 .2647788518+07 .26349178016+03 .1847068841+01 35906732179+03 91178890045+00 929389855+06 40763896352+06
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L C C C C C C C C C C C C C C C C C C C			A S A A A A A A A A A A A A A A A A A A

• 63567840000+07 • 78750000512-05 • 8881759490+01 • 1032694490+02 • 83568911914+00 • 54097624496-03 • 61031971743-08 • 73152000000+06 • 14861131284+06	.1275219+10 26196830+11 -14620282+11 23806199+06 13489211+07 21045350+06	- 23806199+06 - 13489211+07 - 21045350+06 - 20952921+05 - 45615165+04 - 19533698+05	-•33968605171+00		- 18633769-04 - 86751023-02 - 98378284-03 - 95490268-04 - 73662321-05	.96810223+00 21409333+00 .83658989+01 .17439416+03
BE FD OMZ CHIY UODZ HTC NGCL'H H H NGCL'L	.16799305+11 72645118+11 .29306150+11 .27419065+07 .34687503+06 76812397+10	.27419065+07 .34687503+06 76407391+07 .24638874+05 26553612+04 .13076465+05	3-01 84 #	10000000+01	51613959+02 78138458+03 19890455+04 .42286094+04 .13352673+04	.20458505+06 43890234+05 .18603352+08 .44023031+08
AE	.7568964+10 20215460+11 20215460+10 8572822+05 44437899+06 22422799+06	0PXF/PUG MATRIX 85722822+05 44437899+06 22422799+06 19557346+05 22847651+04 7392903G+04	BOUNDARY CONDITIONS B3 =44573851233-01 DESIRED VALUES	.60000000+02 PBWU MATRIX	77622668+0251613945 20310716+057813845 .114183830+041989045 .11741707+05 .4228609 .98757836+03 .1335267 SIMULTANEOUS EQUATION MATRIX	.25888698+07 57226390+06 .49687386+08 .55338601+09 .64023031+08
.71364449781+07 .16234500072=02 .47881444528+00 .0000000000000000000000000000000000	. 54218855+08 .23921849+08 .23921849+08 .93642513+04 -92789618+04	.69602513+04 .33843564+04 .82789618+04 .12394242+02 .28376403+02 .73783174+01	29236744997+00 .45041994451+00	•10000000+03 •4999999814=U1	51146671+02 71940329+03 22798829+04 -32873718+04	.17122769+06 .35394847+05 .16613333+08 .49687386+08
731546364-01 Q	- 45093890+08 - 16373396+09 - 60126605+08 - 23612576+05 - 80971146+04 - 29340567+05	.23612576+05 80971146+04 29340567+05 .22332409+02 .79008190+02 .64008129+02	3573-03 B2 # 5510-02 ERR #	.20000000+01 TOL =	.33651062-01 .24759485+02 50779166+00 57764936+01	-,29227089+04 .64736918+03 -,35394847+05 -,57226390+06
RHO = .89731546364=01 F = .0000000000 ISP = .400000000000 PRES = .54719990322+04 MACH = .5194687318=01 CK1 = .056730030600 J = .95573003067+05 D2 = .10509151564+03	. 16866221+08 . 47293474+08 . 14289684+08 . 5959448+04 . 25568909+04	.59594448+04 .25568909+04 .070715365+04 .16505370+02 .21334200+02 .10657541+02	81 =57400393573-03 85 =50625276510-02	.6400000+07 AK = 1.000	20124638+00 11165239+03 47778634+00 .27363636402 .50233028+00	.13215545+05 -29227089+04 .17122769+06 .25888698+07 .20458505+06

.96810223+00	21409333+0U	.83658989+01	.17439416+03 RIGHT HAND SIDE	*85961032+U1	•76226890-04
.84477444+01	18/1417/+01	* 15363831+03	*78872304+03 Answer	-,26279326+U3	•91468365-03
-,32222317-02	.20436015-01	10196012-04	•12833431-04 CHECK	-,18982926-U5	•82294966+02
•84477444+D1	18714177+01	-•15363831+03	.78872304+03 ITERATION PARAMETERS	,26279326+U3 ERS	•91488365-03
.37939891+02	,38124511+02	.20360935+03	.20243845+03		

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	.39860319000+15	•28608000000+02	• 90000000000+02	•14030918566+06	######################################		20691540729+02	.17999863636+01	.635678400000+07	.78750000512-05	77140676824-08	.22431394296+02	•30492771216-U3	82848262873+00	•54287453755=03	.01019/1/43-UB	•731520000000+00	00000000000		• 00000000	• 00000000	000000000	00000000	000000000	0000000•	•0000000•		•00000000•	• 00000000	• 0000000	*0000000	0000000.	00000000	•0000000	INTEGRATION STEPS TAKEN	.39860319000+15	*28608000000+02	•90000000000•	.21933077446+05	•294 ⁸ 3466586+U3	.48451372494+00	69244970207+06	*31409251016*06	.05/0348/077400
į	••	# "I		1	747	04 = 1 LFZ =	DF 2 =	ETA =	9£	F.0	# 7W0	#¥1HD	DCEL#	# Z00	2000	ا ا ا	2C.XVII	LNGO		00000000	•00000000•	• 00000000	•00000000	•00000000	0000000	• 00000000		,00000000	•00000000	•00000000•	• ບບບບບບໍ່ເພັນ	.0000000	• 0000000	• 00000000	ATION S	H E 5	11	# 7 Y	ALT =	# 7×A	# Zn	LF 2 #	DF 2 = 10	I ₹
:	.79182741874+84	.12244760060+07	58346132000+04	-17680176196+01	P0+5292701111-	.26149355026+02	62423675945+01	.45557718401+00	.637816600000+07	57500000139-0S	87791612754+00	.24367580723+03	•91500003418+02	.38157691120+00	.18874743185-03	00000	.5000000000000+00 .15884027431+00	21023191184+03		1000.	0000•	0000	0000	000.	0000	0000.	×	1000*	0000	0000	1000	0000•	0000	0000.	52 INTEGR	.30490504769+03	42397036393+07	43917202939+02	11262665890+01	•13297795132+U3	.16303262979+00	.71254950016+06	•14193434539+U6	10-1503/17101
	.79182	.12244	- 58346	17680	1041/10	.26149	62423	.45557	.63781	575000	87791	.24367	•915000	.38157	18874	0000000000	.158884	.21023	PXF/PUO MATRIX	.00000000	•00000000•	,00000000	•00000000	• 00000000	00000000	•00000000	DPXF/PUO MATRIX	•00000000	•000000000	•00000000	•00000000•	00000000	00000000	•00000000	FINAL VALUES	.30490	42397	43917	11262	.13297	.16303	71254	, F 6 T + T •	*1001
	1t	= 2	m 70	# Z00	 - - -	 	DF.Y =	00	A FF	H	= Awo	CHIP=	PANG	00 Y	- 4000	EXA	CK3	H SNO I	PXF/PU	00.	30.	70.	00.	00.	00.	00.	DPXF/P	00.	00.	00.	00*	00.	00.	00•	FINAL	n >	= 2	# 70	= Z 00	VRY #	# 	 	DF Y	#
, i	.65000732772+07	62961421000+07	17567557000+04	.91182839786+01	+0+60696181/4+	.45035125020+01	18130906127+02	.46919919631+00	.61922721324+02	.16234500072-02	.47881444528+00	•00000000000•	*88986254448-12	40989705383+00	.94156871838-04	·/>>>993704/5+0U	• 500,000,000,000,00	.68028973356+02		• 00000000	• 0000000	• 00000000	00000000	•00000000	00000000	00000000•		• 00000000	• 00000000	• 00000000	** 68026332=04	•12314616=03	•14800444=03	•107u51a6=07		.63993663431+07	32617970520+07	.28101017482+03	14610468517+01	38129117558+03	45945727757+00	78394562585+06	**40697207975+06	00+62502404822•
	n œ	# **		# \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	H :	LF. X	DFX:	H C	3	Н	OMX II	e G	# JUNE	UCX III	# X 000	(L A	CK2	LAT		0000	0000	0000	0000	0000	0000	0000		0000	0000	0000	26158135-03	37373915-03	34/29551-03	68305993-07		# *	H .	μλo	₩ ¥00	# XX	# ×		X 70	"
,	,0000000000	.10416416000+07	505669500000+04	15169047902+01	13280731000+06	38124511840+02	20243845502+03	65821803840+03	31358995814-08	72921150604-04	, 00000000000	+00000000000+	,00000000000	68513884435-03	14005598208+02	12000053346-01	. 00000000000	5919948284-07		• 0 0 0 0 0 0 0	00000000	• 00000000	0000000.	000000000	00000000	00000000		•0000000°	• 0000000		-	•	•	•		.1777919U548+U4	35124752862+07	10987105642+03	+25083240533+U1	•132807310UU+U6	49999357626+03	10106926040+02	56052597851+01	50+0+85081285
	no• = _	Ħ	ŧŧ	I II	II	ALFA 38	•	•	RH0 = .31	0M = +72		•	•	•	Ħ.	n	CK	02 = .55		• 00000000	• 00000000	• 00000000	• 30000000•	• 00000000	00000000	n00n0¤aa•		000000000	900000000	*00000000	•42142701-03	.99014565-04	.24154452-04	•41949384-07		11.	X = 35	UX = *10	11 ×	9	•		·	AKEA

•63567840000+07 •78750000512-05 •77140676824-08 •93829649057+01 •10342283867+02 •10342283867+02 •51284525-03 •61031971743-08 •731520000000400 •17026869423+06	.71259237+10 30027205+11 .17521553+11 .1565730+07 26741855+07 17092959+07	•1565730+07 •26741855+07 •17092954+07 •61214121+04 •22127330+05 •18159742+04	23626468841+40	- 1682D452-04 - 085259728-02 - 78714352-03 - 042876188-04 - 065847126-05	*15584559+01 **32565404+00 *79682287+02 *43425895+03
8E	.32934965+11 85140843+11 .38930031+11 .98734159+07 13937171+08	.98734159407 38554664407 13977171408 .14832571405 .46271206405 .38125991405	84 = auoooao+a	67049429+02 90831984+04 13653804+04 .53135122+04 .93980414+03	EQUATION MATRIX -07 .1B439215+07 -07 .10789521+06 -09 .10789522+09 -10 .5430143+09 -09 .11348990+09
AE = .6378166UBUB+U7 FH = .575BUBUBL139-05 OMY = .87791612754+UB CHIP= .15058414272+03 PANG= .10016843492+03 UDY = .38157691120+09 UDDY = .18874743185-03 CK3 = .50000UBUBUB+UBUBUBH LONG= .19797509178+UBUBUBH LONG= .14504293287+U3	-23918636+11 -23918636+11 -86914646+10 -15602118+07 -15776675+07 -85289078+09	DPXF/PUD MATRIX 17602118+07 15776675+07 20826375+07 41496435+04 12815621+05 11682822+05 -37892963+05	33 =28836476671-02 DESIRED VALUES .60000000+021	-14760220+03 -14760220+03 -100703133+05 -10070571+04 -15084354+05 -61444956+02	**************************************
*55410030565+07 *16234500072-02 *47881444528+00 *0000000000000000000000000000000000	.21490485+08 62516284+08 .30854382+08 .12257036+05 67025560+04	.12257036+05 .67025560+04 .12039779+05 .10381228+05 .63527788+02 .1599500+02	-,27039721685+00 -,35909555639+00 -,10000000+b3	60444627+02 92419438+04 13615621+04 .42530096+04	*18382620+07 **38200401+06 *10565675+09 *53504117+09 *10789522+09
47347232325-01 4 = 72921150604-04 FJ = 0000000000000000000000000000000000	.77635084+08 -18701951+09 -81169876+08 -40108634+05 -18037144+05 -41356137+05	+40108634+05 -18037,144+05 -41356137+05 30290115+02 +18181850+03 78044192+02	6966-03 82 = 19287-U2 ERR = 10L = 10L =	.65654815-01 .30181156+02 23257347+00 69803857+01 43815684+00	-,72236653+04 -,15067768+04 -,38200401+06 -,20567039+07
KHO = .6734/232322=01 OM. = .7292115u6u4-04 F = .00000000000 1SP = .400000000000 PRES= .41207265845u4 MACH= .1708335/786+01 CDO = .51208912u62-01 CKI = .0000000000 J = .1065u648426+06 D2 = .1041317u411+u3	.25879958+08 53798055+06 .20475028+08 .10492219+05 53725499+04	.10495219+U553725499+U410488500+05 .94527651+01 .51797258+Q2 .23036377+Q2	B1 =19800796966-03 B5 =23677639287-02 .64000000+07 .20	35271361+00 16291784+03 48761671+00 .34421519+02	.34645626+05 7223653+04 .18382620+07 .98682040+07 .18439215+07

•73314003-04		.85913775-03		+11026857+03		+85913775-03		
,76299226+U2		.37869393+03		-,63795715-05		.37869393+03	ERS	
.43425895+03	RIGHT HAND SIDE	,35987576+04	ANSWER	.32102084-04	СНЕСК	.35987576+04	ITERATION PARAMETERS	.19956954+03
.79682287+02		.50412341+03		39761331-04		.50412341+03		.20243846+03
32505400+00		31183819+01		.50072063-01		31183819+01		,38169430+02
.15584559+01		.14853995+02		-,78397851-03		,14853995+02		.38124512+02

.39860319000+15 .286808000000+02 .9000000000+02 .14030918568+06	000000000 000000000 000000000 00000000	\$7EPS TAKEN \$39860319000+15 \$286080000000000 \$2813104861+02 \$30496961875+03 \$44467395756+06 \$31128523350+06 \$31128523350+06
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• 79182741874+04 • 12244760000000000000000000000000000000000		ALUES 48 INTEGRATION .32751201955+03 GM40069703325+07 PH13790037335+02 AZ84441076308+00 ALT .14173456077+03 VRZ95500451417+06 LFZ14466974128+06 DFZ1641033548+00 ETA
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7	00000000 00000000 00000000 00000000 0000	
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## FD OMZ	.45028265+11 -89408746+11 .46695181+11 .16916486+08 -78032902+07 -319466446+08	.16916486+08 78032902+07 19466446+08 23925682+05 .93831569+05 .77578386+04	0339-02 84 # -•10000000+0	-,63893715+02 -,20755872+05 -,10902773+04 ,59974577+04	.58520224+07 .58520224+07 .10332194+07 .48587795+09 .18645404+10
FH =5750000139-05 OMY =87791612754+00 CHIP= .15343766797+03 PANG= .99738658194+02 UDY =22084951584-03 EXA = .00000000000 CK3 = .500000000000000 CK3 = .21102585572+00 LONG= .14653001669+03	PXF/PUD MATRIX •15609704+11 •2552647+11 •10963980+11 •46912169+07 •3302688+07 •40545190+07	DPXF/PUG MATRIX - 46912169+67 - 33027688+07 - 40545190+07 - 98843172+04 - 30229521+05 - 75229033+04 - 70672889+05	B3 = .44803770339-02 DESIRED VALUES .60000000+021	-20453941+03 -20453941+03 -64981549+05 -12193682+04 -17065417+05 -57441899+03	SIMULTANEOUS EQUATION MATRIX •23670676+08 •5852022 41783270+071033219 •19491598+10 -4858779 •75149508+10 -1864540 •18645404+10 -4683698
•47131101088+07 •16234500072-02 •47881444528+00 •0000000000000 -11584425299+06 -13391820299+06 •13391820264-03 •12005165329+01 •5000000000000000	.30104418+0865347590+08 .36507252+08 .18099511+0510132701+05	.18099511+05 -10132701+05 -15607373+05 -18076605+02 -96403646+02 -26753781+02	16396237907+00 22390478825+00 .1000000+03	72225642+02 21971799+05 10783095+04 .48543949+04 73141044+03	.61399121+07 10831007+07 -50802802+09 -19491598+10
49564806591-01 4 = - 00000000000000000000000000000000000	10171290+0919392606+09 .97995780+08 .56719768+0527065339+05	.56719768+05 27065339+05 52712192+05 49458524+02 .26158435+03 54458560+02	5401-03 B2 x 9403-03 ERR = .20000000+01	.82187551-01 .47781380+02 -80049454-01 -69036928+01	13203401+05 .23307916+04 10831007+07 41783270+07
RHO = .49564806591=01 OM = .72921150604=04 F = .00000000000 1SP = .400000000000+03 ORNG = .76534254602+07 PRES = .30588181395+04 MAN = .18287018575+01 CK1 = .00000000000 U = .11351367176+06 D2 = .10568074811+03	.32753026+08 .55812307+08 .25369068+08 .15899266+05 .84168632+04	.15899266+0584168632+0414009937+0516236894+02 .78494712+0211227494+02	81 = .15920885401-03 85 =71485369403-03 .64000000+07 .20	-,48764335+00 -,27071666+03 -,93182879+00 ,38934082+02	.74810130+05 13203401+05 .61379121+07 .23670676+08

.89816458-04		.94417920-03		.10025876+03		•94417920-03	
.19654151+03		.14704920+04		14860026-04		.14704920+04	IRS.
.79996271+03	RIGHT HAND SIDE	+0+++5+16+	ANSEER	.29033506-04	CHECK	.67974544+04	ITERATION PARAMETERS
•20803528+03		.17074205+04		~ 40356239-04		•17074205+04	
-,45045326+00		-,40879432+01		.36922050-01		40879432+01	
.25533286+01		.23175705+02		13075632-02		+23175705+02	

.19745406+03

.19956954+03

+38244349+02

.38169431+02

TRIAL NUMBER 18

,39860319000+15 ,28608000000+02 ,900000000000+02 ,14030918566+06 -,56813936515+04 -,5798478013+00 -,1799863636+01 ,1799863636+01	77140676824-08 236769124+08 2367659124+08 30621930907-03 79798478013+00 56411413463-03 56411413463-03 56411912403-03 564119120000000000000000000000000000000000	000000000	.00000000 .000000000 .000000000 .0000000	.39860319000+15 .28608000000+02 .90000000000+02 .2448935522+05 .30283834173+03 .43857688643+00 .49939493104+06 .31411034685+06
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. 791827 . 122447 . 583461 . 176800 . 171400 . 470702 . 637926 . 6378265	- 27 20 20 20 20 20 20 20 20 20 20 20 20 20	PXF/PUD MATRIX	DPXF/PUG MATRIX .00000000 .000000000 .00000000 .0000000	334142 373297 1 • • 407845 1 • • 137333 1 • • 137333 1 • 142445
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.0000000000000000000000000000000000000	00000000000000000000000000000000000000	000000000000000000000000000000000000000	• • • • • •	• 15673917218+04 • 30856154477+07 • 3098780329435+03 • 13280731000+06 • 54736456146+03 • 14562095870+02 • 11834057207+02
			.00000000 .00000000 .39726315-03 .10337116-03 .35749013-05	
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5 7 8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	.59412380+11 .91319370+11 .54868996+11 .32247434+08 .14696902+08 .168399408+08	.32247434+08 14696902+08 28399408+08 72377796+05 .19043982+06 73476991+05	9-02 B4 m	-•10000000+01	03,11575717+03 06,43728217+05 02,16140245+04 05 -66590127+04 04 .24474997+03	.18134291+08 28143368+07 .19206655+10 .65265971+10
AE = .63781660000+07 FH =57500000139-05 OMY = .87791612754+00 CHIP= .15395230168+03 PANG= .9978669786+02 UOY = .40143086464+00 UODY = .24988302162-03 EXA = .000000000000 CK3 = .5000000000000 DHT1= .21083942278+00 LONG= .14816297705+03	26084010+11 26084010+11 3522561+11 13522561+11 0144403+08 57758433+07 68744560+07	DPXF/PUG MATRIX *10144403+08 57756433+07 68744560+07 21686585+05 56729589+05 18342495+05 12540213+06	BOUNDARY CONDITIONS B3 = .36641151709-02 DESIRED VALUES	.60000000+02	29645316+U3 14637223+D6 -43431768+D2 -18980D05+D5 1438278D+D4	.60543921+08 93956293+07 .64044510+10 .21787230+11 .65265971+10
• 43754418414+07 • 16234500072-02 • 47881444528+00 • 0000000000000000000000000000000000	.40369072+08 66414360+08 .42291616+08 .29425960+05 15176606+05 21268195+05	.29425960+05 15176606+05 21268195+05 50660684+02 .16625147+03 10053999+03	13670076801+00 .14968323748+0D	•10000000+03 •4999999814=01	-,97155593402 -,43040785405 -,16101170404 -,54348343404	.17805846+08 27624677+07 .18855467+10 .64044510+10
0604-04 FJ # # # # # # # # # # # # # # # # # #	.13028032+09 -119567301+09 .11513967+09 -88629210+05 -4062698105 -64062998105	.88629210+05 40626998+05 69982595+05 14375386+03 45501375+03	2300-04 82 m 9449-02 ERR =	•20000000+01 70L =	.10519256+00 .63301230+02 .41023984+00 68508701+01	26124163+05 -40541604+04 27624677+07 93956293+07
RHO = .44374020452=01 OM = .72921150604=04 F = .00000000000000000000000000000000000	.40849958+08 56429090+08 .30549271+08 .2594109+05 12759722+05 19196965+05	.25934109+05 12759722+05 19196965+05 42756639+02 .13428173+03 72376163+02	81 m .39831832300-04 85 m12862859449-02	.64000000+07 AK = 1.000	68482822+00 40799618+03 43476244+01 -43136455+02 40769471+01	.16835763+06 26124163+05 .17805846+08 .60543921+08

+10007135-03		.99246710-03		•78270616+02		.99246710-03		
.43610712+03		.39613782+04		-,80097816-05		.39613782004	ERS	
.14536811+04	RIGHT HAND SIDE	.13484261+05	ANSERR	.22541456-04	CHECK	.13484261+05	ITERATION PARAMETERS	.19474484+03
.42930574+03		.39686769+04		46022117-04		.39686769+04		.19745407-03
62923477+00		59117701+01		.47285006-01		59117701-01		,38055189+02
.40575343+01		.38163992+02		.33014589-02		.38163992.02		.38244349+02

.39860319000+15 .28600000000+02 .90000000000+02 .14030918566+06 .56813936515+04 .78147700142+00 .35672199707401 .17998636401 .179998636401 .179998636401 .179998636401 .1799986364000 .179000000000000000000000000000000000000	000000000	000000000	\$7EP\$ TAKEN •39860319000+15 •286080000000000000000000000000000000000
GM AALT AALT AALT CON			
• 79182741874+04 • 12244760000000000000000000000000000000000			ALUES 43 INTEGRATION -40725547785+03 GM -1042385906+01 AZ -1042385906+01 AZ -316753790034+03 AZ -16753790034+03 VRZ -54165867170-02 UZ -11186067424+07 LFZ -13398204609+00 EZ
7 2 2 1 8 2 8 2 8 8 2 8 8 8 8 8 8 8 8 8 8	PXF/PU0 MATRIX • 000000000 • 000000000 • 000000000000	00000000 •00000000 •00000000 •00000000	FINAL VALUES V # 40725 Z #34015 DDZ # .10423 VRY # .54165 LFY # .54165 CFY # .13398
COCCOOTACCOOCCCCOOCCCCCCCCCCCCCCCCCCCCC	x 4/7 00000000000000000000000000000000000	7XF700000000000000000000000000000000000	H H H H H H H H H H H H H H H H H H H
• 65000732772+07 • 62981421000+07 • 91182927255+01 • 97329988103+00 • 15422948280+01 • 15422948280+01 • 16434280+01 • 1642721324+02 • 16234500072-02 • 16234500072-02 • 16234500072-02 • 162345000070-02 • 162345000000000000000000000000000000000000		.00000000 .00000000 .00000000 =.84367598=04 .12865919=03	.44013426500+07 -43612254022+07 -2932886187+03 -279286187+03 -51312225612+03 -89965553655+00 -40009635648+06 -4871445799+06
T		00000000 00000000 28222839-03 36948061-03 35685450-03	7
.0000000000000000000000000000000000000	000000000000000000000000000000000000000	• • • • • •	.14891211058+04 2976179968+07 2825555557+03 37012152563+01 .13280731000+06 .63961389436+03 .16791369924+02 .1679136924+02
		.00000000 .00000000 .38172543-03 .10493822-03	. 14891 . 29976 . 28255 . 32825 . 3280 . 63961 . 18700
X X X X X X X X X X X X X X X X X X X		0000 0000 0000 0000 0000 0000 0000 0000	H H H H H H H B B B E T A A C K B D D X A C K B C C A A B II B H H H H H B B B B C B A B B B B B B B B B B B B B

• 63567840000+07 • 78750000512-05 • 77140676824-08 • 31034907411+00 • 10920612420+02 • 7814770142+00 • 57212391619-03 • 61031971743-08 • 73152000000000		8 -13674676+08 810385905+08 853269310+07 666717327+05 617372386+06	23896472430~01 01	
BE PD OMZ B N	63522626411 90253813411 .58449224+11 .39061571+08 29102270+08	.39061571+08 19321052+08 29102270+08 19963113+06 17037005+06 47380016+06	-02 84 = -	
0000+07 2754+00 2754+00 6179+03 2231+02 6042+00 7738-03 00000 0692+00	40 QQ - 20 Q	1 1 1 1 1	5851-02	TERS
5781660000+075500000139-0587791612754+00 .15411456179+03 .99457082231+02 .4054756042+0027242447738-03 .600000000000000 .500000000000000000000	PXF/PUD MATRIX -2086870+11 -25864538+11 -14591832+11 -17577606+08 -78041424+0770454019+07	DPXF/PUD MATRIX • 13277606+08 • -78041424+07 • -52049757+05 • 71889622+05 • -48200052+05 • -48200052+05 • -53495842+05 • -53495842+05	63 * .93050035851-02 DESTRED VALUES .60000000+021	ITERATION PARAMETERS •19677676+03
# # # # # # # # # # # # # # # # # # #	PXF/PU	DPXF/7 11.13.13 11.148 11.170	63 DESI	ITERAT • 19
.45321909331+07 .16234500072=02 .4788144528+00 .000000000000 10042123124+06 4732988103+00 .22029655906=03 .10059600000000000000 .40387829772+05 .21956586748+02	.43151522+08 -65527325+08 .44969277+08 .35284771+05 -10522082+05	.35284771+05 19407363+05 20522082+05 14485157+03 .224977775+03 1876719+03	.16596447844+00 .16596447844+00	.4999999814-01
6 F O E X S O T O E O E O E O E O E O E O E O E O E	-13795602+09 -19250896+09 -12268327+09 -10405953+06 -50216115+05 -1006210+05	-10405453+06 -50216115+05 -4107006210+05 -41070925+03 -4107473+03 -4107473+03 -4107473+03	-03 82 == -02 ERR == -20000000+01	TOL =
.33661435655-01 .02921150604-04 .000000000000 .400000000000+03 .68284013121+07 .21127168764+04 .4302451375-01 .44302451375-01 .00000000000000000000000000000000000	. 1379 . 1925 . 1026 . 1040 . 1000	11.040.000.000.000.000.000.000.000.000.0	.41962212480-03 .1697808U414-02 3000+07 .200	9.88.
.33661435655-0 .72921150604-0 .0000000000 .40000000000000 .68284013121+0 .21127168764+0 .44302451375-0 .44302451375-0 .00000000000 .12786438592-0	.43133969+08 .55606678+08 .32765838+08 .31346237+05 .1615914+05	.31346237+05 -16155834+05 -19215914+05 -12248317+03 -17425908+03 -1116890+03	4196221 1697808 .64000000+07	<pre>* *500 *********************************</pre>
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.39860319000415 .286080000000002 .9000000000002 .14030918566+06 56813936515+04 10349017289+00 1034017289+00 1034017289+00 .1799863634601 .1799986363600 .1799986363600 .1799986363600 .1799986363600 .1799986363600 .179998017289+00 .2375710509+00 .2375710509+00 .2375710509+00 .2375710509+00 .2375710509+00 .237571050900000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000	.39860319000+15 .286080000000+02 .900000000000000000000000000000000000
6 M A A A A A A A A A A A A A A A A A A			ATION S GM PHI M VRZ ALT LVZ LVZ ETA H H H H B ETA H H H H B
58346132000+07 58346132000+07 17680050086+01 17140022624+04 17140022624+04 17140022624+04 17140022624+04 17140022624+04 17140022624+04 5720392011+00 5720392011+00 5720392011+00 5720392011+00 57500000139-05 5750000139-05 5750000139-05 5750000139-05 5750000139-05 5550183656-03 5550000000000000000000000000000000000			ALUES 44 INTEGRATION STEPS -34101146299+03 GM 8 .39 -34871526049+07 PHI 8 .28 -332608289450+02 AZ 8 .90 -33129848+03 VRZ 8 .30 -39216540116-01 UZ 8 .44 -10243523702+07 LFZ 8 .47 -11319175509+06 DFZ 8 .31
V V V V V V V V V V V V V V V V V V V	**************************************	.00000000 .00000000 .00000000 .00000000	FINAL VALUES V 341 Z 342 DZ 343 VY 362 VY 362 VY 86392 VY 8
65000732772+076598142100040791182916190+019534780199+011547801818+0023447801818+001824501072-021824501072-021824501072-021824501072-021824501072-021824501072-031824501072-0318277997105-0318577997105-0318577997105-0318577997105-0318577997105-0318577997105-03	000000000000000000000000000000000000000	.00000000 .000000000 .000000000 84820292-64 .12823860-03 .18044984-03	.44001536539+07 -42507752149+07 -26807081542+03 -23145745373+01 -44369002695+03 -69713818639+00 -64771083643+06 -45598336029+06
**************************************		.00000000 .00000000 .27766386-03 .37006314-03 .35400338-03	7 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
- 505669500000000000000000000000000000000	000000000000000000000000000000000000000	1103	.15478240678+04 30492265470+07 20764348192+03 .31280731000+06 .55747628285+03 .14880291267+02 .12964156563+03
D X Y X X X X X X X X X X X X X X X X X	000000000000000000000000000000000000000	.0000000 .0000000 .39341442-03 .10377697-03	A K K K K K K K K K K K K K K K K K K K

. 78750000512-05 . 77140676824-05 . 22475185647+01 . 10697731789+02 . 5989017289+00 . 56611658002-03 . 61031971743-08 . 73152000000+00 . 21365155632+06	1132143729+11 1232143729+11 13 -22780076+11 14 -11733731+08 1682095942+07 1665079042+07 16621634+10	8 11733731+D8 8 62095942+07 8 65079042+07 5 36033466+05 6 59349401+05 6 54434220+05 6 15865323+06	47000136875-01		3 18205629-04 5 10181699-01 4 175999-01 7 4775992-04 8 20918253-04	+45318862+01 7 +67288861+00 0 +49266628+03 0 •16476623+04
139-05 FD 85 87 87 84 84 84 84 84 84 84 84 84 84 84 84 84	. 61838276+11 - 91560572+11 . 56184045+11 . 35643856+08 - 16326098+08 - 16576+10+08	.35643856+08 36326098+08 30169710+08 95915427+05 10393888+06 43567514+06	580-02 84 m 1000000000000000000000000000000000		-,12360926+03 -,49328284+05 -,19231774+04 ,67666246+04	110N MATRIX .22235601+08 33039245+07 .24176531+10 .81142456+10
FH =57500000139-05 OMY =67500000139-05 CHIP= .15387413509+03 PANG= .99836341133+02 UOY = .40283791649+00 UOY = .25551838556-03 CKA = .000000000000 CK3 = .50000000000000 UHI = .21904969325+00	PXF/PUG MATRIX •20343514+11 •26180383+11 •13932541+11 •1348285+08 •63741422+07 •73833717+07	DPXF/PUO MATRIX •11348285+08 •63741422+07 •73833717+07 •27354459+05 •61152058+05 •27711863+05 •10728064+06	63 = .28093224580-02 DESIRED VALUES .60000000+021	PBWU MATRIX	31809816+03 16182307+06 7911843+03 19288595+05 15904322+04	SIMULTANEOUS EQUATION MATRIX .72789649+08 .2223560 -10815305+083303924 .79066136+10 .24174553 .26562012+11 .8114245
.15234500072-02 .15234500072-02 .47881444528-00 .0000000000000000000000000000000000	.42069949+08 -66533681+08 .43236273+08 .31972390+05 -1646405+05 -323164316431+07	-31972390+05 -16460605+05 -22316432+05 -67988532+02 -17918791+03 -12699868+03	t .	•4999999814=01	10334282+03 48181296+05 19282414+04 -55286430+04	.21676592+08 32199686+07 .23567067+10 .79066136+10
1111-01 6 8 00604-04 FJ 8 000000 000 000 8 5993-07 XRNG 5993-07 XRNG 5993-07 CDX 8 0000 CK2 8 1457-06 HT1 8	.13506226+09 .11788325+09 .11788325+09 .95761086+05 .43665309+0573398665+05	.95761086+05 43966309+05 73398665+05 19635961+03 -48893254+03 33332878+03	3870-03 ERR #	101	.10848245+0U .66U32084+U2 .71947920+0 66928953+01 .56761163-01	29650272+05 .44055637+04 32199686+07 10815305+08
KHO # -12715277111=01 M # -72921150604=04 ISP # -400000000000 DRNG# -69761675993+07 PRES# -26632505723+04 MACH# -18913080738+01 CDO # -47472007194=01 CKI # -12715451457+06 D # -12715451457+06 D # -12715451457+06	.42222419+08 56503496+08 .31376942+08 .28183402+05 1383402+05 20194111+05	.28183402+05 13839402+05 20194111+05 5729323+02 94100298+02 26631093+03	85 *92200333870-03	AK # 1+000	-,73351006+00 -,44450441+03 -,66788414+01 ,43865306+02 -,43789908+01	.19957265+06 29650272+05 .21676592+08 .7278649+08

.42374004+D262866673+D1 .45537709+D4 .15274969+O5 .460922D2+D4 .10169246-D2	ANSWER •62122449-02 •53995277-01 -•48199403-04 •16122354-04 •39773941-07 •60444659+02	CHECK 2374004+02	ITERATION PARAMETERS 8197059+02 .37841124+02 .19677677+03 .19368307+03	.42374004+02 .62122449-02 .42374004+02	. 62866673+01 . 53995277-01 . 62866673+01		• 15274969+05 ANSWER • 16122354-04 CHECK • 15274969+05 ITERATION PARAMETE • 19368307+03	.46092202+04 .39773941-07 .46092202+U4	.10169246-02
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TRIAL NUMBER 21

.39860319000+15 .9000000000000000000000000000000000000	000000000000000000000000000000000000000		000000000000000000000000000000000000000	**************************************
		000000	000000	
9 M	- C C C C C C C C C C C C C C C C C C C			ATIO GM PHI AZZ ALT VRZ UZ EFZ
79182741874+04 12244760000+04 583461320000+04 1740022624+04 17140022624+04 17140022624+04 27331576260+04 6156436861+01 61564038861+01 61560000139-05 8779166000+07 8779164073996-03 27164073996-03	15884027431+00 21023191184+03	0000000		-45267834778+03 GM -36283090665+07 PH1 -21175925962+02 AZ -3695173268+07 AZ -13836705221+03 UZ -11466838727+07 LFZ -16728382583+06 DFZ -12571019274+00 ETA
-79 i 8274 1874 -122447 60000 -58 346 13 200000000000000000000000000000000000		/PUO MATRIX .000000000 .000000000 .000000000 .000000	**************************************	FINAL VALUES V = .45267 Z =36283 DZ = .7175 ODZ = .13183 UY = -114664 OFY = .1528
	# 5 H O I	PXF/PU0 • 0000 • 0000 • 00000 • 00000	×	
S P O S P P P P P P P P P P P P P P P P	353	r X	0	FIN V 2 DDZ VRY UY LFY CFY
• 65 0 0 0 7 3 2 7 7 2 + 0 7 2 4 0 0 1 1 5 2 5 5 5 1 0 0 4 0 4 0 4 1 1 5 2 5 2 2 1 4 4 0 1 1 2 5 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	.0000000000000000000000000000000000000	000000000000000000000000000000000000000	.0000000 .0000000 .0000000 8499666-04 .12804893-03 .19594731-03	.44019820763407 .43169368848+07 .31505200579403 .3322197276403 .5564268375+03 .89760054150+00 .5886966995+06 .49433973014+06
			033	01 36 61 M P2 00 00 68 63
	LAI		0000 0000 3243 3243 7271	R C C C C C C C C C C C C C C C C C C C
.1041641600000 .104164160000+07 50566950000+09 .13280731000+06 .7745938217104 .13280731000+06 .7745938217+09 .37841124389+02 .19368307047+03 .55821803840+03 .65821800000000 .0000000000000 .000000000000	0000000000 55122492919-07		.00000000 .00000000 .00000000 03 .28383243-03 03 .386070515-03 04 .35607071-03	-,14873794084+04 -,3030441157+07 -,3243632288+03 -,3280731006+06 -,69226623641+03 -,16616903154+02 -,21626230195+02
1	.551	00000000000000000000000000000000000000	.0000000 .0000000 .0000000 .37456945-03 .16507928-04	1 1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
CATCHTORAGE CECCX CCACTO CATCACCX CCACTO CATCACCX CCCCC AAAA CATCACCACCACCACCACCACCACCACCACCACCACCACC	2 20		0000 0000 0000 0000 0000 0000 0000 0000 0000	HERRERSE BANDX AAA GX BAND BERRESS

.63567840000407 .7875000512=05 .77140676824=08 .75531175961400 .109959100830402 .7540258133400 .56607680608=03 .61031971743=08 .73152000000400	• 18211465+11 • • 32030341+11 • • 2368486+11 • 13228180+08 • • 113228180+07 • 17238738+107 • 13228180+08 • • 13228180+08	ຕ ຕ	=
8E 0MZ CH1Y UOZ UOZ HTC HTC LNCOS LNCOS LNCOS	62151330+11 58392436+11 58392436+11 37083361+08 5824194+08 50019689+10	21567730+06 31560017+06 16252002+06 83935555+06 3-01 84 =	10+0000000++
.63781660000+07 5750000139-05 15385458378+03 99010208573+03 9602444362+00 27164073996-03 27164073996-03 27164073996-03	1 11 11		O2 METERS 3
	PXF/PUD MATRIX -206-8025+11 -26077012+11 -14496374+11 -12907807+007000000000000000000000000000000	63292605+05 .79679099+05 43117448+05 12712135+06 ROUNDARY CONDITIONS B3 = .1698930561	DESIRED VALUES .60000000+02 ITERATION PARAMETERS .19600334+03
7 T T T T T T T T T T T T T T T T T T T	T I X II	B B B B B B B B B B B B B B B B B B B	DEST
.48904820489+07 .1623420072-02 .4788144628+00 .00000000000000000 9280253125+05 48362690997+00 .23397937407-03 .94714851243+00 .50000000000000000000000000000000000	.42061858+08 -66130966+08 -45059778+08 -34502486+05 -19933158+05 -35122407+07 -34502486+05 -19933158+05	15551122+03 -26011653+03 18706565+03 63516829+03 35762535701+00	.35959653997+00 .10000000+03 .49999999814-01
# # # # # # # # # # # # # # # # # # #	.13517753+09 .12265915+09 .12265915+09 .10141629+06 .1045623405 .1045623408 .10141629+06	47406859+03 -71381891+03 47359719+03 18578377+04	.20u00000+61 .20u00000+61 .38108076+62
6575-01 0604-04 00000-03 00000+03 7569+04 7569+04 7730-01 7730-01 7346+06	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-,4740 -,7138 -,4735 -,1857 -,1857	.200 .200 .3810
.31007416575-01 .7221150604-04 .0000000000000 .4000000000000 .68892168209+07 .19545357569+04 .23303436287730-01 .0000000000000000000000000000000000	.42407184+08 .32675464+08 .326754604+08 .30724407+05 .15399570+05 .30670233+07 .30724407+05	13216346+03474 -20110948+03 -713 13487707+03473 46273258+03185 161949476623-03	* .28780750332-02 .64900000+07 .20 * .500
7 C C C C C C C C C C C C C C C C C C C	1	10132 10134 10134 10134 10134	2 4 5

INITIAL VALUES

.63567840000+07 .78750000512-05 .17140676824-08 .19331261524+01 .10743923366+02 .10743923366+02 .10743923366+02 .10743923366+03 .10743923366+03 .107439771743-08 .7315200000000000000	32264789+11 32264789+11 .23159971+11 .12763398+08 89538144+07 66336101407	.12763398+08 69538744+07 64336101+07 44192949+05 .10129646+06 66880736+05	-,37382097303-01 1	18876727-04 10485573-01 13326259-02 48743789-04 -23359501-04	•50189572+01 ••70749260+00 •55441426+03 •18383691+04
BE FD OMZ # # CHIY # # # UDZ # # UDZ # HTC # RCKV # CCLI# CLI#	.63646325+11 .91928187+11 .57305144+11 .38135119+08 .1752388+08 .31163841+08	.38135119+08 17752388+08 31763841+08 12463608+06 .22772231+06 13177235+06	84 = 8000000000000000000000000000000000000	13101538+03 54058960+05 23515784+04 .68576887+04 .14357775+03	.26146564+08 .26146564+08 .36883838+07 .28874807+10 .96076359+10
AE = ,63781660000+07 FH = -,57500000139-05 OMY = -,87500000139-05 CHIP= ,15380548096+03 PANGE ,99857272548+02 UOY = ,99857272548+02 UOY = ,99857272548+02 UOY = ,99857272548+02 CK3 = ,900000000000000000000000000000000000	PXF/PUD MATRIX	DPXF/PUD MATRIX • 1225556468 • 69154396407 • 76237731407 • 34264802405 • 4681540405 • 4681540405 • 4881540405 • 48899933405 • 83899933405	83 = .24474419789-02 DESIREO VALUES .60000000+021	33779718+03 17516062+06 20228561+04 .19551248+05	SIMULTANEOUS EQUATION MATRIX •84554288+08 •11927494+08 •93299328+10 •31070554+11 •96076359+10
• 44747324582+07 • 16234500072=02 • 47881444528+00 • 000000000000 • 11429816235+06 • 146254390458+00 • 19782982180=03 • 11191760232+01 • 5000000000000000000000000000000000000	.43307462408 66750412408 .44057331408 .33892851405 17670131405 22749526405	.33892851+05 17670131+05 22749526+05 89337389+02 .19130163+03 15136880+03	57781353085-01 -68864559724-01 .10000000+03	10919413+03 52601783+05 23633166+04 -56078402+04	.25400377+08 35822180+07 .28050221+10 .93299328+10
1142-01 Q	- 13860143+09 - 19636060+09 - 12023134+09 - 10109465+06 - 46999980+05 - 75151041+05 - 10515836+08	.10109465+06 46994980+05 75151041+05 2625223+03 .52048267+03 39916337+03	.831-04 B2 = 1085-03 ERR = 100000000+01	.10985519+00 .67358462+02 .11369812+01 64708787+01	- 32469801+05 . 45803425+04 - 35822180+07 - 11927494+08
RHO = .41462149142=01 OM = .72921150604=04 F = .000000000000 ISP = .4000000000000 PRES= .25768389185+04 MACH= .19413589538+01 CK1 = .0941358968=01 J = .10943950160+03	.43248109+08 56676048+08 .32075975+08 .29885130+05 .14829401+05 .30810366+07	.29885130+0514829401+052067980+0575542705+0215180381+0311342395+03	81 = .74600866831-04 85 =47548434085-03 .64000000+07 .20	77867552+00 47759359+03 10037989+02 .44519407+02	.23019987+06 32469801+05 .25400377+08 .84554288+08

.11172641-03		.60441870-03		•46704679+02		.60441870-03		
.56964450+03		.28614117+04		-,83701639-05		.28614117+04	ERS	
.18383691+04	RIGHT HAND SIDE	.93859782+04	ANSKER	.12772809-04	CHECK	+93859782+04	ITERATION PARAMETERS	.19481683+03
.55441426+03		.28244596+04		23870473-04		.28244596+04		.19600335+03
70749260+00		36474035+01		,20708640-01		36474035+01		,38056037•02
.50189572+01		.25909322+02		.90825529-03		.25909322+02		.38108076+02

INITIAL VALUES

.39860319000+15 .28600000000+02 .90000000000+02 .14030918566+06 .5681393615+04 .78193390638+00 .1799863636+01 .1799863636+01 .1799863636+01 .1799863636+01 .239767000012-05 .23976706032+02 .23976706032+03 .23976706032+03 .23976706030000000000000000000000000000000	00000000000000000000000000000000000000	\$1EPS TAKEN \$39860319000+15 \$286000000000+02 \$7000000000000000 \$25323753443403 \$32356018443*03 \$4477190297*00 \$32069749972*06 \$32069749972*06
64 ALT N N N N N N N N N N N N N N N N N N N		
.79182741874+04 .12244760000+07 .58346132000+04 .17680014575+01 .17140022624+04 .40332591380+02 .522133591380+02 .6221362206+01 .6221362206+01 .6221362206+01 .6221362206+01 .6221362206+01 .6221362206+01 .622136284+02 .6221754+00 .6378166000139-05 .6378166000139-05 .63884583851+03 .60000000000000000000 .15884027431+00 .15884027431+00		LUES 43 INTEGRATION 337159167240+03 GM 19636606964+02 AZ 24801914260+00 ALI 14920820961+03 VR2 10565245302-01 UZ 11190082077+07 LFZ 14788809644+06 DFZ 13045282127+00 ETA
1224476000+071224476000+07**1224476000+07**17680014575+01**1740022624+07**1740022624+07**1740022624+07**17400262624+07**1740020000000000+07**17400241840241840241184403**1023191184403**12244000000000000000000000000000000000	PXF/PUD MATRIX	VALUES 43 INTEG -37159167240+03 -33422136788+07 -196336606964+02 -248019142604902 -14220820961+03 -10565245302-01 -11190082077+07 -11188809644+06
V Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	A	FINAL VALUES V
• 65000732772+07 • 62981421000+07 • 91182926621+01 • 9182926621+01 • 19783056909+04 • 15701804633+01 • 15701804633+01 • 1806986147+02 • 1806986147+02 • 1822721324+02 • 1623450072-02 • 16234500072-02 • 16234500072-02 • 162345000000000000000000000000000000000000	.00000000 .00000000 .00000000 .00000000	.64002054858+07 .27288708238+03 .275881284403 -47821837121403 -6978539777+00 -69398426096+06 -47398735489+06
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. (000000000000000000000000000000000000	•••••	. 14860082238+04 - 2933550531+07 - 25145062127+03 - 3552111377+03 - 13280731000+06 - 59636154582+03 - 15730751241+02 - 17306733191+02
	.00000000 .00000000 .00000000 .00000000	1 2 2 4 4 8 4 4 8 4 4 8 4 4 8 4 4 8 4 8 4
0	0000000 000000000000000000000000000000	H H H H H H H H H H H B B F H B B B F H B B B B

.6356784000407 .7875000512-05 .6053552437+00 .10873410107+02 .578193390638+\$0 .5744680046-03 .5744680046-03 .57476800000000	.20676573+11 32049500+11 .24024954+11 .16462374+08 10814395+08 75595251+07	.16462374+08 .10814395+08 .75595251+07 .66026531+05 .12117509+06 .18322017+06	-•43815794668-02		- 19895038-04 - 11121523-01 - 15777878-02 - 50049996-04	.63986801+01 .83088261+00 .74220136+03 .24181335+04
BE FD OMZ CHIY CODZ UDDZ H H HTC NGCRU	. 91330859+11 . 91330859+11 . 60099876+11 . 47378943+08 - 21818124+08 - 34906888+08	.47378943+08 -21818124+08 -34906888+06 -19624413+06 -2814369+06 -28143699+06 -49130738+06	3-02 B4 E		-,15152156+03 -,69293226+05 -,34817379+04 -,70430573+04 -,35228042+01	.40089546+U8 52091487+U7 .46448813+10 .15181470+11
AE	-2293124+11 -22193124+11 -26192952+11 -15175408+11 -15175408+11 -83328960+07 -86600184+07	. 15448058+08 8328960+07 86600184+07 86600184+07 866597+05 5886597+05 5886591+05 55796881+05	BOUNDARY CONDITIONS B3 = .23200161353=02 DESIRED VALUES .6000000+02 =-1	PBWU MATRIX	39409892+031515215 21678837+066929322 51777994+043481737 -2007984+05 .7043057 20072852+04 .3522804	.12524050+09 .16273644+08 .14502844+11 .47431394+11
• 45310270575+07 • 16234500072-02 • 47881444528+00 • 0000000000000000000000000000000000	.46876964+08 -66169034+08 .46013388+08 .46680039+05 -20727067+05 -24795142+05 37825664+07	.40680039+05 20727067+05 24795142+05 13981327+03 -22837034+03 21473292+03	*19393723386-01 *19393723386-01	•4999999874-D6		.38305107+08 49764081+07 .44384111+10 .14502844+11
38711286786-01	.14848295+09 .19422687+09 .12593317+09 .11999049+06 .5448024+05 .82058638+05	1999049+06 54848024+05 82058638+05 41609090+03 .6237108+03 62893860+03	2523-04 B2 = 2949-03 ERR = 20000000+01	10L ×	.11843059+00 .74446911102 .20459887+01 61537009+01	42976515+05 .55844220+04 49764081+07 16273644+08
KHO = .38711286786=01 OM = .72921150604=04 F = .0000000000 ISP = .400000000000 RNG= .400000000000 PRES= .2413245442+07 MACH= .2018661568+01 CD0 = .45775044795=01 CK1 = .00000000000000 J = .1328688687+06 D2 = .1176316924+03	.46075376+08 56133790+08 .33837625+08 .35816762+05 173466326+05 22666329+05	.35816752+05 1734626405 22666329+05 11749710+03 17875213+03 16367351+03	81 x .64215352523-04 85 x .14434342949-03 .64000000+67 .20	AK # 1.000	-,90,159816+00 -,57299407+03 -,18080193+02 ,45700192+02	.33076539+06 .42976515+05 .38305107+08 .12524050+09

		.19494523+03	.19481683+03	,38084305+02	.38056037+02
	ERS	ITERATION PARAMETERS			
21195170-03	-,13380991+04	41647924+04	12760071+04	+14275096+01	-,10985842+02
		CHECK			
.28173243001	-,24032672-05	.10088733-05	.20524217-06	-,22409045-02	49336176-03
		ANSWER			
21195170-03	-,13380991+04	41647924+04	12760071+04	.14275096+01	10985842+02
,		RIGHT HAND SIDE			
•12618137-03	,77579029+03	.24181335+04	•74220136+03	-· 83088261+00	.63986801+01

TRIAL NUMBER 24

	.39860319000415 .286080000000000 .900000000000000000000000000	.5768006765-03 .61031971743-08 .7315200000400 .0000000000	00000000 00000000 00000000 00000000 0000	000000000000000000000000000000000000000	39860319000+15 *28608000000+02 *2619640507+05 *32474726772403 *45471363548+00 =*3629084608+06 *3219232298+06 *3219232298+06 *37759880243+00
	9 M M M M M M M M M M M M M M M M M M M	UODZ# HTC RCRV# DCLI#			
L VALUES	- 79182741874+04 - 1224476000407 - 58346132000404 - 17680015772+01 - 17140022624+04 - 27324293635+02 - 62300298129+01 - 45467675452+00 - 5750000139-05 - 87791612754+00 - 238937588+00 - 238937584+00 - 238937584+00 - 238937584+00	2733065615-03 .00000000000 .500000000000000 .15884027431+00	**************************************	• ************************************	FINAL VALUES 118 INTEGRATION V = .36497034494+03 GM = .35282151325+07 PHI = .21772241108+00 ALT = .21772241108+00 ALT = .21772241108+00 ALT = .11958380974+03 VKZ = .518085519-02 UZ = .11199808945+07 LFZ = .112862220388+00 ETA = .12862220388+00 ETA = .212862220388+00 ETA = .2128622020000000000000000000000000000000
INITIAL	H H H H H H H H H H H H H H H H H H H	CK3 # CK3	PXF/PU		F I N A L N L L L L L L L L L L L L L L L L
	-62981421000+07 -17567557000+07 -91182927327+01 -97182927327+01 -971829299999 -14714286436690 -1620878683401 -1620878683401 -1620878683401 -1620878683400 -1620878683400 -1620878683400 -16208789899000000000 -16208986254448-12 -189986254448-12	.22149505267-03 .75999370475+00 .50000000000+00 .00000000000	000000000000000000000000000000000000000	.00000000 .000000000 .000000000 .12870846-03 .19027721-03	.64000165865+07 -44701504863+07 .26687391346+03 -26952909752+01 -47415916687+03 -89061384687+00 -5877093583129+06 -47003583129+06
	# I	CC A H H H H T 1 L H H H L L L L L L L L L L L L L L L	0000000	00 00 00 58-03 39-03 02-03	# # # # # # # # # # # # # # # # # # #
		101	00000000	.00000000 .00000000 .00000000 .28186058-03 .36948139-03	
	.0000000000000000000000000000000000000	.14005598208 .12000053346 .40000000000 .00000000000000000000000		.00000000 .00000000 .38299278-03 .10487259-03 .81867943-05	.14831908995+04 29205590074+07 24828758503103 .35497737020+01 .13280731000+05 .59239576349+03 .15483460379+03 .171130505239603
	7	MAC C C C C C C C C C C C C C C C C C C			7

-6367840000+07 -77140676824-08 -37346.60691+00 -10849714941+02 -78265924285+00 -57686006765-03 -57686006765-03 -57368040740 -57368040740	.20911721+11 31969847+11 .24079140+11 .16753651+08 10705635+08 78375813+07	*16753651+08 -*10705635+08 -*78375813+07 -*68745697+05 -*10513485+06 -*10513495+06	16344440868-03	19690266-04 10989471-01 16227001-02 49041950-04 -27550419-04	.63517877+01 .83306558+00 .73944991+03 .24108576+04
BE FD CHIY CHIY UODZ HIC HIC BCRV B B LNGOB	.69343240+11 .60292339+11 .48076840+08 21616819+08 3571498+10	.48076840+08 -21616819+08 -35560395+08 -20208122+06 -29164670+06 -21966546+06	84 m	15235716+03 70016481+05 35938107+04 .70553914+04 18685213+02	.40682175408 53392585+07 .47298376+10 .15472397+11
.63781660000+07 5750000139-05 87791612754+00 .15295287185+03 .9994138633602 40644744390+00 2733065615-03 .5000000000000000000000000000000000000	MATRIX 46207+11 52989+11 8602+08 22709+07	0PXF/PU0 MATRIX82856/75+0782856/75+0752820635+057965/388+0562863708+0562863708+0595578510+0595578510+05	B3 # .10071699659-02 DESIRED VALUES .60000000+021	7 + 0 3 4 + 0 4 5 + 0 4 9 + 0 5 1 + 0 4 1 S E © U A T I	.12687472+09 16651745+08 .14742514+11 .48257871+11
7 AE 2 FH K H 0 OMY H K CHIPH H 0 UOY H 1 EXA H 1 CXA H 1 CXA H 2 LONGH	K 1 11		в3 ОESI 3		
.4565620640+07 .16234500072-02 .47881444528+00 .000000000000 -11089287507+06 47142866366+00 .22149505267-03 .10795661156+01 .5000000000000000 .3993232523+05	.47312047+6865979314+08 .46132112+08 .41127304+0520481426+0525317999+05	.41127304+05 20481426+05 25317999+05 14489422+03 23556642+03 22249508+03	.62869814851-02 .62869814851-02 .10000000+03	12600767+03 6678597+05 35858697+04 -57816904+04	.38770408+08 50874885+07 .45078799+10 .14742514+11
H H H H H H H H H H L C C C C C C C C C	.14963621+09 .12628054+09 .12628054+09 .12117347+06 54169823+05	.12117347+0654169823+0583485614+0542952264+0369044743+03	04 ERR = 20000000000000000000000000000000000	.11988704+00 .7552474+02 .21073350+01 62146175+01	43785435+U5 -57467378+O4 5U874885+O7 16651745+U8
39531121887-01 72921150604-04 000000000000 4000000000000 66767390648+07 246205050585+09 45922234842-01 000000000000000 13363906369+06			76149-	1	
	.46394484+08 .35956287+08 .33960968+08 .36185088+05 .17160123+05	.36185088+05 17160123+05 23072044+05 12154144+03 12569+03 17050494+03	= .518328 = .577893 .64000000+07 = 1.000	90432311+00 57547851+03 18459408+02 .45726506+02	.33636U8+06 43785435+05 .38770408+08 .12687472+09
7	1 11 1 11 1 11	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	# 150 A	1 1 1 1 D W 2 W	n → n → →

•12340518-03		69796463-04		•63023659+00		-+69796463-04		
.77493223+03		43911199+03		39634788-05	ę, ,	43911199+03	ERS	
.24108576+04	RIGHT HAND SIDE	13653686+04	ANSWER	*83291191-06	CHECK	13653686+04	ITERATION PARAMETERS	.19546364+03
•73944991+03		41891820+03		.55028273-05		-+41891820+03		.19494523+03
83306558+00		.47163939+00		90478324-02		.47163939•00		.38180739+02
.63517877+01		**35962763+01		16830975-02	ne.	-,35962763+01		.38084305+02

.63567840000407 .787140676824-08 .34734777155-02 .10841612684+02 .78564370314+00 .58084354647-03 .508103100000000 .731520000000000 .22667888109+06	. 20627081+11 . 31735652+11 . 23928992+11 810327928+08 10228+08 78528634+07 0 -1825287+10 78528634+07 	10239672857-02	
9 E 0 M Z C H I Y W B U U D Z C C C C C C C C C C C C C C C C C C	-, 68416422+11 -, 90327170+11 -, 59858600+11 -, 46744123+08 -, 35221491+08 -, 532122491+08 -, 53212285+10 -, 6744123+08 -, 53212285+10 -, 19836209+06 -, 19836209+06 -, 19836209+06 -, 19836209+06 -, 19836209+06 -, 19836209+06 -, 19836209+06	-03 84 = . -•100000000+0	
00000+07 0139-05 2754+00 2285+03 7145+02 9587+00 6806-03 00000	40 40 40 40 40 40 40 40 40 40 40 40 40 4	0036-03	
5750UU00139-05 5750UU00139-05 87791612754+00 15268882285+03 99975607145+02 40647409587+00 27416356806-03 00000000000000 55420930329+00 55420930329+00	PXF/PUD MATRIX -22178869+11 -125910518+11 -15128311+11 -1531950+08 -79701241+07 -87939861+07 -15400 MATRIX -1531950+08 -79701241+07 -87939861+07 -87939861+07 -81283373+05 -6184394+05	BOUNDARY CONDITIONS B3 = .41764050036-03 DESIRED VALUES .60000000+021 ITERATION PARAMETERS .19507483+03	
P P P P P P P P P P P P P P P P P P P	D D D D D D D D D D D D D D D D D D D	BOUNDA B3 == DESIRE . • • • • • • • • • • • • • • • • • • •	
.45719629273+07 •16234500072-02 •47881444528+00 •0000000000000 11061577484+06 46641481656+00 -2159922539-03 •1075739502539-03 •1075739502539-03 •239906251978+05 •23200135951+02	.46700016+08 -65472097+08 -45817635+08 -40172895+05 -25211479+05 -37434015+07 -19567321+05 -19567321+05 -19567321+05 -19567321+05 -252146300+03 -22746300+03	.12988876868-01 .13036275541-01 .10000000+u3 .4999999874-06	
6 4 4 4 4 4 7 6 7 6 7 7 7 7 7 7 7 7 7 7	-14776285+09 -12534837+09 -12534837+09 -11827871+06 -11128848+08 -111288449+05 -111288449+03 -111288447434+03 -11827871+06 -11827871+06 -11827871+06 -11827871+06 -11827871+06 -11827871+06 -11827871+06 -11827871+06 -11827871+06 -11827871+06	0-04 82 = 9-63 ERR = 170L = 170L = 138108414+02	
39310659902-01 72921150604-04 000000000000 4000000000000+03 66822387078+07 24488935948•04 20129469709+01 45842104633-01 00000000000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	9000-04 0309-63 .200	
.39310659902-01 .72921150604-04 .000000000000 .4000000000000000 .24488935948-04 .20129469709+01 .45842104633-01 .00000000000	.45852710408 .35822108408 .35862633408 .35366948405 .22935988405 .32613888405 .32613888405 .35366948405 .35366948405 .12046551403 .12046551403	19801549000-041011583u309-63 .64000000+07 .20 .38084305+02 .381	
2 C C C A P D L L M M M M M M M M M M M M M M M M M	1	85 P 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	

.39860319000+15 .286480000000+02 .1403091856406 56813936515+04 78340584030000 7077702982+01 20675162509+02 .1799863636+01 .83567840000000 .23982603138+02 .77140676824-08 .23982603138+02 .77140576824-08 .23982603138+02 .77140576829-08 .23982603138+03 .73152000000000000000000000000000000000000	\$0000000 \$00000000	TEPS TAKEN *39860319000+15 *286080000000000000000000000000000000000	.32533790153703 .45575746482+00 3647362943+06 .32275398839+06
68 A A A L A A L A A L A A L A A L A A L A A L A A L A A L A A A L A		.00000000 .00000000 .00000000 .00000000	V K Z U Z U Z L E E E E E E E E E E E E E E E E E E
- 12244760000+07 - 12244760000+07 - 17680117247+01 - 17680117247+01 - 17140022624+01 - 40645924435+00 - 57322145465+02 - 62374264995+01 - 45521657561+00 - 63781660000139-05 - 63781660000139-05 - 63781660001139-05 - 63781660001139-05 - 63781660001139-05 - 63781660001139-05 - 637816600001139-05 - 63781660001139-05 - 637816600000000000000000000000000000000000		0000000000000000000000000000000000	.1925/202479+U3 .49043600652-02 .11191220526+07 .14135191871+06
. 79182741874 . 12244760000 . 17680017247 . 17140022624 . 4064595 . 27322145465 . 62374264995 . 45521657561 . 6378165761 . 6378165761 . 6378165761 . 637816495 . 63816600000 . 638184135 . 7353888413 . 15884027431	PXF/PUG MATRIX • 00000000 • 00000000 • 00000000 • 00000000	FINAL VALUES 1 ***********************************	. 1725/4 . 490436 . 111912 . 128672
	4/7X 00.000 00.000 00.000 00.000 00.000	FI V V V V V V V V V V V V V V V V V V V	
• 65000132772407 • 62981421033407 • 71182927722401 • 71182927722401 • 77182927722401 • 77182927722401 • 779783056909404 • 16719434118401 • 16719434118401 • 16719434118401 • 16719434118401 • 16719434118401 • 16719434118401 • 16719434118401 • 17010000000000000000000000000000000000	00000000000000000000000000000000000000	84247107-04 128768950-03 128768950-03 15332431-07 4470011317+07 2680839644+01	47368289338483 89009049007400 58750659475+06 46962919861+06
######################################		28 64489 03 28 64489 03 35 69 46489 03 35 69 7146 03 70 87 92 85 5 07 3404 6 = 3404 6 = 3404 7 7 = 3404 6 = 3404 6 = 3404 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	>)
. 10416416003407 - 10416416003407 - 151656950000404 - 15169262191401 - 15280731000404 - 38108413920402 - 1950748390403 - 185821803840403 - 185821803840403 - 140080000000000000000000000000000000000	00000000000000000000000000000000000000	333401 93401 9164281	.13280731000700 .59210113216+03 .15484304390+02 .17016961301+02
		.38384894-03 .1649305-03 .17464305-05 .35727043-07 .35727043-07 .17464305-05 .357205 .17690	. 5921 d . 15484 . 17016
7	00000000000000000000000000000000000000	1 X X X X X X X X X X X X X X X X X X X	VR VR ALFA BETANN AREANN

.63567840000+07 .78750000512-05 .77140676824-08 .28100055786+00 .10847306765+02 .577709373-00 .577709373-03 .577709373-03 .57312200000-00 .22728304753+06 .00000000000	.20860469+11 31914125+11 .24044600+11 .1672838+08 10598927+08 78681628407	.16672838+08 10598927+08 78681628+07 68561068+05 .12443568+06 10400625+06	18719270421-03		19652420-04 10988424-01 16199246-02 48817944-04 27574175-04	.63225700+01 83692846+00 .73646537+03 .23997/10404
8E FD OMZ CHIYH II COCELH II CODZ II K HTC RCKV III	908996947+11 9089969411 .60197307+11 .47825837+08 21364239+08 35540866+08	.47825637+U8 21364239+U8 35540565+U8 20071639+U6 .28873179+U6 21697623+U6	9-03 84 #	**100000000+01	-,15159450+03 -,69702136+05 -,35819286+04 ,70426534+04 -,16144173+02	.40316374+08 53403571+07 .46899992+10 .15333491+11 .49208401+10
AE = .63781660004076000000000000000000000000000000	PXF/PUG MATKIX .2239418U+1126075913+11 .15226830+11 .15613088+0882126035+0788484522+07	.15613068+0882126035+0782126035+078848452+0752608145+05528081450562335064+05	BOUNDARY CONDITIONS 83 s .78109716659-03 PESIKED VALUES	.60000000+02 PBWU MATRIX	39446973+U3151594521767984-D6697D213539U1215+U43581928 .2UD68858+D5 .7U426532U4547D9+D41614417	.12572354+09 16653805+08 .14617164+11 .47820684+11
.45626494711+07 .16234500072-02 .47881444528+00 .40000000000000000000000000000000000	.47198657+0865858769+08 .46061504+08 .40941131+0520268645+0525341401+05	.40941131+05 -20268645+05 -25341401+05 -14423779+03 -23456075+03 -22021056+03	.54774070704-02 .55362120591-02		-,125442U2+U3 -,66518528+U5 -,35852D58+U4 -577U1326+D4	.3&440344+U8 509U9865+N7 .44/2U821+1U .14617164+11
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	14927961+09 19321773+09 12607408+09 12060794+06 -53579116+05 -83479158+05	.12060794+1653579016+0563479158+0542700840+0364011719+0358411987+03	4823-85 B2 = 8399-84 EKR =	.2008888461 10L =	.12036u78+U0 .75874677+U2 .213U9231+U1 62565786+U1 .13414936+U0	
RHO = .39533766141-01 OM = .72921150604-04 ISP = .00000000000 ISP = .400000000000 ORNG= .66768907844+0/ PRES= .24621623175+04 MACH= .200548947270+01 CD = .45930881/24-01 CK1 = .00000000000 J = .13360250930+06 D2 = .11139604372+03	.46290202+08 .35648032+08 .33900475+08 .36024658+05 .16988773+05 .323078477+05	.36024658+05 169887/3+05 23078477+05 12093446+03 .18452898+03 16882714+03	81 = .51467244023-U5 85 = .4475306α399-04	.64000000+07 AK = 1.000	-,89986713+00 -,57284666403 -,19492277+02 ,45618936+01	.3060499+06 .43790310405 .36440344+08 .12572354+09

		.19505986+03	.19507484+03	.36109179+02	.38108414+02
	ERS	ITERATION PARAMETERS			
61445722-04	-,38590472+03	-,12003921+04	36828481+03	.41644053+00	-,31609653+01
		CHECK			
.88492948-01	-,71927719-08	+20223005-06	32221203-06	.27534287-03	13346040-D4
		ANSWER			
61445722-04	34590472+03	12003921+04	36828481+03	*41844053+00	31609653+01
		RIGHT HAND SIDE			
012338415-03	•//141269+03	•23997710+04	./364653/+03	00+9497696	10+00/522604

TRIAL NUMBER 27

THITIAL VALUES

.39860319000+15 .286080000000+02 .900000000000 .1403091856416 56813936515+04 78330276466+00 97032034917+01	.17999863636+01 .43567840000+07 .737146676824-08 .23986074175+02 .30476263059-03 .78330276466+00 .5778/813012-03 .61031971743-08 .7315200000000	00000000000000000000000000000000000000	119 INTEGRATION STEPS TAKEN 9332469+03 GM = .398603190U0+15 8946481+U7 PHI = .2860800000000+02 2365166+00 ALT = .25181807172+05 7176527+03 VR = .3540502847+03 7933829-02 UZ = .46690907597+03 7933829-07 UF = .364930380U+06 8925817+U6 DFZ = .32360515170+06 4555112+00 ETA = .97507692102+00
9 В В В В В В В В В В В В В В В В В В В	614 675 675 675 671 671 671 671 671 671 671 671 671 671		A 1 1 CN S A 1 CN S A 1 CN S A A L I B B B B B B B B B B B B B B B B B B
1874+04 0000+07 2000+04 6844+01 2624+04 9461+00 4486+02	0968+00 0000+07 2754+00 9617+03 94617+03 1417-03 1417-03 00000+00		9 INTEGR 2469+03 2469+03 2481+07 2379+02 5157+03 3429-02 7077+07 5112+00
.79182741874+04 .1224760000+07 .128346132000+07 17880016844+01 1714902264+44+01 1714902264+006 .27324664486+02	.4522370968+00 .437816600001-07 -579000010139-09 .23901909617+03 .91500003418+02 .40514594617+03 .00000000000000000000000000000000000	- · · · · · ·	8 7 7 7 7 6 7 8 11
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0000 0000 0000 0000 0000 0000 0000 0000 0000	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	V = .361 Z = .352 DZ = .176 DZ = .176 VRY = .141 VRY = .141 UY = .140 UFY = .140 CD = .129
65981421010407 62981421010407 1756/557010404 1182927929401 47030160945401 47030160945401 1658643488401	.46903718503400 .46923721324402 .1623450007202 .47831444528400 .60000000000000000000000000000000000	.00000000 .00000000 .000000000 .00000000	.6400000744407 .44708789901407 .26465067905403 26779945929401 47205489516403 68709355729406 46944387024406
2	#		
.uuuunuuunu .iu414414uuunu .iu414414uuuunu .iu414414uuuunu .iu4645262944u .iu3280731uuu+u .iu3280731uuu+u .iu459386217404 .iu459386217404	65821803840+03 31358995814-08 72921150604-09 40000000000000 4000000000000000000	. 00000000 . 00000000 . 00000000 . 00000000	.14029448474+04 29197947462+U7 24620383031+U3 .35494248640+U1 .13280731010+U6 .59154046816403 .15494627081+U2 .17015872338+U2 .17015872338+U3
. 1000000000000000000000000000000000000	.65821803840 .31358995614 .73721158995614 .000000000000000000000000000000000000	.00000000 .00000000 .00000000 .00000000	. 146294 . 291979 . 3546203 . 354942 . 132807 . 540540 . 170954
F X D D X Y X D D X Y X D D X X D D X X D X X Y Y X D X X Y Y X Y Y Y Y	7	000 000 000 000 000 000 000 000 000 00	D D D D D D D D D D D D D D D D D D D

.63567840000+07 .78750000512~05 .20315942044+00 .20315942044+02 .0849602784+02 .078330276466+00 .5787813012~03 .573787813012~03 .573787813012~03 .5737878130000000000		.16642568+08 10565970+08 78935446+07 68421643+05 12494915 20549017+06	1036994727-05
BE 900 000 000 000 000 000 000 000 000 00	69171923411 90882547411 90210766411 47729511408 31559464608	.47729511+0835282658+0835594646+0819969048+0528384655+0628384675+06	-05 84 m
00000+07 0139-05 2754+00 8383+03 2545+03 9461+00 1417-03 0000 2962+00 0295+03		5 5 5 S 5	8009
.63781660000+07 .557500000139-05 .87791612754+00 .15281198383+03 .1000012545+03 .406514994617-03 .500000000000000000000000000000000000	PXF/PUD MATRIX	0PXF/PUD MATRIX	B3 =20861388009-05 DESIRED VALUES .60000000+021
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	X T 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TX	B3 DES1 CASE
• 45473844807+07 • 16234500072-02 • 4788144528+00 • 0000000000000 • 11126135424+06 • 47030469945+00 • 22044155789+03 • 10831163360+01 • 500000000000000+00 • 23256393721+02	.47205419+08 .65848836+08 .46071486+08 .4083503405 .20206591+05 .25404841+05	.40883503+05 .20206591+05 .25404841+05 .14348934+03 .23562124+03 .22568650+03 .38878332+03	•13961189771-04 •14154286274-04 •10000000+03
41.00.00 X S S X S X S X S X S X S X S X S X S	. 1929584+09 . 19318375+09 . 12610096+09 . 12043337+06 . 83651644+05	.12043037+06 53403348+05 83651644+05 42436486+03 4298212+03 58527055+03 10945173+04	-07 ERR **
39620684537-01 72921150604-04 00000000000000 4000000000000+03 66757007875+07 24673315027+04 2296428705-01 45996428705-01 0000000000000000000000000000000000	12061	10940 10940 10940 10941 10941	.4874 - 07
.39620684537=01 .72921150604=04 .000000000000000000000000000000000	.46297186+08 .55839099+08 .33907944+08 .35983642+05 16941860+05 231312866+05	.35983642405 =.16941860405 =.23131286405 =.12018578403 =.16544015403 =.16924151403	23244205746-07 233418654874-07
7 0 4 1 0 0 4 1 0 0 4 1 0 0 0 0 0 0 0 0 0		8 8 8 8 8 8 8 8 9 8 9 8 9 8 9 8 9 8 9 8	a a

THIS IS A FULL PRINT OF CONVERGED CASE

TNITIAL VALUES

. 39860319000+15 . 286680000000000000000000000000000000000	0000000. • 00000000. • 00000000. • 10000000.	1 1 1	110N STEPS TAKEN .3986U319CLC+15 .28508CDCCC0+02 .9CCCCCCCCC+12 .12008877293+06 57789462198+04 77756327749+00 43870884560+C2 9536895463+02 .180CDC013154+01
6M ALT = VRZ = UZ = CFZ = DFZ = ETA = ETA = ETA = ETA = UC = UC = UC = UC = UC = UC = UC = UC	.00000000 .00000000 .00000000 .00000000	.0000000000000000000000000000000000000	I INTEGRATION GM = .398 PHI = .285 ALT = .120 VRZ =577 UZ =438 LFZ =438 DFZ =953 ETA = .180
.79182741874+04 .1224476C000+67 58346132000+67 17686L16844+01 .466146844+01 .4661468640377+62 62376613771+61 .4552371732+00 .562376613771+61 .4552371732+00 .5750001016+67 .575000101754+62 .6378166006477 .63781660006600 .57500199955+03 .9150CC03418+62 .7374111417-C3 .500000000001+03	000000000000000000000000000000000000000		01ATE VALJES .79418704793+64 .63356744889+6659694703170+6492295398058+0080795576581+03 .40623541743+06 .15196362854+03 .15196362854+03 .15196362854+03
111 111	PXF/PUD MATRIX -000000000 -0000000000000000000000000	0PXF/PUD MATRIX .10CCCCCC+C1 .0CCCCCC .0CCCCCC 63733287-C7 354894-C7 1976939-C4	AE III
V V V V V V V V V V V V V V V V V V V	7 X Y O O O O O O O O O O O O O O O O O O	X	1 N TER 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
-62981421006+C7 -1756757000+C4 -1756757000+C4 -19783055909+C1 -19783055909+C4 -19783055909+C4 -18117236956+C2 -18117236956+C2 -18117236956+C2 -18117236956+C2 -18117236956+C2 -18117236956+C2 -18117236956+C2 -18117236956+C2 -18117236956-C2 -18117236956-C2 -18117236956-C3 -18117236956-C3 -18117236956-C3 -18117236956-C3 -18117236956-C3 -18117236956-C3 -1811723	. 10000000 . 00000000 . 00000000 . 00000000	.CCCGGCG .0GGGGG .CCGGCGG .1296810-C5 79115G4-C6 12925G11-G5	.\$48C\$373375+C7 642771229C1+G7 93C4642678+G1 93924642678+G1 51314513323+C4 48C29055245+GC .25489C98794+C2 34683457994+C2 39657781C39+CG
78	1000+01 1000+01 1000 1000 1000 1000	.CCCCCCC .0030000 .0CCCCCCC .6809954-06 .2680954-06 .78239069-05	0 C C C C C C C C C C C C C C C C C C C
.00000000000 .104164166CC+67 .5056950000+64 .13280731000+64 .38109173204+65 .38109173204-66 .38109173204-07 .31358995814-68 .37358995814-68 .37358995814-68 .658218000000000 .600000000000000 .60000000000	.10300000. .10300000. .0000000. .0000000. .0000000.	. CCCCCCC . 0030000C . 0CCLCCC 663954-06 . 2639572-05 . 78239059-05	.1CCCCCCCC+C3 .52959530430+05 5172C114713+C4 78389571556+01 .1328C7310CC+C6 .77705785517+04 .31453954794+C2 .19729303410+03 .658218G3840+L3
	10000000 0000000 0000000 000000 000000 0000	.CCCCCCC .0CGCCCCC .CCCCCCC 1330720-05 68683129-06 44129601-06	.10000 .529595 .529595 .7817201 .132867 .777053 .314539 .197293 .658218
T X O Z A X V K D O X Y X V K D O X Y X V X V X V X V X V X V X V X V X V	3000 0000 0000 0000 0000 0000		######################################

.7875000512-05 -77140676824-08 -2368567814+02 -15448448511-62 -78330279570+00 -5787813012-03 -61031971743-08 -73152006606460 -41473762421-04	.12366917-01 10321892+00 .99772791+02 .28808180-03 28002243-02 .99308640+00	.288U8180-03 28GC2243-02 .993G8646+00 .26547781-05 44143322-04 14187440-03 18G646G1-03	.3986031900015 .286080000000000000000000000000000000000	.40512519-01 59019196 +00 .19811638+03
FD = 0 OMZ = 0 OMZ = 0 CMIY = 0 CEL = UGS = 1 HTC = HTC = 0 CEL = 0 CE	-,82G261G7-G1 ,10046616+03 -,99156128-G1 -,21G8808-G2 ,10143CC1+G1 -,26275554-G2 ,37389928-G1	21088C88-02 .10143001+01 26275654-02 2624663-04 .3645683-03 377887C2-04 .12336C5-02	GM = AZ = A	17172313+00 .20422568+03 43455328+00
57500000139-05 87791612754+00 23829033117+03 -91320619548+62 -40651458587+00 27374111417-03 50000000000 40821604223+00			3624354856 +C 31852931193+ 5301651469-0 5301651469-0 1846673032 +C 1846673032 +C 1846673032 +C 1846673032 +C 1846673032 +C 1846673032 +C 1846673033 +C 184769168 +C 184869 +C	
PH CHIP CHIP UCDY EXA CKX DHTI	PXF/PUG MATRIX -99768178+C2 -88660045-C1 -128C4466-C1 -99296738+00 -24025666-C2 -3058510-D3 -7228C414-C2	DPXF/PUD MATRIX .99296738+CL24C25666-D2 .3D58551C-U314365518-633759243-C4 .32617476-D51569432C-C3	V V S S S S S S S S S S S S S S S S S S	PXF/PUG .1980 5048
.16234500072-C2 .4781444528+C2 .6060000000 .47832888C5C+C2 -47030056530+00 .75999950611+00 .5060600000C+C	.45776375-03 -33831182-02 .99336213+00 .74302415-05 -6186769-04 -13578377-03	.74302415-C561867649-C413578877-C3 -25810115-0744462481-C614695708-05	.64635639144+C7 54634699942+O7 .11729859131+C3 .95366298225+O1 52102226512+C4 49173593394+O 954164941453+C3 .53182917877+C1 .69770474569+G4 .16234506072-C2 .47881444529+O3 .16234506072-C2 .47610789427+G3 476366530+C6 .72044158789-O3 .72044158789-O3 .72044158789-O3 .72044158789-O3	.11927652-02 11235894-[1 .97258536+00
FU MOM X X X X X X X X X X X X X X X X X X X	27638476-02 .10137523+01 32926706-02 48667070-04 .28142946-03 59147918-04	48667L7C-04 .28142946-03 59147918-04 26345335-06 .3G3781CL-C5 175203G3-06	7 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	69980303-02 .1C5933CC+61 98934989-02
.7292115G6G4-U4 .CCCCCCCC0 .4COCCCCCO .769513425G+C6 .2294364549-C2 .12GGGGGG47-C1 .12GGGGGG47-C1 .CCCCCCCCCCCC .12GGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGG	27638 .10137 32926 48667 59142	4866 2814 2614 3637 3752	2CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	- 5998 - 1659 - 9893
.72921156604-0 .CCCCCCC0 .400C00C000+C .77695134250+C .22943645649-C .19545121802+C .1200000047-0 .CCCCCCCCC .12732169726+0	.99315564+0C 29074001-02 .4673C461-03 13842429-03 5312C44C-C4 .77005215-05	13842429-63 53125446-04 .77665215-05 14256595-05 38617497-06 .31871075-07	-2000000000000000000000000000000000000	97209172+00 963616CD-C2 12936498-D2
1	.9931 29073 1384 5312 700	1384242 53125444 .7700521 1425659 3801749 .3187107	CCCAPTOR ASSESSED CONTRACTOR OF A PARTICLE O	.972D 9636 .1293

MUNICOL TAKEN	HINET SCOTO MONTH COUNTY	THIS MEDIATE WALLES	
.81474265-02	.12032044+00	.70714559-02	.23865029-04
- 29921007-03		.19576488-63	88646293-C6

.14308189-03 64828109-02 .97121566+00 42169382-01	.14308189-03 64828109-02 .97121566+00 24148934-05 13961531-04 29512062-03	110N STEPS TAKEN -3986031900015 -286080000000000000000000000000000000000	. (1406/824-08 .2390978746+02 .302503679570+00 .5787813012-03 .61031971743-08 .73152000000000	.47802551+00 69342068+00 .29359861+03 .21557972-01 .93816581+00	.21557972-01 .19746275-01 .97815581+00 .92289553-03 .10459364-02 29921007-03
.69256351-02 .10741449+01 12794952-02 .64290674+00	.69256351-02 .10741449+01 12794952-02 .44955106-03 .11929963-02 .15362673-03	S 4 INTEGRA 17+C4 6M = 07+06 PH = 62+04 AZ = 41+00 ALT = 90+07 ETZ = 10+07 ETZ = 139-05 FD = 33-05 FD =	UNY = CHIY= DCFL= UOD = HTC = RCRV= RCRV= LNGO=	.10895050+02 .32754562+03 .23663471+01 .38407628+00 .1585779+01 .93653724-61	.38407628+00 .15857779+01 .93653724-01 .11613468-01 .13687037-01 .23650865-02
.97077547+00 55135187-62 .39422681-03 36579877-61	0PXF/PUG MATRIX •9707754760 •55135187-02 •39422681-03 -30016730-03 -10865639-04 -42194662-06 31970942-03	6		PXF/PUD MATRIX .2937D952+03 -51135135+00 .21357D66+00 .94863185+00 .17605002-01 .58238929-C2 .14468998+00	0PXF/PUD MATRIX .94863185+00 .1760502-01 .5823829-02 .23472913-03 .9170525-03 .1057648-63
.60692855-05 89650996-04 27923566-03 24406320-03	.60692855-05 89650990-04 27923566-03 38349941-07 10183676-06 14405468-05	.64491226368+67 6403855344+07 .10778997750+04 .97243577742+01 52059086721+C4 50497023840+06 11755741591576+06 .23711501676+06 .15224739990+06	.478314452840U .0000000000000 .285718333040 .22044155789-03 .500000000000000000000000000000000000	.27437922-62 18717639-01 .93785117+00 .57888266-64 16096473-04 46673533-63	.57888266-04 16096473-04 40675533-03 .22592025-05 .238646293-06
.19851725-05 .67632581-63 54506091-04 .43809667-02	.19851725-05 .67632581-03 54506091-04 .23526412-05 .62178511-05 .82121333-06		40000000000000000000000000000000000000	.3728528-01 .11958139+01 -25615157-02 .15051944-02 .27466129-02 .33421861-03	.15051944-02 .27466129-02 .33421851-03 .42469161-04 .50235130-04 .87987869-05
28351984-03 76631949-04 .80417896-05 20865924-03	-,28351984-03 -,76531949-04 -,80417896-05 -,14582148-05 -,81440390-07 -,12515123-07	אה קרה היא מאא היא היא היא היא	S	.93754996+00 15958834-01 .23053550-02 37683454-03 11399170-04 .18723242-04	37683454-03 11399175-04 .18723242-04 .65868994-06 .24998446-05 .40264411-06

.398603190C0+15 .286080000000+02 .9000000000000+02 .68981355708+05 55607317358+00 76696589020+05 71706189919+05 .1799998088+01 .63567840000+07 .63567840000+07 .23861305583403 .23861305583403 .5787813012-03 .61031971743-08	.20775749+02 .18560592+02 .38607017+03 .6688552+00 .58883380+00 .89927178+00	.66685652*00 .58883380+00 .89927178*00 .20364122-01 .15755327-01 -15032898-02 .13425695+00	60319 60319 60319 60206 60206 711185 71185 7185 7
# 6M = PHI =	.20991792+03 .64698995+03 .27908216+02 .55629027+01 .63744626+01 .3683913+00	.55629027+01 .63744626+01 .36683913+00 .14559072+00 .11627716+00 36908492-02 .10086524+01	6M = PHI = AZ = ALT = LFZ = DFZ = DFZ = CFT = DFZ = CHIV = DCEL =
V = .7959C794785+64 Z =11588229119+67 DZ =58441625870+64 DDZ = .16909364970+61 VRY = .20486291586+64 LFY = .20486291586+66 DFY = .26417280227+65 CD = .25417280227+65 CD = .51573348565-61 AE = .6578166000+67 AE = .6578166000+67 CH = .5750000139-05 CH = .27574111417-03 CH = .27374111417-03 CK3 = .500000000000 CK3 = .500000000000000 CK3 = .500000000000000000000000000000000000	PXF/PUD MATRIX .40014668+03 .16313075+02 .27832333+01 .14031733+01 .51550274+00 .49349926-01	DPXF/PUD MATRIX .14031733+01 .51550274+00 .49349926-01 .1568999-01 .1376816-01 .74556337-04 .11438054+00	973119 973119 900902 327546 327546 327546 1161233 1161233 1161275 1161275 1145858
-64342325319+67 V -62463437690+07 Z -26890902726+04 DZ -10772812768+02 DD -5204339509090 -5204339509090 -55211406886+05 DF -14756690510+00 CD -184756690510+00 CD -18475690510+00 CD -1475690510+00 CD -1475690510+00 CD -1475690510+00 CD -1475690510+00 CD -1475690510+00 CD -1470300569090 CD -1470300569090 CD -1470300569090 CD -1470300569000 CD -1470300569000 CD -1470300569000 CD -14931211348+04 PAI -2500000000000000 CC -25044155789-03 UD -250600000000000000000000000000000000000	48606248-C1 • 21228300-01 • 89479616+C0 • 14314053-02 • 12939221-C2 • 45524152-G3	.14314053-02 .12939221-02 .45524152-03 .41302816-04 .34114172-04 .217976992-05	64016959422+67 V59800660527+07 Z31368802948+64 DZ42133836455+01 DD49948521176+C4 NP)98922593888+06 LF)1138532592+07 DF1076556847-01 C1076556847-01 C10765588+06 LF)1767475287+09 AE1623450072-02 FH28374400474+05 PAI470300565007-00
7	.72221451+CG .2010355401 .87656166-C1 .18241617-01 .18357493-C1 .13326602-C2	.18241617-01 .18357493-01 .13026602-62 .45416451-03 .36465716-03 .10353267-04	C C C C C C C C C C C C C C C C C C C
-, 4CDDUDGDCD+63 -, 10196407475+07 -, 4982819904+64 -, 32974219246+01 -, 13280731000+66 -, 77905424197+64 -, 1196640472+62 -, 21874680075+03 -, 65821803840+03 -, 65821803840+03 -, 6921156604-04 -, 00000000000000 -, 40000000000000+03 -, 556292402+07 -, 643618384982+04 -, 000000000000000+03 -, 5662924020+02 -, 11370334982+04 -, 11370334982+04	5451+C0 5028-01 9591-02 6873-03 0139-62 5208-04	5873-03 5139-02 5208-04 7666-04 5429-06 5429-06	-5000000000000000000000000000000000000
X X X X X X X X X X X X X X X X X X X	. 92290 . 1924 . 75139 . 1133	.71998 .11336 .76235 .35637 .29756 95348	T X X X X X X X X X X X X X X X X X X X

- 55 - 10 - 12 - 15 - 15	7	24 80 15 13 14		CDD III
. 95017668+01 . 55144256+01 . 10003061+02 . 12044250+00 . 92027625-01 . 15794893+00 . 78096836+01	.600000 178139 214837 72938 .132807 .410536 .558299 .593792 .658218 .284614 .72921 .000000 .449583 .18671 .137871 .137871 .137871 .137871 .137871	.2442996-01 .80885580-02 .50121462-02 .16953756-03 .1357900-02 .14831563-02	.18661891+01 .37655682+00 .74688827-01 .24429996-01 .8088586-02 .50121462-02	. 24229393846+02 .11999999740-01 .00000000000 .11044663666+05 .43751550667+03
1001 114 1362 1785 3783	GGGCGC+C3 3912374+C7 3773344+C4 395576C+01 C73100C+C6 3651138+C4 9971827+C6 9298522+C1 11667844-C4 C10CGCGCC C16CGCCCCC 545681748+C7 7105422+C1 C16CGC53-C1 C2CGCCCC 5724616+C3	.29168 95783 .61479 23399 16065 .17496	1.80.86 50.86 50.87 50.87 50.87 999	846+02 740-01 1000 1666+05
.10012613+03 .60769534+02 .11444599+03 .13622855+01 .10400539+01 .17859843+01		.29169389+00 95783252-01 .61479372-01 2329902-02 16065912-01 .17496990-01	.1202874F+02 .60385167+01 80869777+00 .29168383+00 95783254-01 .61479372-01	UODX: CLA : CK2 : HT1 : LAT :
.10006961+C2 63898607+C1 .12409973+G2 .1395579C+C0 10670671+C0 .18300935+C0	.639618DLC26+C757422099146+D717619160061+C450964590498+C152881197914+C456062651797+D039642556793+C610644861090+C73748709817-D2 .157876304528+C094364400142-8+C094364400142-C594364400142-C594364400142-C594364400142-C594364400142-C594364400142-C594364400142-C5	.28173140-0193301260-0255794034-0220642378-0315656310-02 .17192832-02 .27517909-01	.11650316+C1 .37358871+0p .75217512+C6 .28173140-G1 9330126C-C2 .55794034-C2	.22044155789-E3 .76000105010+00 .5C0C0060CC0+C0 .1C637106463+05 .45161742757+C2
PXF/PU0 280 -507 -609 465 -799	V = .429 7 =218 DZ =327 DDZ = .114 VRY = .401 LFY =105 DFY = .784 ORY = .877 ORY = .877 ORY = .877 ORY = .877 ORY = .881 ORY = .273 ORY = .273 ORY = .273 ORY = .273 ORY = .881 ORY = .273 ORY = .273 ORY = .881 ORY = .8	- 12 - 42 - 42 - 55 - 68 - 75	PXF/PUO .921 .158 275 .126 426 .285	UCDYE
/PUG MATRIX .48200819+04 .28001491+C4 .50785302+04 .60927637+C2 .46557566+02 .79903243+C2 .39188941+04	652000111 65200011169911796566 6520001116991796666 652000111696666666666666666666666666666666		/PUO MATRIX * 92118888+03 * 15869183+03 * 27585582+02 * 12634602+02 * 42633284+01 * 28560708+01 * 24904661+03	27374111417-C3 .0000000000 .5000000000000000000000000
.32552 19772 .37264 .44369 33873 .58168	σ	t i i	.3856 2757 3106 1978	
.32552124+05 19772143+05 .37264636+05 .44369564+03 33873521+03 .58168835+03	GM = .399 AZ = .900 AZ = .900 VRZ =299 VRZ =299 VRZ =299 ORZ =73 DFZ =13 DFZ =13 DFZ =13 DFZ =29 ORZ =23 ORZ =31 ORZ =	.94881C61+0231063784+0219784-053+0274813134+0052420045+01 .57028239+01 .90763468+02	.38564467+04 .19888448+04 27578593+03 .94881C61+02 31063784+02 .19784953+02	UDDZ = HTC = HCRV = HCR
.51018211+04 32732441+04 .63588065+04 .71123068+02 5438850+02 .93270973+02	.39860319000115 .286080000000102 .900000000000000002 .27208221489+05 .29625907464+04 -72405395881+0029384834135+061378265559+07 .17999888497+01 .63567846000000000000 .15018130124-08 .23690794790+02 .16342475485+0278302794790+02 .57787813012-03 .61031971743-08 .73152000000000	-,14595 -,50221 -,94365 -,79385 -,85945	.55703357+03 .17999618+03 .41483217+03 .41595294+02 50221781+01 .34917191+01	.57787813012-C3 .61031971743-08 .731520C0000+00 .11452220869+05

.71123568+02 54388856+02 .93270973+02 .3048537+00 29573199+00 .36157129+00	**39860319000115 **28608000000000000000000000000000000000	.13111656+0510365184+05 .16758794+05 .83077107+0288695487+02 .10764414+03	.83077107+02 88695487+02 .10764414+03 2856258-01 35789896+00 25586430-01	.39860319000+15 .28608C00000+02 .900000000000000000000000000000000000
.44369564+0333873521+03 .58168835+03 .183383340117854617+01 .21660930+01	11 INTEGR 0+C4 GM = 6+C4 AZ = 7+C4 AZ = 7+C4 AZ = 7+C7 GM Z = 7+C0 UZ = 8+C6 LFZ = 1-C1 ETA = 6+C2 GMZ = 8+C3 CMZ = 8+C3 CMZ = 7+CC UCZ = 7+CC	.82357963405 63758898405 .10185280406 .51668551403 54941987403 .66852673403	.51608251+03 -54941987+03 .66852873+03 -17959835+00 -22160594+01 -15991157+00	JES 5 INTEGRATION 2288+D4 GM = .398 4352+G7 PHI = .286 1703+D4 AZ = .90D 2152+G1 ALT = .4441
0PXF/PUD MATRIX •60927637+02 •46557566+02 •79903243+62 •2601829+00 •25241034+66 •30833192+00 •61820947+01	1A1E 2472 2474 2472 2474 2476 2476 2476 2476	PXF/PUG MATRIX .11678599+05 .18690910+04 .13976692+05 .71118756+02 .75900028+02 .92186283+02 .92186283+02	PXF/PUD MATRIX .71118756+62 .75900028+62 .92185283+62 24741788-61 35643049+00 21735309-61	INTERMEDIATE VALUES V = .35072628288+04 Z =27362344352+67 DZ =24257051703+04 PDZ = .31181G82152+61
.13955790+CL 10670671+C0 .18306935+C0 .59661012-03 57874691-C3 .70739009-03	.64110712354+C7 .55729501674+07 .17385024216+04 .21917313538+C1 -19842591711+C4 -30485632010+C6 -31485632010+C6 -14193840938+06 .57C42588352-C1 .14174117673+08 .1623450072-C2 .000000000000000 .153855400 .000000000000000000 .1538516972+C0 .22044155789-03 .76011501777+C0 .76011501777+C0 .76011501777+C0 .76011501777+C0 .76011501777+C0 .76011501777+C0 .76011501777+C0 .76011501777+C0 .76011501777+C0	.25719?30+C2 20297324+f2 .32789292+f2 .16295f46+C0 17390044+C0 .21112597+f0	.16295646+CG 1739CG44+CC .21112597+OG 56D38567-C4 70151311-G3 5621G896-G4	.54151301334+07 53891491662+07 .19015501576+04 .23653411919+00
.13622855+01 10400538+01 .17859843+01 .56340327-02 54863926-02 .13268618+00	7 Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	.75365802+63 -19584194+03 -31277047+03 -15846975+01 -16872004+61 -26528401+61	.15845975+01 168726C4+01 .20528401+61 5499762F-63 58055241-02 490856515-61	50000+03 R = 7882+C7 Y = 9835+C4 DY = 1422+G1 DDY =
.12644256+CO 92527625-O1 .15794893+CC .51305546-O3 49802751-O3 .60836305-O3	X = .7CDCCGDCGGCCCXX DX = .197582855364C7 DX = .187582855364C7 DDX = .174859537746U WKG = .132807310CG+C6 4 .43C3788C235401 ALFA = .4537703521+64 4 .43C3788C235401 ARFA = .65218C384G+C3 RHO = .3437728CGCGCGGGGGCCC TSP = .40CGCGGGGGGCCC TSP = .40CGGGGGGGGCCC TSP = .40CGGGGGGGCCC TSP = .40CGGGGGGGCCC CKI = .11065164139+C2 CCI = .119882719C9-C1 CKI = .00CGGGGGGGGGCC CKI = .40C35893G265+C2 0 = .97248839G8+C2 0 = .97248839G8+C2	.2365943+02 -17566556-62 .27583726+02 .14655016+66 -1499556+00 .18217619+60	.14655010+00 14995566+00 48891312-04 60527755-63 42987073-C4	T = .8CLGCJGGBOB+B3 0x =215D34578R2+C7 0x =16736B5B35+C4 DDx = .12236711422+61

2099877009940467731439136+0034633016114+0621237122035+06 .18003101587+01 .63567840000+07 .77140676824+02 .2330795264+02 .82209126407+0178330279570+00 .57787813012-03 .61031971743-08 .73152000000000000000000000000000000000000	.21195540+05 -20732503+05 .27241037+05 .79062196+02 -11381100+03 .10131861+03	.79002196+02 -11381100+03 .10131861+03 -11216288-01 -72232569-01 -72793927-01	.39860319000+15 .28660800000002 .900000000000000000000000000000
VRZ = LFZ = DFZ = ETA = FP = CHIY= DCEL= UDZ = UDZ = HTC = RCRV= DCEL= LNGO=	.13256797+06 12800814+06 .16695371+06 .49059567+03 .62926143+03 .31534504+05	.49059567+03 -70579275+03 -62926143+03 -71497150-01 -45785692+00	6 M = .398 PHI = .398 ALT = .444 VRZ =177 VRZ =177 UZ =228 DFZ =228 DFZ =228 DFZ =228 UZ =774 UZ =774 UZ =778 UZ =778 UZ =778 UZ =778 UZ =778 UZ =788
VRY = .18466126149+04 UY = .3956728136+06 LFY =86747021076+06 OFY = .18265122252+06 CD = .41041440933-01 AE = .63781660000+07 FH =5750000139-05 OMY =87791612754+00 CHIP= .22751895422+03 PANG= .30029568279+02 UUY = .40651458587+00 UUDY = .20000000000 CK3 = .50000000000+00 CK3 = .50000000000+00 DH71= .10686836709+03	PXF/PUD MATRIX .18597412+05 .17742060+05 .22994505+05 .67603043+02 -97418816+02 -86783600+02 .43260083+04 .315	0PXF/PUD MATRIX .490 .67603043+02 .490 97418816+02705 .86783600+02 .629 97910765-02714 62023464-01451 62279688-01451	INTERMEDIATE VALUES V = .32073001493+04 Z =29628358961+07 DZ =20996181200+04 UV = .34916392600+04 UV = .3897245783+00 LFY = .28740794462+06 CO = .2877416306+06 CO = .60187348036+06 CO = .60187348036+06 CO = .63781660000+07 FH =5750000139+05 CHP= .22406955886+03 CHP= .2240695888+00 UOY = .40651458587+00 UOY = .40651458587+00 UOY = .40651458587+00 UOY = .27374111417-03 EXA = .0000000000 CK3 = .50000000000
18487751264+04 62023230990+00 45403650692+06 18697601236+06 .12656156504+C0 .82059341666+07 .16234500072-C2 .4781444528+00 .0000000000000000000000000000000000	.41575170+02 -,40624603+02 .53348508+02 .15495446400 -,22315867+00 .19872069+00	.15495446+00 22316867+C0 .19872069+00 22074653-C4 1421600-03 14276605-C3	.6416373340+0752006535402+0718416278122+0417429700028+046616855721+0055649785405+0655649785405+0655649789405+07162345000000000000000000000000000000000000
LVXXX OOY CCL XXX MONX CCL XXX UUUNX CCC CCC LCCCX CCCC CCCC CCCCCCCCCCCCCC	.40723410+03 39314167+03 .51267512+03 .15064368+01 21573456+01 .1932268C+01	.15064368+01 .21673456401 .1932680+01 .21946573-03 .14342035-02 .13874559-02	4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
13280731000+06 33300352085+04 9585974449+01 79210762978+01 65821803840+03 22484831005-02 72921150604-04 00000000000 46000000000 460000000000	, ,	, ,	23118505507407 15532932392404 15532932392404 13640656525401 13280731000406 30433779045404 12409882035402 57463481334401 58218060000000000000000000000000000000000
VKR = 133 ALFA = 998 BETA = 998 ARHO = 72 OM = 72 ON	.36730434+02 -35037214+02 .45330434+02 .1336014350 -19248538+00 .17149954+00	.1356143+00 19248538+06 .17149954+00 19387739-04 12284583-03 12307423-03	X X X X X X X X X X X X X X X X X X X

• 00000000000	.29085927+05 -32201232+05 .36974847+05 .78201739+02 -11666545+03 .92637261+02	.78201 11666 .92637 37485 99631	110N STEPS TAKEN - 3986D319DDD+15 - 2866B00DDD0+02 - 43882375856+05 - 1399372494+04 - 5875D915D31+00 - 58875B915B915B915B915B915B915B915B915B915B91	.72383386+D2 12533511+D3 .78554D5D+D2
441+03 LNG0=	.18156508+0619915006+06 .22741223+06 .48565370+0372367615+03 .57546200+03	.48565370+03 72367615+03 .57546200+03 23163915+00 61690673+00 69525398+00	1+04 6H = 1+04 6H = 5+01 PHI = 6+04 AZ = 6+04 AZ = 6+04 AZ = 6+04 AZ = 9+00 UZ = 10+07 ETA	.44954660+03 77770051+03 .48810909+03
LONG= .15051423441+03	PXF/PUG MATRIX .25348600+05 27559341+05 .31292159+05 .66904060+02 99867203+02 .79352512+02 .43560435+04	OPXF/PUD MATRIX .66904060+02 99867203+02 .79352512+02 32253988-01 85318996-01 96051972-01	INTERMEDIATE VALUES V = .28664769811+04 C =31546931167+07 DZ = .37948828345+01 VRY = .37948828345+01 VRY = .37972864319+04 DDZ = .37948828335-04 VRY = .37972864319+04 DFY = .30011112863+06 C = .85723681497-01 AE = .63781660001079-05 C = .85723681497-01 AE = .63781660001079-05 C = .85723681497-01 AE = .63781660000107 C = .8572368117-03 C = .8572368117-03 C = .90258611522+02 U O Y = .40651458587+00 C X = .00000000000 C X = .000000000000 C X = .0000000000000000000000000000000000	DPXF/PUD MATRIX .61904498+02 10729657+03
.32619459561+02	.57051263+02 63114535+02 .72440050+02 .15338616+00 22878018+00 .18169880+00	.1533816+00 -,22878018+00 .18169880+00 -,73444246-04 -,19531867-03 -,21999545-03	64166216053+07 50169028932+07 17969843043+04 12762335235+01 16110943862+04 58969020134+00 58663566540+00 58461143828+07 19859130361+00 56461143828+07 10859130361+00 5646114328+07 17881444528+00 21479808602+06 21479808602+06 21479808602+06 204415789-03 317764+02 37178838838400 5000000000000000000000000000000000	.14197823+00 24579128+00 .15408275+0
.68073727345+02 LAT =	.55768579+03 61160209+03 .69832429+03 .14912517+01 22222427+01 .17670576+01	. 14912517+01 22222427+61 .17670576+01 71149557-03 18945077-02 21350448-02	-10000300000+04 R = -24600060011+07 Y = -14091351815+04 DY = -14205658593+01 DDY = -13280731000+06 VRX = -27204530982+04 VX = -15280731000+06 VRX = -15280731000+06 VRX = -15104779297+02 DFX = -15104779297+03 UDX = -151047759+03 UDX = -151047759+03 UDX = -151047759+03 UDX = -151047597759+03 UDX = -15104981495+01 UDX = -15101113246591	.13803654+01 23881200+01 .14988145+01
D2 = .6807372	.50072554+02 -54435507+02 .61807201+02 .132220400 19733197+00 .15681751+00	.1322190+00 -1973197+00 .15681751+00 -63682060-04 -16854625-03 18976590-03	T = .10000300000+04 X =24600060011+07 DX = .14091351815+04 DDX = .1420565853401 WKG = .13280731000+05 VR = .2720453082+04 ALFA = .16089431353+02 AREA = .65821803840+03 RHO = .23180779297+02 AREA = .65821803840+03 DRNG = .23180745672-02 OM = .72921150604-04 F = .00000000000000000000000000000000000	.12234522+00 21201797+00 .13299196+00

-,75721332-01 -,68557511-01 -,17022188+00 ,16641011+01	.39860319000+15 .39860319000+15 .2866030000000000000000000000000000000000	.43595400+0557165453+05 .52597457+05 .68454326+0212638661+03 .62115977+02	7026+03	.39860319000+15 .2860800000000+02 .39251296696+05 58346827818+03 37738982728+00 31322975707+06
47035605 +00 42935986+00 10564601+01 .10346804+02	2+04 GM = 7+07 PHI = 0+01 ALT = 0+01 ALT = 0+06 LFZ = 0+06 LFZ = 0+06 LFZ = 0+07 BE =	.27167883+0635404911+06 .32448460+06 .42517026+0378442716+03 .338607536+03	.4251 7844 .3860 .9548 .9431 9632	0+04 GM = 5+07 PHI = 9+03 AZ = 9+01 ALT = 1+00 UZ = 0+06 LFZ = 9+06 DFZ = 9+0
-,64990535-61 -,58734525-01 -,14577801+60 -,14248985+01	INTERMEDIATE VALUES V = -24480942392404 Z = -331885945547407 DZ = -413407845760404 DDZ = -413407845760404 VRY = .149417828784401 VRY = .3619316387554001 DFY = .36193163875400 FFY = -91219095310406 CD = .103105968817400 AE = .63781660000407 FH =57500000139-05 CHIP= .217241545400 CHIP= .217244551372403 PANG= .9028695716402 UDY = .40651458587400 CK3 = .500000000000000000000000000000000000	PXF/PU0 MATRIX •37757729+05 •48930181+05 •44675272+05 •58524903+02 •10819451+03 •53213334+02 •45810363+04	DPXF/PUD MATRIX .5852490346210819451+03 .53213334+02 .12941757-01 .13023677+0013293451+0014968109+00	V = .19687568850+04 Z =34218673995+07 DZ =92112065959+03 DDZ = .4282278729+01 VRY = .122826278729+01 UY = .32824780861+00 LFY =94980357910+06
14850493-03 13465339-03 33382555-03 .32645132-02	*54153256980+07 -44457622829+07 -16097001951+04 -22514240864+01 -14784322472+04 -356117524246 -21874200687+00 -54460363323234+07 -1623450070000000 -1623450072-02 -47881444528+00 -000000000000000000000000000000000	.85511212+02 11207125+03 .10308352+03 .13427460+00 2478555+00	.13427460+C0 24786562+O0 .1018455+C0 .30122108-O4 .29828453-C3 30429445-C3	.64132517660+C7 .4697144313+07 .13477396927+04 -31350110409+01 -13195805921+C4 -86566567832+00 -74557687295+06
14443873-02 13180749-02 32441262-02 .31770416-01	11000300000+04 R = 25938762077+07 Y = 1266204794+04 DY = 13280731000+06 VRX = 13280731000+06 VRX = 13280731000+06 VRX = 13280731000+06 VRX = 13281313996+04 UX = 15193499850+02 CL = 15193499850+03 MD = 61438933049+07 VRN G= 125847137119-01 CK2 = 11301150537+06 HT1 = 1130115057+06 HT1 = 113011505	.83438666+C3 10872575+04 .99640010+63 .13055626+01 244087531+01 .11854938+01	.13055026+01 24087531+01 .11854938+01 .29307639-03 .28962399-02 29580079-02	27124632777467 Y =27124632777467 Y =11002172491464 DV =18022277581401 DDV =13280731000466 VRX =18948239136404 UX =21246289280462 LFX =191714653584D2 DFX =291714653584D2
12841876-03 11619018-03 28805952-03 .28162831-02	T = .11000300000 X =2538762077 DX =12666204794 DDX = .13580731000 WKG = .13280731000 VR = .23301139796 ALFA = .18697690953 BETA = .18697690953 RHO = .30477997090 OM = .72921150604 F = .00000000000000000000000000000000000	.74597363+02 9664335+02 .88255861+02 .1156898+00 2138UD28+0U	.11566898+0C 21380028+0O .1051675-10C .25606652-04 .25732203-03 2626849-03	T = .12C0LGUCUCO+04 X =2712463277+07 D X =11GO5172491+64 DDX = .18022277581+01 WKG = .13280731GOC+G6 VR = .18948239136+04 ALFA= .21246289280+62

.17394291576+01 .63567840000612-05 .78750000512-05 .19162458959+02 .10535859728+02 .1053585970+00 .7830279570+00 .573152000000+00	.50482503+05 69066985+05 .57944719+05 .6828459+05 11376958+03 .43710711+02	.68589459+0211376958+03 -43710711+0211177468-0121654213+0021654213+01		.57451478+05
ETA = BE	.31445458+06 42792455+06 .35772481+06 .42600129+03 70629059+03 .27177256+03	.426C0129+03 -70629059+03 -27177256+03 69627522-01 .4412831+00 13450775+01 .62706301+01	6M = ALT = ALT = ALT = ALT = ALT = BL	.35773651+06
.12109639693+00 .63781660000 +07 .57500000139-05 .87791612754+60 .20358831987+03 .90877946596+02 .40651458587+00 .20000000000000000000000000000000000	.314 427 426 706	1 1 1	2 + 10 4 1 + 10 7 1 + 10 0 8 + 10 3 8 + 10 3 8 + 10 0 9 + 10 0 9 + 10 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1	.357
.12109639693 .6378166000 .637816000139 .20358831987 .90877946596 .90877946596 .90877946596 .90877946596 .2000000000000000000000000000000000000	F/PUD MATRIX .43644835+05 5911853+05 .49256147+05 .58618952+02 973910064-02 .37446975+02 .46042404+04	DPXF/PUD MATRIX		PXF/PUD MATRIX .49599626+05
CD = FH = DMY = DMY = DMY = DMY = DMOY = DMOY = DMOY = CK3 = CK3 = DMT1= DMT1=	۵. ×		V V V C C C C C C C C C C C C C C C C C	PXF/PU(
.23832948690+00 .52341287970+C7 .16234500072-02 .47881444528*C0 .00000000000000000000000000000000000	.99020518+6213541257+63 .11357285+63 .13454159+0022313051+60 .85746851-01	.13454159+00 22313051+00 .85746851-01 21911350-04 .13990145-03 42472508-03	.64097577938+07 -4579971439+07 -97768416573+03 -42097953961+01 -1139478390+04 -95067698469+00 -7788010773+06 -55512456921+06 -555124560072-02 -16234500072-02 -1634500072-02 -1634500000000 -16890584159+06 -16890584159+06 -16890584159+06 -2044155789-03 -57966768569+00 -39780449112+05 -39780449112+05	.11269054+03
CC CC O O O O O O O O O O O O O O O O O	.96573C77+63 13141072+04 .10984679+04 .13084679+1+01 .31587991+01 .83450344+00	.13080428+01 .21687991+01 .83450344+00 -21391040-03 .13552957-02 .41302902-02	Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	.10986280+04
65821803840+03 44296244406-02 72921150604-04 000000000000 40000000000+03 33922726+07 3383922726+07 59700451485+01 18819361707-01 000000000000	.9657: -13141 -10984 -13086 21683	.13080428+61 21687991+01 .83450344+00 21391040-03 .13552957-02 41302992-02	.13000000000000000000000000000000000000	.10986
.65821803840 .44296244406 .72921150604 .000000000000 .40000000000 .31872861626 .53700451485 .18819361707 .000000000000	.86232801+02 11679756+03 .97309399+02 .11585724+00 19245772+00 .74011088-01	.11585724+0L -19245772+0C .74011088-01 -19339809-04 .12087376-03 -36651294-03	2805909708+03 8905909708+03 25676415999+01 132807310099+01 14131551804+04 22144118003+02 2537692182+02 2537692182+02 2537692182+02 2537692182+02 2537692182+02 2537692182+02 2537692182+02 2537692182-03 2537692182-03 2537692182-03 263764936-03 24584804936-01 24584804936-01 24584804936-01	.98002208+02
ARE A: RHO :: RHO :: RHO :: ISP :: ISP :: DRRNG:: MACH:: CCN :: D2 ::	.862: -116: -973(-1158: -192401		T X X X X X X X X X X X X X X X X X X X	. 9801

79863391+05 .61160687+05 .72962105+02 98955491+02 .19733649+02	.72962105+02 98955491+02 .19733649+02 .10796947+00 .2603415+00 27343211+00	.39860319060+15 .28608000000000 .900000000000000 .3051289444+05 .20473118714+03 .15557658333+00	20490849864.6615357029466.40613488858971.40163567840000.0777140676824-0880920196640.40111212221976.40278350279570.400573787813012-03731520000000000	.65158999+05 -87904399+05 .61579417+05 .77284764+02 -5818999+02 -12971886+02	.77284764+02 58189999+02 12971886+02 11065363+00 -45752891+00 36253766+00
49495690+06 .37772627+06 .45311852+03 61445372+03 .12281502+03	.45311852+03 61445372+03 .12281502+03 .66985497+00 .16190864+01 16988163+01 60461109+01	28 +C3 GM 85+07 PHI 25 +C3 AZ 46+01 ALT 35 +O3 VRZ 75+00 UZ	LFZ = DFZ =	.40559838+06 54489088+06 .38034966+06 .47987000+03 36139112+03 80355167+02 .32441152+05	.47987000+03 -36139112+03 -80355167+02 -88820867+00 .28408194+01 -25517147+01
68359979+05 .52011700+65 .52333515+02 84693820+02 .16917164+02	DPXF/PUD MATRIX .6233515+02 .84693820+02 .16917164+02 .92036695-01 .2235625+00 23402838+00 83321170+00	V = .79781567128+C3 Z =35229037985+U7 DZ =13730856525+U3 DDZ = .2646671846+01 WRY = .42545679135+O3 UY = .14076333775+O0		PXF/PUD MATRIX .56182969+05 .75241352+05 .52373440+05 .65994803+02 -,49797612+02 -,11055142+02 -,11055142+04	0PXF/PUD MATRIX .65994803+02 49793612+02 11055142+02 94914855-01 .39156187+00 30985009+60
-,15658750+03 ,11988186+03 ,14311888+00 -,19408522+00 ,38716580-01	.14311888+00 19408522+00 .38716580-01 .21177329-03 .51169534-03 55634436-03	.64052168656+07 45038279855+07 .54846144610+03 40254645876+01 78842252851+03 97774312039+00	6600247833+06 59140125014+06 .28417470111+00 .46446650956+07 .46446650956+07 .47881444528+00 .0000000000000000000000000000000000	.12784914+03 17235894+03 .12070404+03 .15159628+66 11413487+00 25436854-01	.15159628+00 11413487+00 25436854-01 21706738-03 .89736285-03 71113586-03
15199416+04 .11598839+64 .13912979+01 18867741+61 .37710935+00	.13912979+01 18867741+01 .37710935+00 .20567370-02 .49719708-02 5216376-02	.14006060600+04 R = .28864312566+07 Y = .56289097114+03 DY = .38568387995+01 DDY = .13280731000+06 VRX = .91898771686+03 UX = .	CC	.12455873+04 16732707+04 .11673390+04 .14734296+01 11096942+01 24673547+00	.14734296+01 11096942+01 24673547+00 21132554-02 .97231714-02 69139244-02
-13505021+03 -10275570+03 -12320016+00 -16737288+00 33438275-01	.12320016+00 16737288+00 .33438275-01 .18190925-03 .44172769-03 46252236-03	į l	LFA = .20172674729 ETA = .24284973613840 HO = .16710721717 M = .72921150604 = .000000000000 SP = .4000000000000000 RNG = .66343369734 RES = .10945094916 ACH = .30348230767 NI = .00000000000000000000000000000000000	.11101399+03 14865949+03 .1347097+03 .13043716+00 98406169-01 21846329-01	.13043716+00 -98406169-01 -21846329-01 -18758523-03 -77380639-03 -6124C184-03

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.39860319000+15 .286080000000000000000000000000000000000	.63567840000+07 .7875000512-05 .77140678824-08 .26315638259+00 .10849603700+02 .78330279570+00 .57787813012-03 .61031971743-08 .7315200000+00	.70928910+05 -9132905+05 .59307651+05 .60477724+02 -,26798195+02 .51210005+04 .60477724+02 -,26798195+02 -,40921571+02 -,26798195+02 -,19904534+00 -,30095739+00 -,30095739+00	.100000000000+61
6M PHI ALT = C UZ = C LFZ = C TA = C	•	.44142079+06 -36616612+06 .3662860+06 .37543154+03 -1643715+03 -25390316+03 .37543154+03 .37543154+03 -1643715+03 -25390316+03 -25390316+03 -1236643715+03 -1236643715+03	LAM7= LAM7=
.36189408358 +03 .35278957139+07 .17619653197 +02 .18172834836+00 .14147208884 +C3 .33457494 +05 .11195829779 +07 .112914541885 +00	.63781660000+07 .57506000139-C5 .87791612754*00 .15281138648+03 .1060013074+03 .40651458587 *C0 .27374111417-03 .00006000000 .25019006760+00	1 11 111 111	4DA VALUES 33141033909+00 331965965069+02 AMDA VALUES 60580489990+02 30856165926+05
.36189408358+03 35278957139+07 17619653197+02 .18172834836+00 .14147208884+03 .35457403627-02 11195829779+06	63781660000+075750600139-C515281198648+031060012774+0327374111417-030000600000000000000000000000000000000	PXF/PUG MATRIX .61108724+05 .78172325+05 .504134960+05 .51616073+022923336+02 .43787977+04 CPXF/PUG MATRIX .51616073+0222923396+022923396+022923396+022923396+022923396+022923396+022923396+0225923396+0225923396+0225923396+0225923396+0225923396+0225923396+0225923396+0225923396+0234923601+02	٠
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	AE = FH = CHIP= CHIP= CHIP= CHIP= CHIP= CHIP= CHIP= CHIP= CK3 = CK	PXF/PUC - 611 - 781 - 516 - 516 - 516 - 349 - 722 - 349 - 722 - 349 - 722 - 349 - 722 - 349 - 722 - 72	FINAL L LAM3= LAM6= INITIAL LAM3= LAM3=
.640C0000917+07 .26465103983+03 -2677999581+01 -47205572823+03 -4895063581+01 -5870345648+06 -46944401464+06 .28935200589+0	.45473904518+07 .16234500072-02 .47881444528+00 .00000000000 -11126147144+06 -47030056530+00 .22044155789-03 .10831143733+01 .50000000000+00 .39917058410+05	.13912693+0317907787+03 .11624854+03 .11624854+0352563510-0180261059-01 .10100376+0252563610-0190261059-019045730-0359032066-03	48740628019+00 .76807949433+02 .58856570851+03
7 X X Y X X X X X X X X X X X X X X X X	FJ OMY OMY CRNG UDDY CCA HT1 ::	-17355788+04 -11746726404 -11527467401 -51105976+00 -77961097+00 -97949867+02 -11527467+01 -11527467+01 -5116976+00 -37961097+00 -37972713-02 -37972713-02	LAMS= LAMS= LAMS= LAMS=
.14829448474+04 .29197955092+07 .24620459514+03 .35494278452+01 .13280731000+66 .590541893040+03 .15494635701+62 .15494635701+62 .17005912681+02	.39620598199-01 .72921150604-04 .00000000000000 .40000000000000-C3 .66757026373407 .24673263681+04 .20000173553+01 .45996387722-01 .00000000000000	.13555788+04 .11246726+04 .11527467+01 .511059467+01 .97949867+02 .97949867+02 .97949867+02 .97949867+02 .97949867+02	29306736668+00 42943398168+03 52147295108+02 26352105840+05
.14829448474+04 29197955092+07 24620459514+03 .35494278452+01 .1328731000+06 .590541899340+03 .15494635701+02 .17005912681+02	.39620538199 .72921150604 .00000000000 .40000000000 .657506373 .24673263681 .2000173553 .4596387722 .4596387722 .1353548692	.12074966+03 .96485198+03 .9963947+02 .10201838+00 45304248-01 69021755-01 .87175413+01 .10201838+00 45304248-01 69021755-01 50174178-03	-,29306736668+00 ,42943398168+03 ,52147295108+02 ,26352105840+05
	RHO O X O O X O O X O O X O O O X O O O O	. 1207 . 1944 . 9963 . 1020 . 6902 . 8717 . 1020 . 1020 . 5074 . 5074	LAM4:: LAM4:: LAM1:: LAM4::

APPENDIX II

COMPUTER PROGRAM LISTING
FOR OPTIMAL TRAJECTORY TRIAL DECK

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AASSIGN SEMTOJBOEMTIJSIECRJLBELP.
AREWIND MII.
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CTHC=CBSCTHC*RCBNVJ
RCTHC=RC*CTHC
SRAD=SIN[RAD*RCBNVJ
CRAD=CBS[RAD*RCBNVJ
SCRAD=SIN[XRAD*RCBNVJ
                                                                                                      RC8NV=*1745329252E+01
                                                                                            [RISP] 30,40,30
                                                                                                                       9M=*729211506E#04
AA=*6378166E+07
FJ=1*62345E*03
                                                                                    D6 20 I=1,7
) X[I+8]=RLMI[I]
RMD=0.
                                                                                               RMD=FS/RISP
CONTINUE
TO=TI
                                                                                                                     BE=6356784 •
                                                                                               00
                                                                                        80
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FH==5.75E=06
52
FO=1.013.25E+05
FO=1.013.25E+05
FO=1.013.25E+05
FO=1.013.25E+05
FO=1.013.25E+05
FO DB 60 1=1,13
FB INTEGRATION SUBRBUTINE
FB INTEGRATION SUBRETATION
FINANCIAL SUBRETATION SUBRETATION
FINANCIAL SUBRETATION SUBRETATION
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	SUBROUT INE
[11,5] # # # # # # # # # # # # # # # # # # #	00NSTANTS FOR STANTS F
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28 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	9EF1C10-YSC COSE+C3 9EF1C1ENTS COSE+C3 ETAIL 114-52824387840EV ETAIL 114-52824387840EV ETAIL 114-52824387860EF0 ETAIL 114-52804132EF0 ETAIL 114-52805EF0 ETAIL 118-100511345875EF0 ETAIL 11025738875EF0 ETAIL 11025738875EF0 ETAIL 110537066087EF0 ETAIL 134-33629812F0	LA (2) = = 21619280500E + 1.2 (12) = = 21619280500E + 1.2 (13) = = 1.3 (6.2 + 0.3 0.3 0.2 (1.2 + 0.3 0.2 0.2 0.3 0.2 (1.2 0.3 0.3 0.2 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	CLA[17] = -17289709179E=10 CLA[18] = -17289709179E=10 CLA[1] = +-1690547318E=01 CA[2] = -+44068023555E=01 CA[2] = -+44068023555E=01 CA[3] = -+44068357082E=01 CA[4] =022608357082E=01 CA[5] = -+070956344732E=02 CA[5] =022608357082E=02 CA[5] =022608357082E=02 CA[5] =022608357082E=02 CA[6] =022608357082E=02 CA[1] =02260835038E=04 CA[1] =02260835038E=04 CA[1] =02260835038E=04 CA[1] =02260835038E=04 CA[1] =02260953597E+01 CA[1] =02260953597E+01
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CA=CGSIA[FGR]
SB=SIN[BETGR]
CB=CGSIBETGR]
CB=CGSIBETGR]
D6 90 I=1,3
U0[I]=SA*[CB=VXRXV[I]+SB*VXR[I]]+CA*VR[I]
VECTBRS NEEDED FOR DOWN RANGE AND CROSS RANGE IN PRINT SUBROUTINE
R0=SGRT[X[I]+X[2]+X[2]+X[3]+X[3]]
RXVOB[I]=X[1]+X[3]=X[6]=X[1]
RXVOB[2]=X[4]+X[3]=X[6]=X[1]
RXVOB[3]=X[1]=X[5]=X[4]+X[2]
RXVOB[3]=X[1]=X[5]=X[4]+X[2]
RXVOB[3]=X[1]=X[4]=X[4]=X[4]
                                                                                                                                                                                                                                                                                                             VR[1] = VR[1] / VRM
VXR[1] = VR[2] + X[3] = VR[3] * X[2]
VXR[2] = VR[3] * X[1] = VR[1] * X[3]
VXR[3] = VR[1] * X[2] = VR[2] * X[1]
VXRM = SGRT[VXR[1] * VXR[1] + VXR[2] * VXR[3] * VXR[3]]
                                                                                                                                                                                     AB(2) = COP * SIA

AB(2) = COP * SIA

AB(3) = COP * COA

COMPUTATION OF UD BAR IN TERMS OF ALEG AND BETG

VR(1) = X(4) = OM * (AB(2) * X(2) = AB(3) * X(2) 1

VR(2) = X(5) = OM * (AB(2) * X(1) = AB(1) * X(3) 1

VR(3) = X(5) = OM * (AB(1) * X(2) = AB(2) * X(1) 1

VRM = SORT[VR(1) * VR(1) + VR(2) * VR(2) + VR(3) * VR(3) 1

DO 70 [= 1,3]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                RXVOBILI #RXVOBILI / RXVO
RVR (1) = RXVOB (2) *ROB (3) *RXVOB (3) *ROB (2) RVR (2) = RXVOB (3) *ROB (1) "RXVOB (1) *ROB (1) START OF TRIAL INTEGRATION
                                                                                                                                                                                                                                                                                                                                                                                         VXR(I) #VXR(I) /VXRM
VXRXV(I) #VXR(2) #VR(3) #VXR(3) #VR(2)
VXRXV(2) #VXR(3) #VR(1) #VXR(1) #VXR(3)
VXRXV(3) #VXR(1) #VR(2) #VXR(2) #VR(1)
ALFGR#ALFG*RCGNV
BETGR#BETG*RCONV
SAFSIN (ALFGR)
ACA[13]=+.54856065063E+00

ACA[14]=-.11125040668E+00

ACA[15]=+.13269270447E-01

ACA[15]=-.85605013509E-03

ACA[17]=+.25986787609E=04

ACA[18]=+.35797751349E-08

ACA[18]=+.35797751349E-10

COMPUTATION OF UNIT NORTH VECTOR
                                                                                                                                                 COA=COS[RAZ]
SIP=SIN[RPHIL]
COP=COS[RPHIL]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     ROB [1] *X[1] /RO
                                                                                                                     RAZ#AZ*RCBNV
SIA#SIN[RAZ]
                                                                                                                                                                                                                                                                                                                                                                               De 80 1=1,3
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1PS TAKEN]
200 FORMAT (1H0,50X,25HEND CONDITION MULTIPLIERS,/,5[E15.8,2X]]
210 FORMAT (1H0,50X,19HBOUNDARY CONDITIONS)
220 FORMAT (1H0,50X,14HDESIRED VALUES,/,5[E15.8,2X])
230 FORMAT (1H0,50X,14HDESIRED VALUES,/,5[E15.8,2X])
240 FORMAT (3E18.1]
250 FORMAT (3E18.1]
250 FORMAT (1H1,/,51X,14HINITIAL VALUES)
270 FORMAT (1H1,/,51X,14HINITIAL VALUES)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             190 FORMAT (1HO/50X/19HINTERMEDIATE VALUES/1X/14/1X/23HINTEGRATION STE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   77770 A3
77760 A7
77750 A11
                                                                                                                                                                                                                                                                                                                                                                                                                            160 CALL RK713 [T.STEP,TGL,X,X,15,1000,M]
IF (LCH) 170,170,180
170 T=STEP
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CALL DEG [K,TF,DX]
PRINT 270, M
CALL PRINT (TF,X,DX)
CALL BOUND (TF,X,DX)B,ERR]
PRINT 200, PB
PRINT 210
PRINT 220, [B[I],I=1,12]
PRINT 220, [B[I],I=1,12]
PRINT 240, ERR
69 T0 10
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      77772 A2
77762 A6
77752 A10
                                                                                     110 FPT=TF
120 LCH=1
130 CANT
                                                                                                                                                                                                                                                                                                                                                      IF (TF-STEP) 150,150,160
                                                                        CALL PRINT (TI,X,DX)
T=TI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               CALL DEG (X,T,DX)
PRINT 190, M
CALL PRINT (T,X,DX)
TOL= .05
CALL DEG [X,TI,DX]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      77774 A1
77764 A5
73754 A9
                                                                                                                                                                                                                                                                                                 G0 T0 160
STEP=T+DTP
                                              PRINT 260
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  GB TB 140
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    CONTINUE
                                                                                                                                                                                                                                                                      STEP=FPT
                                                                                                                                                                                                                                                                                                                                                                                                         STEP=TF
                                                                                                                                                                                                                                                                                                                                                                                   150 LCH=1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   COMMON ALLOCATION
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77766
77756
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77740 A15 77730 A19 77720 A23 77710 B3 77710 B3 77660 B7 77660 A2 77066 CLA 77066 CLA 77066 CLA 77066 CCLA 77066 CCLA 77066 CCLA 77066 CCC 76746 ACCA 76746 ACCA 76756 ACCA 7675	00127 B 002176 J 00213 BFTG 00223 RPHIL 00233 SIP 00263 RC	RK713
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	DX 11 ATL COA COA T ALFGR	a 1 ≈ 2 × 1
777388 777788 777788 777788 777788 77768 77768 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030 777030	000071 000175 000201 000211 000241 000241	DES
A13 A173 A21 BB BB BB BB BB BB BB BB BB BB BB BB BB	X X X X X X X X X X X X X X X X X X X	Z II
20000000000000000000000000000000000000	18N 00033 00167 00200 00207 00227 00227 00237	REQUIRED COS S
A418 B800 B800 B800 B800 B800 B800 B800 B8	ALLBCATIBN KLMI VXR UCH DJP THC RAZ CBP SSA RXVO ERR	
777746 777736 77771666 77771666 777067 77067 77067 77067 77070 7707 770	PRBGRAM 00015 00161 00177 00205 00225 00225 00235	SUBPRGGRAMS SQRT BBUND THE END

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DIMENSION X (151) DX(153) ALPH(131) BETA(13,121) CH(131)
DIMENSION X (151) VXR(31) U(31) ALB(31) DB(31) AB(31) UO(31) UOD(31)
DIMENSION VRC31, VXR(31) RXVOB(31) RXVOB(31) RXVOB(31) RXVOB(31) RXVOB(31) RXVOB(31) RXVOB(31) DIMENSION UXE(31) UYE(31) PB(5)
DIMENSION UXE(31) UYE(31) PB(5)
LOGMON AO,A1,A2,A4,A5,A6,A7,A8,A9,A10,A11,A12,A13,A14,A15,A16,A
L17,A18,A19,A20,A21,A22,A6,A73,B1,B2,B3,B4,B5,B6,B7,B8,D1,D2,D3,D4
COMMON GM,PHIL,AZ,BETA,ALPH,CH,AB,ALFA,BEDA,RCONV,CLA,CA,ETA,AREA,
LWKG,R,RE,VR,VRM,U,ALT,RH9,QQ,ALB,DB,BE,OM,AA,FJ,FH,FD,F,RISP,RMD,E
ZXA,UO,UOD VS,ACH,TO,FS,PO,WKGO,PRES,HEATC,CK1,CK2,CK3,RCURV,ROB,RX
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     SCHI*[U[1]*VXR[1]+U[2]*VXR[2]+U[3]*VXR[3])/VXRM
CCHI*[[U[1]*X[1]+U[2]*X[2]+U[3]*X[3]]*VRM2*VDX*UP3]/VXRXV
                                                                                                                                                                                                                                                                                                                                                                                                                                                 VXR.13]=VR[1]*X[2]=VR[2]*X[1]
VXRM*SQRT[VXR[1]*VXR[1]+VXR[2]*VXR[2]+VXR[3]*VXR[3]]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         CALL TANGL (SCHI,CCHI,PANG)
RANGE WILL BE WRBNG IF RANGE ANGLE > 180 DEGREES
SCHI*RVR[1]*X[1]+RVR[2]*X[2]+RVR[3]*X[3]
CCHI*ROB[1]*X[1]+ROB[2]*X[2]+ROB[3]*X[3]
CALL TANGL (SCHI,CHI,PHIR)
CCHI**[3]*RXVOB[1]*X[2]*RXVOB[2]*X[3]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         CALL TANGL [SCH], CCH], ALFA]
CCHI*[X[1]*DX[1]+X[2]*DX[2]+X[3]*DX[3]]/[R*V]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   VXRXV*SQRT[VRM4*R2-VDX*VDX*VRM2]
UP3*U[1]*VR[1]+U[2]*VR[2]+U[3]*VR[3]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 VDX=VR[1]*X[1]+VR[2]*X[2]+VR[3]*X[3]
                                                                                                                                                                                                                                                                                                                                            DCEL *DČEL+ALB (1) *ALB (1) +DB (1) *DB (1)
DCEL *SQRT (DCEL) /WKG
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    [[PH]R+360+]++5E+04] 30,20,20
                                                                                                                                                                                    V=SQRT[X[4]**2+X[5]**2+X[6]**2]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          CD=CA+2.*ETA*CLA*[1..CCHI]*CLA.
                                                                                                                                                                                                                                                                         CCHI = SQRT [U[1] + U[1] + U[3] + U[3] 1
CHIY = ATAN [SCHI/CCHI] / RCBNV
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       CALL TANGL (SCHI, CCHI, BEDA)
SCHI = SGRT (SCHI + SCHI + CCHI + CCHI)
                                                                                                                                                                     3V0B, RVR, RLGO, UXE, UYE, P6PU, PB
                                                                                                                                                                                                                                                                                                                                                                                                                VXR[1] *VR[2] *X[3] *VR[3] *X[2]
VXR[2] =VR[3] *X[1] *VR[1] *X[3]
                                                                                                                                                                                                                                          CALL TANGL [SCHI, CCHI, CHIP]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 SCH1 = SQRT [1 • "CCH1 * CCH1]
PHIC*ATAN [CCHI/SCH1]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              SCHI#SQRT[1. CCHI*CCHI]
SUBRBUTINE PRINT
                                                                                                                                                                                                                                                                                                                                                                                                  VRY4#VRW0*VRW0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       CCHI #UP3/VRM
                                                                                                                                                                                                                                                                                                                                                                                 VRM2#VRM*VRM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    XXNG*PHIC*RE
                                                                                                                                                                                                                                                                                                                             10 I=1,3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        CL = CLA * SCHI
                                                                                                                                                                                                       SCH1 = U [3]
                                                                                                                                                                                                                         CCHI + U [1]
                                                                                                                                                                                                                                                           SCHI #U[2]
                                                                                                                                                                                                                                                                                                             DCEL *0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               R2=R*R
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   PHIR#0.
                                                                                                                                                                                                                                                                                                                              8
                                                                                                                                                                                                                                                                                                                                               9
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      င္လ
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              U
```

```
PRINT 110, WKG, [VR[I], I=1,3], VRM, [U[I], I=1,3], ALFA, [ALB[I], I=1,3], 18EDA, [DB[I], I=1,3], AREA, CL, CD, ETA, RHG, QO, AA, BE, GM, FJ, FH, FD, F, [AB[I], I=1,3], RISP, RMD, CHIP, CHIY

21, I=1,3], RISP, RMD, CHIP, CHIY

PRINT 120, RAGA, XRNG, PANG, DCEL, PRES, UO, ACH, UOD

PRINT 130, CA, CLA, EXT, RLG

PRINT 140, DX(8], RLAT, RLG

HAM=X[9]*DX[1] +X[10]*DX(2]+X[11]*DX[3]+X[12]*DX[4]+X[13]*DX[5]+X[4]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      14]*DX.65]*X[15]*[CK1*RMD+0K2*DX[7]+CK3*DX[8]]
PRINT 150, X[9],X[10],X[11],HAM,X[12],X[13],X[14],X[15],DX[9],DX[1],LOX(11],P8PU,DX[12],DX[13],X[15],DX[13],DX[14],X[15],DX[14],DX[15],DX[14],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX[15],DX
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  CLAT=SGRT[10-SLAT*SLAT]
RLAT=ATAN[SLAT/CLAT]/RC6NV
PRINT 100, T.R.V.GM, [X[1], I=1,3],PHIL,[X[1], I=4,6],AZ,[DX[1],I=4,8
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    #E18.11.2X,5HG
#E18.11.2X,5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                #E18.11,2X,5HV
#E18.11,2X,5HZ
                                                                     AJ=CK1*MCG+CK2*X[7]+CK3*X[8]
CGMPUTATION OF VECTORS NEEDED FOR LONGITUDE
RPHIL=PHIL*RCONV
RAZ*AZ*RCONV
SIA*SIN(RAZ)
CGP*COS(RAZ)
SIP*SIN(RPHIL)
WT=OM*[T*TO]
WT=OM*[T*TO]
CMT*COS(WT)
SINT*SIN(WT)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               UXE(13)=C0P4*SIWT+SIA*SIP*CWT
UXE(23)=C0A*SIWT+SIA*SIP*CWT
UYE(13)=SIA*SIWT-C0A*SIWT-COA*SIWT-COA*SIWT-COA*SIWT-COA*SIWT-COA*SIP*CWT
UYE(23)=SIA*SIWT-COA*SIP*CWT
UYE(23)=SIA*CWT-COA*SIP*CWT
UYE(23)=SIA*CWT-COA*SIP*CWT
UYE(23)=SIA*SIWT-COA*SIP*CWT
UYE(23)=SIA*SIWT-COA*SIP*CWT
UYE(23)=SIA*SIWT-COA*SIP*CWT
UYE(23)=SIA*SIWT-COA*SIP*CWT
UYE(23)=SIA*SIWT-COA*SIP*CWT
UYE(23)=SIA*SIWT-COA*SIWT
UYE(13)=SIA*CWT-COA*SIWT
UYE(13)=SIA*SIP*CWT
UYE(13)=SIA*CWT
UYE(13)=SIA*SIP*CWT
UYE(13)=SIA*CWT
UYE(13)=SIA*SIP*CWT
UYE(13)=SIA*SIP*CWT
UYE(13)=SIA*SIP*CWT
UYE(13)=SIA*CWT
UYE(13)=SI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    #E18.11.2X,5HR
#E18.11.2X,5HY
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       GG TG 50
70 IF [RLNG=360.] 90,90,80
80 RLNG=RLNG=360.
60 TG 70
90 CGNTINUE
SLAT=SLAT/R
CONTINUE
RANG*RCONV*RE*PHIR
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           1M *E18.11,/,6H X
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    100 FBRMAT C1HO, SHT
       ဓ္ဓ
                                                                                                                           U
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 U
```

11,2X,5HDY = E18.11,2X,5HDZ = E18.11,2X,5HDZ = E18.11,2X,5HUZ = E18.11,2X,5HVRZ = E18.11,2X,5HCD = E18.11,2X,5HUZ = E18.11,2X,5HCD = E	77770 A3 77760 A3 77760 A1 8 77750 A19 8 77730 A23 77700 B3 77700 B4 77700 B4
#	00000000000000000000000000000000000000
7	0 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
811,611 11,611,611,611,611,611,611,611,61	A41 A45 A45 A413 A413 B417 B417 B60 B60 B7 B7 B7 B7 B7 B7 B7 B7 B7 B7 B7 B7 B7
22.5HPH1	77754 77754 77754 77754 777734 777136 77704 77007 77007 77007 77007 76746 76746 76746
110 120 130 140 150	NO AL AFERBACORUM SACO NO AL AFERBACORUM SACO NO
MA	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~

76724 76700 76660	77.89 78.89 0.00 0.00 0.00 0.00 0.00 0.00 0.00	76722 76676 76646	RCURV RLGO PB	76714 76670	ROB XE	76706 76662	RXVOB UYE
PRGGRAM	ALLOCATION	z					
DUMMY	×	DUMMY	X	00033	VXR	***	-
00045	PRINT	00044	>	94000	SCHI	0	CCHI
00052	CHIP	00054	CHIY	00056	DCEL	0	VRMZ
00062	VRM4	00064	VXRM	99000	XOX	0	25
00072	VXRXV	00074	UP3	92000	J	0	8
00105	PANG	00104	PHIR	00100	PHIC	00110	XRNG
00112	RANG	00114	Ą	00116	RPH1L	_	RAZ
00122	SIA	00124	CBA	00126	SIP	_	C 6 D
00132	-3	DUMMY	 	00134	L SO	'n	FWIS
00140	SLAT	00142	CLNG	00144	SING		RI NG
00120	ĭ	00152	RLAT	00154	E A I		ı
SUBPREGRAMS	AMS REQUIRED	SED					
SGRT THE END	TANGL	A T	ATAN	NIS	ces		

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SUBRBUTINE RK713 [TI.TF.TBL.XI.X.N.KT.M]
SEVENTH BRDER RUNGE-KUTTA INTEGRATION WITH STEPSIZE CONTROL

M IS THE NUMBER OF STEPS NEEDED

N IS THE NUMBER OF ITERATIONS

KT IS MAX NUMBER OF ITERATIONS

KRAY F STORES THE 13 EVALUATIONS

ARRAY F STORES THE 13 EVALUATIONS

ARRAY F STORES THE 13 EVALUATIONS

ARRAY F STORES THE 13 EVALUATIONS

F(0) IN FEHLBERGS REPORT IS IN F(1,J)

F(0) IN FEHLBERGS REPORT IS IN F(1,J)

F(1) IS IN F(1+1,J)

PARMETERS FOR DOG SUBRBUTINE MUST BE STORED IN COMMON

DIMENSIONS MUST AGREE WITH NUMBER OF DIFFERENTIAL EQUATIONS AND

NUMBER OF CONSTANTS IN THE PARTICULAR FEHLBERG FORMULA USED

DIMENSION F(13,15), XDUM(15), TE(15), XI(15), ALPH(13), BETA(13,12)

11), KI(15), CH(13)
                                                                                                                                                                          C0MMON A0,A1.A2,A3,A4,A5,A6,A7.A8,A9,A10.A11,A12,A13,A14,A15,A16,A
117.A18,A19,A20,A21,A22,A23,B0,B1,B2,B3,B4,B5,B6,B7,B8,D1,D2,D3,D4
C0MMON GM,PHIL,A2,BETA,ALPH,CH
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        A=X[1]

TE[1]=DT*[F[1,1]+F[11,1]*F[12,1]*F[13,1]]*41,/840,/A

TE[1]=DT*[F[1]]

D0 140 1=2,N

IF [ABS[TE[1]]*ER] 140,140,130

CONTINUE
                                                                                                                                                                                                                                                                                                                                                               D0 50 I=1.N
D0 50 J=1.NN
XDUM[I]=XDUM[I]+DT*BETA[K,J]*F[J,I]
TDUM=T+ALPH[K]*DT
                                                                                                                                                                                                                                                                                                                                                                                                             CALL DEG TXDUM, TEUM, TED
DB 60 1=1,N
C F(K,1)=TE(1)
C GNTINUE
DB 80 1=1,N
O XDUM(1)=X(1)
DB 90 1=1,N
DB 90 L=1,13
O X[1]=X(1)+T+CH(L)*F(L,1]
DB 90 1=1,N
DB 90 L=1,13
O X[1]=X(1)+D1*CH(L)*F(L,1]
                                                                                                                                                                                                                                                DE 10 I=1,N

X[1]=X[[1]

CALL DEG (X, 7,7 FE)

DE 30 I=1,N

F[1,1]=TE[1]

DE 40 I=1,N

NDM[1]=X[1]

NN=K-1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                GB TB 120
                                                                                                                                                                                                                            DT=TF=T
M=0
                                                                                                                                                                                                               _*_I
                                                                                                                                                                                                                                                                900
                                                                                                                                                                                                                                                                                                  30
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       130
                                                                                                                                                                                                                                                                                                                                         0
                                                                                                                                                                                                                                                                                                                                                                                                                                         900
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     100
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60,160,150 0,180,180 210,200	77770 A3 77760 A7 77750 A11 777740 A15 77770 A19 77770 B3 77710 B3 77700 B7	DUMMY XI DUMMY N 000740 L DUMMY 1I 000751 A DUMMY 18L
4 6	CPD B B B B B B B B B B B B B B B B B B B	AK DCM AK DCM
ABS(DT1)) BS(DT1)) BS(DT1)) 190,220 TF-T)) 21	77777777777777777777777777777777777777	00676 00734 00737 00743 00747
1*[TBL/E] DT]-10.*, T1 T1 T1 T1 T1 T1 T1 T1 T1 T2	A A A A A A A A A A A A A A A A A A A	X DUM M NN 3 TF DT1
	3N 77774 77774 77754 777784 777784 777784 777784 777784 777784 77784 77784 77784 77784 77864 77864 77864 77864	00640 DUMMY 00736 00741 DUMMY 00755 EQUIRED
1155 1155 1175 1175 1175 1175 1175 1175	ALLBCAT18N A0 A4 A16 A16 A20 B0 B4 B8 BETA BETA	~ ≪
は、またまで まっぱい まっぱい まっぱい はっぱい はっぱい はっぱい はっぱい はっぱい はっぱい はっぱい は	MM BN N N N N N N N N N N N N N N N N N	00000000000000000000000000000000000000
	0 0	

```
C9=[12**FD*A*[3**E2*1.]*B+3**FH*BB*[1**7**E2]*10**FJ*A]*R2]
                                                                                                                                                                        A= [AB [1]*X[1]+AB [2]*X[2]+AB [3]*X[3]]*R]
BE2=BE*BE
                                                                                                                                                                                                                                                                CONTINUE

REAA*BE/SORTIC63

C13=C12*A*RI

C13=C12*A*RI

D0 50 1=1,3

PVXB [1,1]=0.

PVXB [1,2]=0M*AB [3]

PVXB [1,3]=-0M*AB [2]

PVXB [2,3]=0M*AB [1,2]

PVXB [2,3]=0M*AB [1,2]

PVXB [2,3]=-0VXB [1,2]

PVXB [2,3]=-PVXB [1,2]

PVXB [2,3]=-PVXB [1,2]
                                                                                                                                                                                                                                                                                                                                                                       GP=B*[2**FJ*A+C3+3**C4]
C7=[2*5*GR+1*5+B*[C1+*5*C2]]*R]
                                                                                                                                                                                                        C1=3**FD*[1*/7*=2**E2+3**E4]*B
                                                                                                                                                                                                                                                                                                                                                                GR=B*[FJ*[1.=5.*E2]+C1+C2]
                                                                                                                                                                                                                      C3=4 ** FD * A * [3 * /7 * * E2] *B
                                                                                                                                                                                                                                                                                                                                                                                      C8=2**GP+B*[C3+1*5*C4]
                                                                                                                                                                                                                C2=FH*BB*A*[3..7.*E2]
                                                                                                                                                                                                                              C4=FH*BB* [E2*1*/5*]
C5=AA*AA*BE2
                                                                                                                                                                                                                                                    [C6] 30,40,40
                                                                                                                                                                                                                                            C6=BE2+C5*E2
                                                                                                                                                           B=AA*AA*RZI
                                                                                                                              CONTINUE
R=SQRT [R2]
                                                                                                                                                     R2I=1./R2
                                                                                                                                                                  BB=AA*RI
                                                                                                                                                                                                E4=E2*E2
                                                                                                                                             RI=1./R
                                                                                                                                                                                        E2=A*A
                                                                                                                        R2=0•
                                                                                                                        010
                                                                                                                                                                                                                                                           804
                                                                                                                                                                                                                                                                                                              ည္ထ
   をごてりらるより与れをろてりらるよう 気やをごてりらるくろ らかをごていらる くりられ もごて くららく うらかを ごうららっか カヤヤヤ ヤヤヤ ヤヤ ちゃく ちをもちをもをもる ごうごう ごうごう ごうじょ しょしょしょしょ
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```
D6 60 J=1,3

D7 [1+3, J]=CC1*(2*R21*(C7*X[I]+C8*AB[I])*X[J]+B*(C9*X[I]+C10*AB[I])]

1*[AB[J]-C12*X[J]]]

D6 70 I=1,3

D7 70 I=1,3

D7 [1+3, I]=P[I+3, I]=CC2

VR[I]=X[4]-BM*[AB[Z]*X[3]-AB[3]*X[2]]

VR[I]=X[5]-BM*[AB[I]*X[1]-AB[I]*X[3]]

VR[2]=X[5]-BM*[AB[I]*X[1]-AB[I]*X[3]]

VR[2]=X[5]-BM*[AB[I]*X[2]-AB[2]*X[1]]

VR[2]=X[5]-BM*[AB[I]*X[2]-AB[2]*X[1]]

VR[2]=X[5]-BM*[AB[I]*X[2]+VR[2]+VR[3]*VR[3]

IF [VPM2] 80,90,90
                                                                                                                                                                                                                                                                UM=SGRT[UM2]
D6 130 I=1,3
U[1]=U[1]/UM
ALT=R=RE
CALL ATM6S [ALT,TEMP,PRES,RH6,VS,DVS,DRH6,DPRES]
C10=[2•*FJ+12•*FD*[1•/7•=E2]*B+6•*FH*A*BB]*RI
C11=[1•+GR]*RI
                                                                                                                                                                                                                                                                                                                  ACH=VRM/VS
CALL AERBD (ACH,CLA,CA,ETA,DCLA,DCA,DETA)
F=FS+EXA*[PO-PRES]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                HTM[1, J] = WKG1* [C7+C9] *VR [1] *VR [J]
HTM[1, I] #HTM[1, I] + [F+C7*VRM2] *WKG]
C10=2,*CLA2* [1,*2,*ETA*CA]
                                                                                                                                                                                                    D0 100 I=1,3
UCI1=U0CI1+[T-T01*U0D[I]
UM2=UCI1*UCI1+UC21*UC21+UC31*UC31
IF [UM2] 110,120,120
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             C11=00*00*WKG1*WKG1
C12=-C10/VRM*C11*CK3
D8 170 1=1.3
U8PT[1]=0.
                                                                                                                                                                                                                                                                                                                                                                  00=.5*RHB*AREA*VRM2
CLA2=CLA*CLA
C1=QQ*CLA
C3=CA+2.*ETA*CLA2
C4==2.*ETA*CLA2
                                                                                                                                                                                                                                                                                                                                                WKG = WKGO = KMD * [T = TO]
                                                                                                                                                                                          VRM=SQRT[VRM2]
                                                                                                                                                                                                                                                                                                                                                                                                                                C7=C6*CLA
C8=C6*C3/VRM
                                                                                                                                                                                                                                                                                                                                                                                                                                                            De 150 I#1,3
De 140 J≖1,3
                  C12=A*RI
CC1=GM*R2I
CC2=CC1*C11
CC3=CC1*GP
D0 60 I=1*3
                                                                                                                                                                                                                                                                                                                                                          WKGI=1./WKG
                                                                                                                                                                                                                                                        CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                   C9=C6*C4
                                                                                                                                                                                                                                             UM2=0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  150
                                                                              9
                                                                                                            20
                                                                                                                                                                       800
                                                                                                                                                                                                                                             110
                                                                                                                                                                                                                                                                                     130
                                                                                                                                                                                                                100
```

```
D8 250 I=1/3
D8 250 J=1/3
D8 250 J=1/3
P[I+3,J]=P[I+3,J]+WKGI*[PHI[I,J+3]+P[I+3,J+3]+[[ALBI]-DB[I]]/RH0*
1DRH0+C10*U[I]]*PAX9[J]-C5*PVXB[I,J]
P[I+3,J+3]=[P[I,J]*P[I,J+3]]*WKGI
PHI[I+3,J]=-WKGI*[C7+C9]*VR[I]*VR[J]
D8 160 J=1,3
UBPT[I]=X[J+11]*HTM[J,I]+UBPT[I]
UBPT[I]=UBPT[I]+X[15]*C12*KR[I]
UBPTM=UBPT[I]*UBPT[I]+UBPT[2]*UBPT[2]+UBPT[3]*UBPT[3]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  30 P[1,1] = P[1,1] - CC10
08 240 1=1,3
08 240 0=1,3
PHI[1,4=3] = 0.
PHI[1,4=3] = 0.
PHI[1,4=3] = 0.
PHI[1,4=3] = PHI[1,4=3] + P[1,K] * PVXB[K,J]
40 P[1+3,4=3] = P[1+3,4=3] + P[1,K+3] * PVXB[K,J]
C10 = *EXA*PPRES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   DX (I+3) = WKGI* [ALB []] /CLA*DCLA+C12*VR[]]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 DG 220 I=1,3
DG 220 J=1,3
P(1,J) = [U([]*VR[J]*2.*VR[I]*U(J]]*C7
P(1,J+3)=VR[I]*(C8*VR[J]+C9*U(J)]
                                                                                                                                                                                                                                                                                                                                                                   VDU=VR[1]*U[1]+VR[2]*U[2]+VR[3]*U[3]
                                                                                                                                                                                                                          U[1] =U[] +PBPU* [UBPT[] -U[]]
UM2=U[] +U[] +U[2] +U[2] +U[3] +U[3]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   C12=C9*DCLA+C10*DETA+C11*DCA
                                                                                                                                                                                                                                                                                                                                                                                        C2=-C1*VDU/VRM2
C5=QQ*[C3/VRM+C4*VDU/VRM2]
D0 210 I=1/3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  P [1+3,1+3] = P [1+3,1+3] - C12
PH; [1+3,1] = PH; [1+3,1]+C11
C7=VRM=VDU
                                                                                                                                                                                                                                                                                                                                                                                                                                                                          AL8[1] = C1*U[I] +C2*VR[I]
DB [I] = C5*VR[I]
                                                                                                                                       D6 180 I=1,3
U6PT[]]=U6PT[]]/U6PTM
D6 190 I=1,3
                                                                                                              UBPTM=SORT [UBPTM]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                C9*C8*ETA*2**CLA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  C11=[C1+F]*WKG]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 C7#1./[VS*VRM]
                                                                                                                                                                                                                                                                              UM=SGRT (UM2)
DG 200 I=1.3
U[1]=U[1]/UM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           230 I=1,3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              C12*C5*WKGI
D8 260 I=1,3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  CC10=C7*VDU
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     C8=C6*C7*2+
                           160
170
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C8=VRM/VS*DVS/VS
D8 290 1=1,3
DX[I] =0.
DX[I] =0.
DX[I] =1,3
DX[I] =1,3
DX[I] =C7*DX[I] -C8*PAXB[I]
D8 300 1=1,3
D8 300 1=1,3
D8 300 1=1,3
D9 15 1,3
D9 15 1,3
D9 16 1,3
D9 310 1=1,3
D9 320 I=1,3
D9 32
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              DX[7]=HEATC*C8*VRM2*VRM
DX[8]=C7*C6+VDU*C9/CK3
C10=DRH0*[•5*CK2*HEATC/C8*VRM2*VRM+2•*CK3*DX[8]/RH0]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            30 RH 50.4

40 C6NTINUE

C8=SGRT[RH6]

C9=-C5/VRM*C7*CK3

D6 350 1=1,3

DX[1+44]=0.0

DX[1+47]=0.0

                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  IF [RH6] 330,340,340
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    C7#QQ*GQ*WKGI*WKGI
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    C4=CA*CA
C5=CLA?*C3*2*
C6=C4+C5
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 P[I, J]=0*
PHI[I, J]=0.
PHI[I, J+3]=0.
                                                                                                                                                           280
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            310
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             330
                                                                                                                                                                                                                                   290
                                                                                                                                                                                                                                                                                                                                                                                     300
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  320
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                350
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      360
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PU*C5J+CK2*3**HEATC*C8. *DCAJ+2**ETA*CA*DCLAJ *C1J *PMXB[1]	77770 A3 77760 A1 77760 A1 77760 A1 77740 A19 77710 B3 77700 B7 7766 A2 7766 A2 77066 CLA 77066 CLA 76766 CCA 76766 CCA 76766 CCA 76766 CCA
*[C6*****VRM=3**V CLA*[DETA*CA+ETA* *DCA+C1=VDU/VRM*; [1]+C1=*DX[1]+C2 [1]+C2*PMXB[1]+C3 [1]+C2*PMXB[1]+3] *PVXB[C,1] *3)+C9*U[1] *15]*PUXB[1]	77772 A2 77762 A6 77752 A10 77732 A18 77732 A22 77712 B2 77712 B2 77702 B6 77672 PHIL 77044 VR 77044 VR 77040 CH 77040 FH 77040 FH 77040 FH 77040 FH 77040 FH 77040 FH 77040 FH 77040 FH 77040 FH 77070 RHB 77070 RHB 77070 RHB 77070 RHB 77070 FH 77070 FH 77070 FH 76770 VS
1=C7/VRM2/VRM 2=VRM*[CK3*C1 =CX3*C1A*[CCLA 380 1=10,*PAX XB[1]=[10,*PAX XB[1]=[10,*PAX 390 1=10,*PAX 390 1=10,*PAX 113=0,*PAX 400 1=10,*PAX 400 1=10,*PAX 400 1=10,*PAX 400 1=10,*PAX 400 1=10,*PAX 400 1=10,*PAX 410 0=10,*PAX 410 0=	77774 A1 77764 A5 77754 A9 77734 A17 77734 A17 77714 B1 77704 B5 77674 D1 77674 D1 77062 E1 77062 E1 77062 E1 77062 E1 77062 F1 77012 D8 77012 D8 76772 R1SP 76772 R1SP
ALL 60 00 X 9 8 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PA A A A A A A A A A A A A A A A A A A
A	00 + + + 0 + + + + + + 0 0 0 0 0 0 0 0

				AERBD	∢	ATMBS	SGRT
					RED	RAMS REQUIRED	SUBPROGRAMS
							51
	ŭ	e O	00510	C. L	00506	KGI	00504
	ရှ		00200		00476	S	047
DRHB	7	2	00470	띹	00466	Σ	940
	40		DUMMY	۲ ۲	00460	3	045
	ស្ន	U	00452		00450		7 7
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Z.	00374	œ	00372		00370		· vo
	36		00365	Ξ	00343	PPT	33
PJXB	8	PMXB	00305	₫	00263	83 83	23
H	ঽ	a .	00035		DUMMY		Σ

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SURRBUTINE ATMRS [ALT,TEMP,PRES,RHB,VS,DVS,DRHB,DPRES]
CRMMON AO,A1,A2,A3,A4,A5,A6,A7,A8,A9,A10,A11,A12,A13,A14,A15,A16,A
117,A18,A19,A20,A21,A22,A23,B0,B1,B2,B3,B4,B5,B6,R7,B8,D1,D2,D3,D4
NBTE THAT FORMULAS ARE NOT ACCURATE FOR ALTITUDE GUTSIDE 0 TO 200
ALT MUST BE IN METERS
TEMP IS IN DEGREES KELVIN
PRES IS IN NEWTONS/M2
RHO IS IN KG/M3
                                                                                                                                                                                                                                                                                                                        DA=-AO/(E1*E1)+A2/E2-A4/E3+[2•*A6*Z+AAB]/E4-(2•*A12*Z+AAC]/E5-[2•*
1A18*Z+AAD]/E6
                                                                                                                                                                                                                                                                                                                                                               TEMP=B0+Z*[B1+Z*[B2+Z*[B3+Z*[B4+Z*[B5+Z*[B6+Z*[B7-B8*Z]]]]]]]
DTFMP=B1+Z*[2**B2+Z*[3**B3+Z*[4**B4+Z*[5**B5+Z*[6**B6+Z*[7**B7**B4*Z*
                                                                                                                                                                                                                                                                        A=AO/E1+A2*AL9G[E2]-A4*AL9G[-E3]+A6*AL9G[E4]+A9*ATAN[A10*Z-A11]
1-A12*AL9G[E5]+A15*ATAN[A16*Z-A17]-A18*AL9G[E6]+A21*ATAN[A22*Z-A23]
                                                                                          VS IS IN METERS PER SECOND
DRHO, DPRES, AND DVS ARE IN SAME UNITS AS RHO, PRES, AND DVS BVER
                                                                                                                                                                                                                                                                                                                                                                                                                                                      DRHG = -RHG * [D1 *DA + DTEMP/TEMP]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         60,60,50
                                                                                                                                                CONTINUE
IF [Z-200.] 40,40,30
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              IF [ALT] 70,80,80
RHP=RH0+DRH0*ALT
PRES=PRES+DPRES*ALT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        IF [ EALT-200./.001]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                 DVS=.5*D4*DTEMP/VS
DPRES==D1*PRES*DA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         PRES = DPRES * A + PRES
                                                                                                                                                                                                                                                                                                                                                                                                                    RH8=D2*PRES/TEMP
                                                                                                                                                                                                                                                                                                                                                                                                  DTEMP = DTEMP * .001
                                                                                                                                                                                                                                                                                                                                                                                                                                             VS=SQRT[D4*TEMP]
                                                                                                                Z=ALT**001
IF [Z] 10,20,20
                                                                                                                                                                                                                                                   E5=Z2-A13*Z+A14
                                                                                                                                                                                                                                                                                                           AAC==:060803123
                                                                                                                                                                                                                                                                                                                                                                                                            PRES=EXP[+D1*A]
                                                                                                                                                                                                                                                              E6=Z2-A19*Z+A20
                                                                                                                                                                                                                                                                                                                      AAD=-.028429767
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    A=ALT-200./.001
                                                                                                                                                                                                                                                                                                 AAB=+018031036
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               RHG=RHG+DRHG*A
                                                                                                                                                                                                                                        E4=Z2-A7*Z+A8
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  VS=VS+DVS*ALT
                                                                                                                                                                                                                                                                                                                                                                                                                                  PRES=D3*PRES
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     VS=VS+DVS*A
                                                                                                                                                                                                                                                                                                                                                      DA=DA*.001
                                                                                                                                                                                                                                                                                                                                                                                        188*2111111
                                                                                                                                                                                 CONTINUE
                                                                                                                                                                                                                  E2=2+A3
E3=2-A5
                                                                                                                                                                                                        E1=Z+A1
                                                                                                                                                                    Z=200.
                                                                                                                                                                                           2*2=22
                                                                                                                                      •0=Z
                                                                                                                                      200
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C9 MM P P P P P P P P P P P P P P P P P P	ALLOCATION 7777 A8 7777 A12 7777 A12 7777 A12 7777 A16 7777 B9 0 7777 B8 7775 B8	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	AAA AAS AA13 AA17 AA17 DD	777782 77762 77748 77738 77732 77712 77712	A A A A A A A A A A A A A A A A A A A	77777 77750 77750 77750 77774 77772 77770 77770	AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
7666 GRAM 00054 00102 0110 UMMY PRGGR	GCATIGN GS MP G REQUIR	0056 0056 0044 007 0044 007 007 007	ZZ EE2 EE6 PAAD VEES P	0066 0066 0066 0066 0066 0066	ALT E3 A A RNA DRES	ΦΝΟΣΣ	Z 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4

	DUMMY COSA
[SINA, CBSA, A] 0 0 0 120 8A]]	A SINA
SAJJ 8	DUMMY
NA / CB	С.
SUBROUTINE 1F [CBSA] 1F [CBSA] 60 10 130 A=15*PI 60 10 130 A=2*PI-A 60 10 130 A=2*PI-A 60 10 130 A=10 130	CATION 1. 00013 REGUIRED
1100 00 00 1110 1300 1300 1100 1100 110	an (i)
多人 うらか ちさ でう ご う ご う ご う ご ご ご ご ご ご ご ご ご ご ご ご	PREGRAM ALLI 00011 TANI DUMMY A SUBPREGRAMS THE END
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DCA=DC1/C2-[C1*DC2/[C2*C2]]
A1=AETA[1]+AETA[10]*G[2]+AETA[4]*G[4]+AETA[6]*G[5]+AETA[8]*G[6]
A2=1•+AETA[2]*G[2]+AETA[3]*G[3]+AETA[5]*G[4]+AETA[7]*G[5]*G[5]
                                                                                                                                                                                                                                                                                                                                                                                                                    B1=B1+ACLA[1]*G[1]
B2=1.+ACLA[9]*G[2]+ACLA[10]*G[3]+ACLA[11]*G[4]+ACLA[12]*G[6]+ACLA[
113]*G[7]+ACLA[14]*G[8]+ACLA[15]*G[9]+ACLA[16]*G[10]+ACLA[17]*G[11]
                                                                                                                                                                                                                                                                                                                                                          DA1=AETA[10]+3.*AETA[4]+G[3]+4.*AETA[6]+G[4]+5.*AETA[8]+G15]
DA2=AETA[2]+2.*AETA[3]+G[2]+3.*AETA[5]+G[3]+4.*AETA[7]+G[4]+5.*AET
1A[9]+G[5]
                                                                                                                                        COMMON ACLA, ACA, AETA
COMMON RC, AMC, CTHC, RCTHC, SRAD, SCRAD, CRAD
                                                                                                                                                                                                                                   C2=1.+ACA[19]*G[11]+ACA[18]*G[10]
C1=ACA[9]*G[9]
DC1=0.
DC2=10.*ACA[19]*G[10]+9.*ACA[18]*G[9]
                                                                                                                                                                                                                                                                                                                                                                                  ETA=A1/A2
DETA=DA1/A2=[A1*DA2/[A2*A2]]
B1=ACLA[18]*G[12]
D8 50 1=1.8
                                                                                                                                                                                                                                                                                               DC1*DC1+I*ACA[1+1]*G[1]
                                                                                                                                                                                                                                                                                                        DC2=DC2+I*ACA[I+9]*G[I]
                                                                                                                                                                  IF [ACH-23,0] 20,10,10
                                                                                                                                                                                                                                                                                                                                                                                                                                                      DB1=11.*ACLA[18]*G[11]
                                                                                                                                                                                                                                                                              C2=C2+ACA[I+9]*G[I+1]
C1=C1+ACA[I]*G[I]
                                                                                                                                                                                                                             G[1] =G[1-1] *G[2]
                                                                                                                                                                                                                                                                                                                                                                                                                                              2+ACLA[19] *G[13]
                                                                                                                                                                                                   G[1]#1*0
G[2]#ACH
D0 30 ]#3#20
                                                                                                                                                                                                                                                                     De 40 I=1,8
                                                                                                                                                                                   ACH#23.0
                                                                                                                                                                                                                                                                                                                CA=C1/C2
                                                                                                                                                                           10 XS=ACH
                                                                                                                                                          NMC#0
                                                                                                                                                                                                                                                                                                                                                   16[6]
                                                                                                                                                                                                    80
                                                                                                                                                                                                                             30
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ACLA[11]*G[3]+5**ACLA[12]*G[5]+6** •*ACLA[15]*G[8]+9**ACLA[16]*G[9]+1 [12]		77770 A3 77760 A7	77750 A11	77740 A15	77720 A23	77710 B3	77700 B7 77670 D3	77660 AZ	77076 AB	ひつばなべ しに A	77040 VRM	77026 00	77006 BM	/6//6 TU	DUMMY ACH	76736 WKG0	u CY U	76706 RXVOB	76596 OTE 76596 ACA	76462 CTHC	CRA		164	27 4 XS	00310 DA2 00314 DB2	
+11*G[I] CLA[10]*G[2]+3**, CLA[10]*G[2]+3**, ACLA[14]*G[7]+8 1+12**ACLA[19]*G DB2/[B2*B2]] ACH] ACH] *ACH]		77772 AZ 77762 A6	7752	7742	7722	7712	7702	7662	7104	7070	7044	7030	7010	7000	6750	6740	6730	6714	0740	6464	6454		0126 X 0262 V	A 6060	00306 DA1 00312 DB1	DUMMY DCLA
DB 60 1=1,7 DB1*DB1+11*ACLA[1] DB1*DB1+11*ACLA[1] ACLA[13]*G[6]+7*ACLA[13]*G[6]+7*ACLA[13]*G[10]	Z O	77774 A1 77764 A5	A 9	< <				2 2		ם ה	7 K			7 0	200	S	ï		χ α 7 α	<u>س</u> 2		ATION	RXX RX		DUMMY DCA	THE END
и и и и и и и и и и и и и и и и и и и	COMMON ALLOCATION	77776 AO 77766 A4	⋖(⋖ <	< <	æ	നാമ	α	m.	4 (צו נ	· >		∢ ⊔			ř	5	χ υ Χ υ Χ υ	76470 AETA	RCT	PRAGRAM ALL BCAT	0040	0271 I	DUMMY CA DUMMY ETA	

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SUBRBUTINE BBUND [TF,X,DX,B,ERR]
DIMENSION X[15], DX[15], ALPH[13], BETA[13,12], CH[13], AB[3]
DIMENSION VR[3], U(3], ALB[3], DB[3], UO[3], UOD[3]
DIMENSION ROB[3], RXVOB[3], RXVOB[3], RXVOB[3], RXVOB[3], RXVOB[3], RXVOB[3], RXVOB[3], RXVOB[3], DXE[3], DXE[3], DXE[3], DXE[3], DXE[3], DXE[3], UYE[3]
DIMENSION VXR[3], VXRXV[3], UXE[3], UYE[3]
DIMENSION AETA[15], ACLA[20], ACA[20]
                                                                                                                                                                                                                                                                 B[4]=0.

D9 20 I=1,3

20 B[4]=B[4]+X[I]*[ROB[I]*SRAD-RVR[I]*CRAD]

B[4]=B[4]/RC

B[5]=0.

D6 30 I=1,3

30 B[5]=B[5]+X[I]*RXVOB[I]

B[5]=B[5]-X[I]*RXVOB[I]
                                                                                                                                                       COMMON ACLA, ACA, AETA
COMMON RC, AMC, CTHC, RCTHC, SRAD, SCRAD, CRAD
                                                                                                                                                                                                                                                                                                                                                                                  A = [AB[1] + X[1] + AB[2] + X[2] + AB[3] + X[3]] + R]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         PVXB[I,I]=0.

0 PAXB[I]=[R]=C13]*X[I]+C12*AB[I]

1 PVXB[I,2]=0M*AB[3]

1 PVXB[2,3]==0M*AB[1]

1 PVXB[2,3]=0M*AB[1]

1 PVXB[2,1]==PVXB[1,2]

1 PVXB[2,1]=*PVXB[1,2]
                                                                                                                                                                         RC2=RC*RC
AMC2=AMC*AMC
B [1] =R*R/RC2=1.
B [2] = VRM*VRM/VS/VS/AMC2=1.
V2=X [4] *X [4] *X [5] *X [5] *X [6]
                                                                                                                                                                                                                                                 B[3] *B[3] +X[]] *X[]+3]
B[3] *B[3] /RC/SQRT[V2] =CTHC
                                                                                                                                                                                                                                                                                                                                                                                                                                  RE=AA*BE/SORTIC6J
C12*RE*A*C5/C6*RI
C13*C12*A*RI
D0 40 1=1,3
                                                                                                                                                                                                                                                                                                                                                                                                                C5=AA*AA-BE2
C6=BE2+C5*E2
                                                                                                                                                                                                                            B[3]=0.
DB 10 I=1,3
                                                                                                                                                                                                                                                                                                                                                                                           BE2=8E*8E
                                                                                                                                                                                                                                                                                                                                                   R2*R*R
R1=1•/R
BB=AA*R1
                                                                                                                                                                                                                                                  0
                                                                                                                                                                                                                                                                                          20
                                                                                                                                                                                                                                                                                                                                 30
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D6 70 1=1,3

P8xAT[1,1]=2**X[1]/RC2

D6 60 J=1,3

P8xAT[2,1]=P8XAT[2,1]+2**VR[J]*PVXB[J,1]

P8xAT[2,1]=[PBXAT[2,1]+2**VRM2*DVS*PAXB[I]/VS]*C3

P8XAT[3,1]=X[1+3]=2**VR[1]*C3

P8XAT[3,1]=X[1+3]=C4*[X[1]-C1*X[1+3]/V2]

P8XAT[4,1]=[ROB[I]*SRAD*RVR[I]*CRAD]/RC

P8XAT[4,1]=[ROB[I]*SRAD*RVR[I]*CRAD]/RC

70 P8XAT[4,1]=RXVOB[I]/RC

D6 90 1=1,6

D6 80 J=1,5

B0 B[1+5]=0*

B0 B[1+5]=0*

B0 B[1+5]=X[1+8]+B[1+5]

B(12]=X[1+8]+B[1+5]

B(12]=X[15]-1*

HAM=X[9]*DX[1]+X[10]*DX[2]+X[11]*DX[3]+X[12]*DX[4]+X[13]*DX[5]+X[1]

14]*DX[6]*X[15]*X[15]*[CK1*RMD*CK2*DX[7]+CK3*DX[8]]
PVXB[3,2]==PVXB[2,3]
CALL ATMGS (ALT,TEMP,PRES,RH0,VS,DVS,DRH0,DPRES)
RC2=RC*RC
AMC2=AMC*AMC
VRM2=VRM*VRM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         A A 111
A A 115
B A 23
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              77750
77750
77750
77770
77770
7760
                                                                                                                                                                                          VI=1.7SQRT[V2]
C1=X[1]*X[4]+X[2]*X[5]+X[3]*X[6]
C3=1.7[V5*V5*AMC2]
C4=1.7RC*VI
                                                                                                                                                                          V2=X[4]*X[4]+X[5]*X[5]+X[6]*X[6]
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        RCBNV
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            A28
A410
A414
A418
BB2
BB6
BB6
BB11
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              D0 100 1=1+13
ERR=ERR+B[1]*B[1]
RETURN
END
                                                                                                         D0 50 1=1.5
D0 50 J=1.6
PBXAT[[.J]=0.
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  ALPH
BEDA
ETA
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      B[13] = HAM
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          77777
777564
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        77776 A0
77766 A4
77766 A8
77746 A16
77736 A16
7776 B8
7776 B8
77706 B4
77676 B8
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77054	∝=	77052	RE T	77044	7 Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y	77042	N 0 ₩
702	ALB	701	08	701	BE	700	Σ Θ
700	AA	700	5	700	I	677	5
677	L.	677	RISP	677	RMD	676	EXA
676	on	675	aon	675	۸s	674	ACH
674	10	674		674	90	673	WKGO
673	œ	673	•	673	CK1	672	U.Y.D
672	¥	672	RCURV	671	ROB	670	RXVOB
670	>	667	·	667	UXE	999	UYE
999	9	499	PB	657	ACLA	652	ACA
647	ш	949	RC	646	AMC	646	CTHC
949	5	645	SRAD	645	SCRAD	645	CRAD
PRBGRAM	ALLOCATION						
Σ̈́		DUMMY	ΩX	003	PBXAT	013	PVXB
00152	ХВ	DUMMY	80	00160	VXR	00166	VXRXV
017	ĽMI	00212		021	<u>ت</u>	021	BBUND
021	C2	00220	AMC2	022	٧2	022	82
022		00230	88	023	⋖	023	BE2
023	ณ	00240	င္မ	024		920	C12
920	13	00250	Σ	025	DVS	025	DRHO
025	PRES	00200	œ	026	1>	026	<u>:</u>
026	m	00270	4	027	HAM	Σ	ERR
SUBPREGRAMS	AMS REGUIRED	ED					
SORT	ATMOS						

.000000000000 .10416416000+0	101	8 H 0c ≻	.65000732772+07 62981421000+07	n n	•79182741874+09 •12244760000+07	# H E H G	.2860319000+15
DY # #	DY # #	.9119	**17567557000+04	DDZ m	.58346132000+04 -17680016844+01	42 # ALT #	•90000000000000+02 •14030918564+06
V V V X X X X X X X X X X X X X X X X X	X X X X X X X X X X X X X X X X X X X	**************************************	**47030056509+04 **47030056530+00	# # \$ } \$ }	17140022624÷04 .40651458587+00	VRZ #	56813936515+04 78330279570+00
m k	m k	- 181	.16658663157+01 18117236956+02	# # } } }	.27324664037+02	LF2 #	97032050795+01 20675941056+02
# #		469	46903918859+00	00	.45523371732+00	ETA N	*17999863636+01
) # -		.162	16234500072-02	1 H	-+5750000139-05		.78750000512-05
· WWX		. 478	47881444528+00	# \ WO	87791612754+00	# 2W0	-,77140676824-08
•400000000000+03 MD # +0000 •00000000000 XRNG# +8890		988	88986254448-12	D V L	.91500003418+02	DCEL	.30476263426-03
r a xon	1	470	•47030056530+00	UOY =	.40651458587+00	# Z00	7833027957n+00
H 1	H 1	.220	*22044155789=03	C007	27374111417-03	U002#	•57787813012*03
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Z LAMZ#		.5885	58856570851+03	LAM3=	. 60580489990+02	HAN	.23216986778+04
LAMSH		161.	19169952861+06	LAM6=	.30856165926+05	LAM7	•10000000000000000000000000000000000000
* 16161706463+00 OTFRE 1*464.		4 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +	.46427924821+00 .58854778008+03		.18812765169+00 60573264674+02	POPUT N V W	00000000000
				INTERM	INTERMEDIATE VALUES 10		INTEGRATION STEPS TAKEN
# #	R # 6480	.6480	64805373374+07	# >	.79418704794+04	E G	.39860319000+15
H >- 49	Y =6427	6427	.64277122900+07	2	•63356744889+06	D.H.	.28608000000+02
# 10	11	**8300	*83007721734+03	# 20	59694703170404	AZ H	.90000000000+02
# * 00	#	939	.93924642679+01	= 200	00+0908388684**	A	*12008877289+06
* 3280731000+06 VRX H **513 *77705084518+04 UX H **4903	B 8		*51314513323+04 *48929066245+00	> = * > * =	-+KG795576590+U3	U K Z #	57789462198+04
794+02 LFX = .		.254	25489098925+02	L F Y	.15190362932+03	LF7 #	43870884789+02
3 DFX .		.846	84683458435+02	B	13333554990+02	0FZ =	-,95368955157+02
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		.162	16234500072-02	H I I I I	57500000139-05	10	.78750000512-05
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MD M	•	• 000	0000000000	# DE TO	.23829033117+03	CHIY	.23968567814+02
× KNG III	•	.4783	47832879956+02	PANGE	-91320019547+02	# 1300	.15448448591-02
· E XOO	•	.4703	47030056530+00	# \ 00	.40651458587+00	# ZON	78330279570+00
• RXCOD	•	.2204	22044155789-03	UODY	27374111417-03	#2000	.57787813012-03
.01 CLA		.75999	75999960681+00	H X X Y X	•0000000000	H L I	.61073730421-08
# CXS	e :	. 5000	500000000000000000000000000000000000000	# 22.0	00+000000000000000000000000000000000000	# N	*73052000000+00
# 	R	. 2548	25481720258+02	# 1 L H Q	*40849534874+00		-41469047409-04
LATE		96549	65490027419+02	#5 NO	.19404843730403	# 05 N J	* 6000000000
*63760870321+02 LAMZ# *5455	• •		54587222069403 13504341332404	LAMA	.247361517657+02	1 A A A A A A A A A A A A A A A A A A A	+23213750478404
DLM2#		3900	3900281212+00	DLM3#	*92664419706+01	POPU	*0000000000*
DLMS# =	•	- 545	582614493+03	DLM6=	74331304179+02	DLM7	• 00000000000

.39860319000+15 .286080000000000000000000000000000000000	.7875000512-05 .23944097074-08 .23944097076-01 .1994489726-01 .1994489726-03 .57787813012-03 .61073730421-08 .53901228658-02 .00000000000000000 .23188284803+04 .100000000000000000000000000000000000	INTEGRATION STEPS TAKEN SM	.3986U317UBU+15 .28608000000+02
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.79624354856+04 .33455981201+05 60181289967+04 16501651439=01 .11846673025+03 .216961811450+00 .21695196137+02 .21695196137+02	- 6750000013920 - 87791612754+00 - 87791612754+00 - 87791612754+00 - 1124768168+02 - 40651458587+00 - 2737411417-03 - 50000000000000 - 17099169834+01 - 181456984+02 - 16259395019+05 - 2727257098-01	V = RMEDIATE VALUES 10 V = -79756196417+04 Z = -56706769507+06 DOZ = -59769404362+04 UV = -69769408174+00 VVY = -98728488174+00 UV = -98728488174+00 EV = -98728488174+00 FF = -8879182850400 FF = -887918199+04 CM = -1584781971+00 CM = -1584781871+00 CM = -158478181+00 CM = -158478181+00	*17590774/82404 **11588229119+07
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.\$9000000 .\$8981355629+05 .\$55607310917+04 .*75200317358+00 .*774696988+05 .1799998088+01 .\$3567840000+07	100000000000000000000000000000000000000	INTEGRATION STEPS TAKEN GM = .39860319000+15 PHI = .286080000000000 AZ = .9000000000000000 ALT = .943082257949404 UZ = .073962067923+00 LFZ = .12523605346+07	.18000008244+01 .4354784000405 .787500051205 .23771911160+02 .23791911160+02 .23791911160+02 .23791911160+03 .5781813012-03 .61073730421-08 .7305200000000 .11452221211+05 .00000000000000000000000000000000000	INTEGRATION STEPS. TAKEN GM # .39860319000+15 PHI # .2860800000000000 AZ # .900000000000000000000000000000000000
7			MAY A MAY B M M M M M M M M M M M M M M M M M M	IN TEGA
\$8441025869+04 .16909364966+01 .20486291593+04 .40452405976+00 .216417280482405 .51573348517-01 .63781660000+07	20	INTERMEDIATE VALUES 14 V = .76849731107+04 Z = .17373285355+07 DZ = .46573283197+04 DOZ = .46573283197401 UY = .40341612330401 LFY = .91055119764+06 DFY = .85531277221+06	.12208625719-01 .6378166000407 .87791612754+00 .23393152663+03 .93279279851402 .9000000000000000000000000000000000000	NTERMEDIATE VALUES 92 " "42964437763+04 " "21828397015#07 Z " "32771262273+04 DZ " «11484259158+02
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	# 8 # # # # # # # # # # # # # # # # # #		R H H H H H H H H H H H H H H H H H H H	1 N TERM V Z D Z B B B D D Z B B B D D Z B B B B D D Z B B B B
.20890902733+04 .10772812782+02 5057068269+04 52043396508+00 .1722327494+05 .172327494+05 .172560501+00	.47881444528+00 .0000000000000000000000000000000000	.64016959419407 .3136802524407 .3136802909404 .42133842381401 .40948521059404 .53871762763400 .98922588284406	. 1076568008*01 . 17667476075+09 . 176234600 . 4788144658+00 . 26374400841+05 . 2204415578+00 . 7690105010+00 . 50000000000+00 . 10644384606+05 . 10644384606+05 . 10644384606+05 . 10644384606+05 . 10644384606+05 . 20379827272+03	.639618DDD21+D7 57422D99169+D7 .17619159636+D4 50964577714+D1
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-,49828819897+04 -,32974219418+01 -,13280731000+06 -,77905424194+04 -,11196040465+02 -,21874680076+03 -,65821803840+03 -,97519607922-04	.0000000000000000000000000000000000000	.5000000000000 1.14839846598+07 1.328306746+04 1.182596734+02 1.3280731000+06 74942564701+04 81163340845+00	.65821803840+03 .92336288826-02 .7922150604-04 .0000000000000 .4000000000000 .40000000000	.6000000000000000000000000000000000000
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CI = .77740384104528 C D = .62781660000000	CI = .777470384104528-00		+59379286215+01	DFX #	10644861404+07	DFY #	v.	DFZ #	13782655956+07
9	9		.65821803840+03		*73748703372-02	: C	.12097966434*01	ETA #	1799988497+01
No.	FLAME 1023400072-02 FH 8 57790000000137-05 FD 8 MEAN 9942400072-02 FH 8 5779161274-01 CHIYB MEAN 9942400182-02 CHIPB 22324901434-03 CHIYB MEAN 9942400182-02 CHIPB 2232490143-03 CHIYB MEAN 994240182-02 CHIPB 2232490143-03 CHIYB MEAN 994249844-00 CK3 8 9500000000000 CHIRB MEAN 950000000000000 CK3 8 95000000000000 CHIRB MEAN 950000000000000 CK3 8 9500000000000 CHIRB MEAN 95000000000000 CK3 8 95000000000000 CHIRB MEAN 95000000000000 CK3 8 950000000000000 CK1 8 MEAN 95000000000000 CK3 8 950000000000000 CK1 8 MEAN 95000000000000 CK3 8 95000000000000000000000000000000000		.2946146969-01	GY I	.15787038410+09	A E	-63781660000407	# 60	*63567840000+07
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UDDXX .22044155789-03 UDDYX .27394111417703 UDDXX CLA5009000000000000000000000000000000	CLA = .2204415789-03 U0DV = .2735411417403 U0DDZ CLA = .550000000000000000000000000000000000		.18025458123+04	a XOO	**47030056530+00	100 100	*40651458587400	200	78330279570+00
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LAT M .40904536064n2 LONG .1556452206403 LNGO= LAMSE .55546745104+14 LAM3 .32196815229+14 LAM7E .55546745104+14 LAM3 .32196815229+14 LAM7E DLM2 .20156068864+16 DLM3 .550935794977+13 POPUE DLM2 .13149816070+14 DLM3 .550935794977+13 POPUE DLM2 .20156068864+16 DLM3 .550935794977+13 POPUE N .17356023578+64 DZ24779350845+04 AZ .8007 MY24779350845+04 AZ .8007 MY247793508584-05 DFT24164455884-05 DFT24164455884-05 DFT24164196708 DFT44164196708 DF	LAT # .40004536066472 LONG		,91344056582+05	H	.32506473427+05		.71291613375+02	OCL I *	.15018163974+06
LAMS 55546745104+14 LAM3 21908015329+14 HAM	LAMS 55546745104+14 LAM3 21408015329+14 HAM		.28365724924+03	LAT =	.40904536066+02		. 15566450206403	LNGO	.00000000000
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R a	R ** 644110712343407 V ** 37251818845404 GH ** γ ** 17385023578404 DZ ** 32760956529404 AZ B 00 γ ** 17385023578404 DZ ** 32760956529404 AZ B VRX ** 18170101401 VRY ** 3760956529404 AZ B UX ** 1817011349406 DF ** 11817011349406 DF B LFX ** 14193841713406 DF ** 11817011349406 DF B DFX ** 14193841713406 DF ** 11817011349406 DF B CL ** 5704266378-01 CF ** 17864076974906 DF B FJ ** 16234600072-02 FH ** 57500000139965 DF B FJ ** 16234600072-02 FH ** 57500000139965 DF B FJ ** 16234600072-02 FH ** 57500000139966 DF B FJ ** 4703000000000 CHIP ** 57501441477 DC B CK					INTER	N		ATION STEPS TAKEN
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UX *** - 19842591088+04 VRY *** - 16519835179+04 VRZ *** - 19842591088+04 VRY *** - 1819244703+06 UZ *** - 1819247400 UZ *** - 18192841713+06 DFY *** - 181928417450 DFY *** - 181928016 DFY *** - 18	UX		17485959140+01	100 ×	.21917311000+01	200	.32760956529401	ALT B	.41033067913405
UX	UX		.13280731000+06	# XXX	19842591088+04	Y KY	.16519835179+04	WEZ #	24214953130+0ª
LFX = -30485632916+06 LFY = -1181701349+06 LFZ = - CL = -57042560378-01	LFX = -30485632916+06 LFY = -1181701349+06 LFZ = - CL = -5704256378-01 CD = -1786407697401 ETA = - G = -14174118739+08 AE = -1786407697401 ETA = - G = -16234500072-02 FH = -5750000139+05 FD = - FJ = -16234500072-02 FH = -5750000139+05 FD = - MD = -4788144528+00 OMY = -8750000139+05 FD = - MD = -4788144528+00 OMY = -887501455688+03 CH1Y* - CLA = -13955671345+00 PANG* -88255741411942 OCEL* - UODX* -22044155789+03 UOOY* -027374111417+03 UODZ* - UODX* -22044155789+03 UOOY* -027374111417+03 UODZ* - CCA = -76011501781+00 CK3 = -5805000000000+00 RCRV* - HTI = -35875626844+05 CHTI = -1588117877+02 OCLI* - LAME* -31449145572+19 LAM* -1338098228+18 HAM* = - LAME* -3682910564237+19 LAM* -1338098228+18 HAM* = - LAME* -53991491810407 Z = -273523415407 PHI = - NOV = -53991491810407 Z = -273523415407 PHI = - NOV = -53991491810407 Z = -273523415407 PHI = - NOV = -23653377706+00 UVY = -35672525987+04 AZ = - NOV = -23653377706+00 UVY = -356725259404 AZ = - NOV = -23653377706+00 UVY = -39567298136+00 UVY = - NOV = -23653377706+00 UVY = -39567298136+00 UVY = - NOV = -23653377706+00 UVY = -39567298136+00 UVY = - NOV = -23653377706+00 UVY = -39567298136+00 UVY = - NOV = -23653377706+00 UVY = -39567298136+00 UVY = - NOV = -23653377706+00 UVY = -39567298136+00 UVY = -39567298136+00 UVY = -		,35397702334+04	* XO	58727653040+00	# \	.39938819047+00	2 0	-,70398533376+00
DFX # **14193841713+06 DFY # *118170D1349+06 DFZ # * CL # *5704256578*D1 CD # *18170D1349+06 DFZ # # FJ # *16248D0072*D2 FH # *6378166D0001407 BE # FJ # *16248D0072*D2 FH # *6378166D000139*O5 FD # OMX # *47881444528+00 OMY # *687791612754+00 OMZ # # OMX # *47881444528+00 OMY # *687791612754+00 OMZ # OMX # *47881444528+00 OMY # *687791612754+00 OMZ # OMX # *600000000000 CM1P# *62301645688+03 CH1Y* OMX # *6781150134500000000000000000000000000000000	DFX # **14193841713+06 DFY # *118170D1349+06 DFZ # * * * * * * * * * * * * * * * * * *		.43037878741+01	LFX II	-,30485632916+06	F Y #	**71095340403+06	LFZ =	· 23521390044+06
CL = .5704256578=D1 CD = .17864D7674401 ETA = .6474187418739+08 AE = .6578460000+07 8E = .6478444528+00 OMY =657800000139*05 FD OMX = .47881444528+00 OMY =657500000139*05 FD OMX = .47881444528+00 OMY =65750000139*05 FD OMX = .47881444528+00 OMY =687791612754+00 OMX = .47881444528+00 OMY =687791612754+00 OMX =6780100000000000000000000000000000000000	CL = .5704256578=D1 CD = .17864D7674401 ETA = .6704256578=D1 CD = .16236D0001407 8E = .6478166D00010707 8E = .16236D000139=05 FD OMX = .16234D0072-D2 FH = .55750000139=05 FD OMX = .16234D0007000000000000000000000000000000000		53	OFX #	m.14193841713+06	# ¥ Die X	*11817001349406	DF Z ==	17321488423+06
Q M	G M - 14174118739+08 AE M - 6477616400000000 BE M ON M - 14074118739+08 AE M - 647660000139+05 FD M ON M - 162346000012-02 FH M - 627500000139+05 FD M ON M - 147681440 ON M - 147681440 ON M - 147681444528+00 ON M - 1476814451445741414607 PH M M - 14768144614514677460 ON M - 14768144507 PH M M - 1476814614514677460 ON M - 1476814614614607 PH M - 1476814614614607 PH M - 1476814614614607 PH M - 1476814614614607 PH M - 1476814614607 PH M - 147681461461461461461461461461461461461461461		8	٠ ئ	.57042566378-01	8	.17864076974401	ETA B	. 18001834470+01
FJ # 16224500072=02 FH # 5500000139=05 FD # OMX # 47881444528+00 OMY # 637791612764+00 OMZ # MD X # 47030056530+00 OMY # 68265741411402 OCEL# UOX # 47030056530+00 UDY # 40651456588+03 CH17# UODX # 67011501781+00 UDY # 600000000000000000000000000000000	FJ # 16294500072"02 FH # "-5750000139"05 FD # " MD # -0000000000 CHT # "-5730000139"05 FD # " XRNG# -13965671345+06 PANG# -8826741411402 OCEL# UOX # -47030056530+00 UOY # -4065145658+00 ONZ # " UODX# -22044155789"03 UOOY# -27374111417"03 UODZ# CLA # -500000000000000 CK3 # -600000000000 HTC # FC # # -6000000000000 HTC # # -5000000000000000000 HTC # # -5000000000000000000000000000000000		.34372105538-02	x	.14174118739+08	A E	•63781660000+07	# 60	63567840000+07
0 MX = .4781444528+00 0 MY = .6301645688+03 CHIY* = .2301645688+03 CHIY* = .2301645688+03 CHIY* = .2301645688+03 CHIY* = .2301641411910 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000 x = .4788144528+00 000 x = .837794612754+00 000 x = .47030056530+00 000 cHIPs = .23016456588+03 CHIY* x x x x x x x x x x x x x x x x x x x		.72921150604-04	91 -	2=0	T :	** 57500000139*05	£ :	.78750000512+05
MO M	NO		•000000000	E (-	# ·	87791612754+00	# ZHO	BD#678929041/4"
XRNGs,13955671345+06 PANGs .8828544111902 DCELS UOX s4703005630+00 UOY s40651456587+00 UOY s4703005630+00 UOY s40651456587+00 UOY s4703005630+00 UOY s40651456587+00 UOY s4703005630+00 UOY s40651456587+00 UOY s406011501781+00 EXA s406000000000 HTC s406011501781+00 EXA s4060000000000 HTC s406000000000000000000000000000000000	XRNGs, 17305671345+06 PANGs .8828944111902 OCELS UODX s, 47030056530+00 UOY s, 470300576530+00 UOY s, 47030056530+00 UOY s, 47030056530+00 UOY s, 4703005630+00 UOY s, 4703005000000000000000000000000000000000		• 40000000000+03	E .	• 0000000000	E E	.23016456588403	s X I V	23539936750402
UUDX	UODX		. 48835744892+07	# 5 X X X	1913965671345406	# Z Z Z	88285741411402		.63745348739401
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APPROVAL

MATHEMATICAL CONCEPTS AND HISTORICAL DEVELOPMENT OF THE MASCOT GUIDANCE TECHNIQUE FOR SPACE VEHICLES

by C. D. Baker, W. E. Causey, and H. L. Ingram

The information in this report has been reviewed for security classification. Review of any information concerning Department of Defense or Atomic Energy Commission programs has been made by the MSFC Security Classification Officer. This report, in its entirety, has been determined to be unclassified.

This document has also been reviewed and approved for technical accuracy.

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Director, Aero-Astrodynamics Laboratory

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